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Yoshimine

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(54) **ULTRASONIC PROBE AND ULTRASONIC INSTRUMENT**

(71) Applicant: **OLYMPUS CORPORATION**,
Hachioji-shi, Tokyo (JP)

(72) Inventor: **Hideto Yoshimine**, Hachioji (JP)

(73) Assignee: **OLYMPUS CORPORATION**, Tokyo
(JP)

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Primary Examiner — Ryan J Severson

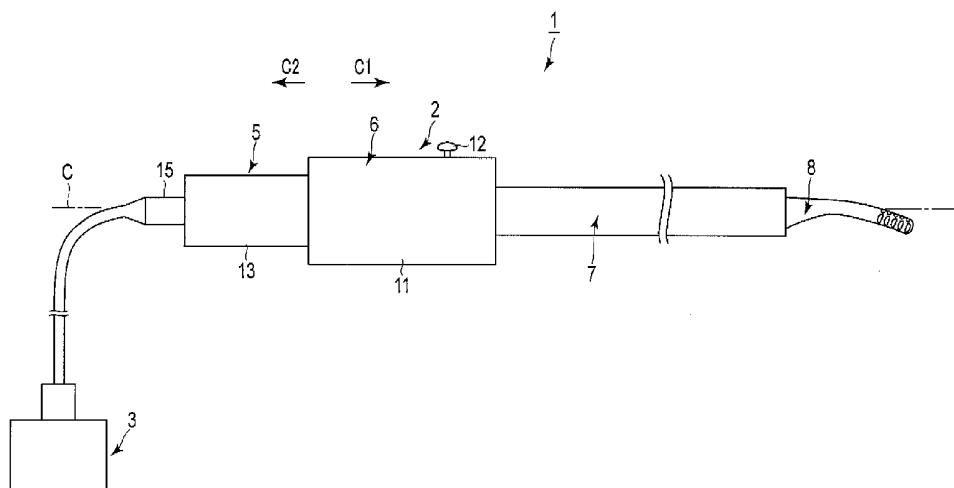
Assistant Examiner — Christian Knauss

(74) *Attorney, Agent, or Firm* — Oliff PLC

(57) **ABSTRACT**

The ultrasonic probe for a shoulder joint includes a curved extending section curved to a probe main body toward a first intersecting direction intersecting a longitudinal axis. The curved extending section includes a first curved outer surface facing the first intersecting direction, a second curved outer surface facing a second intersecting direction opposite of the first intersecting direction, a third curved outer surface facing a first width direction perpendicular to the first and second intersecting directions, and a fourth curved outer surface facing a second width direction opposite of the first width direction. A cutting surface on the second curved outer surface is different from a cutting surface on each of the third curved outer surface and the fourth curved outer surface in extending pattern of the grooves.

17 Claims, 7 Drawing Sheets



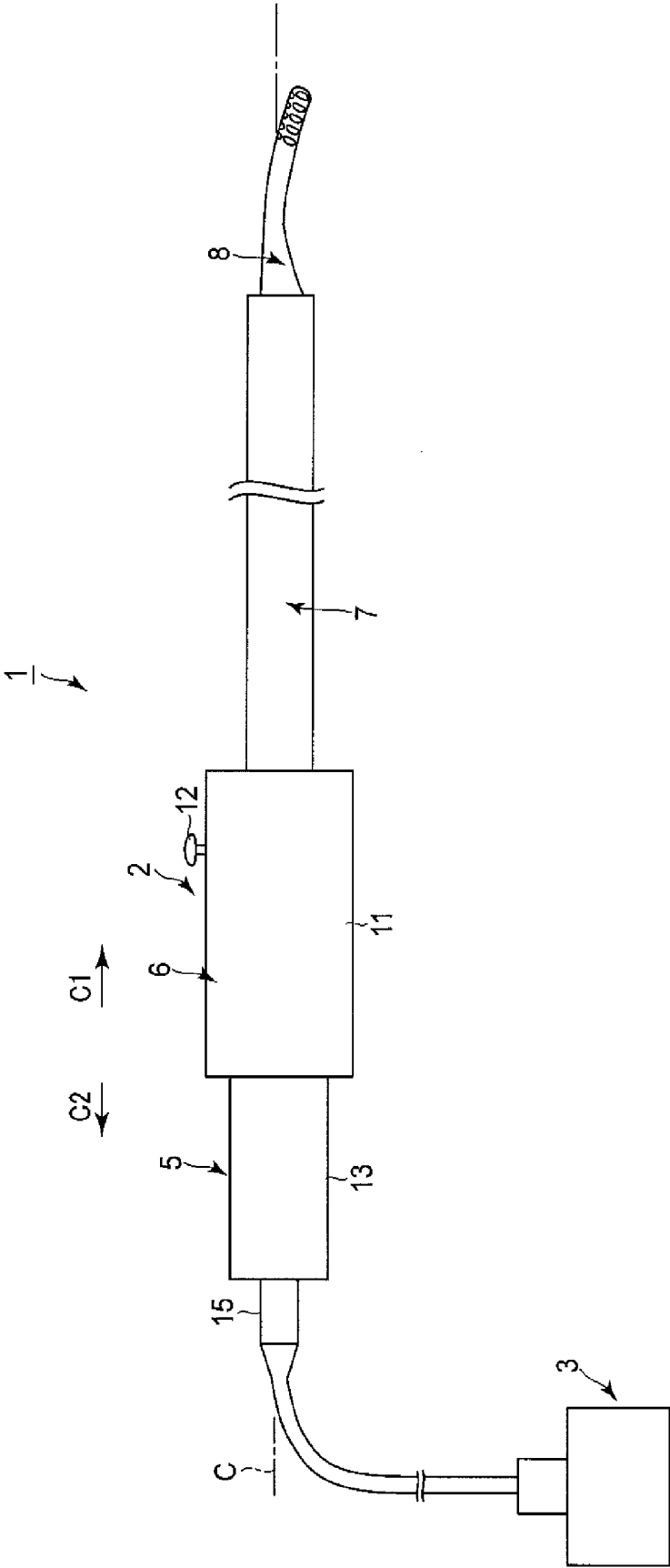
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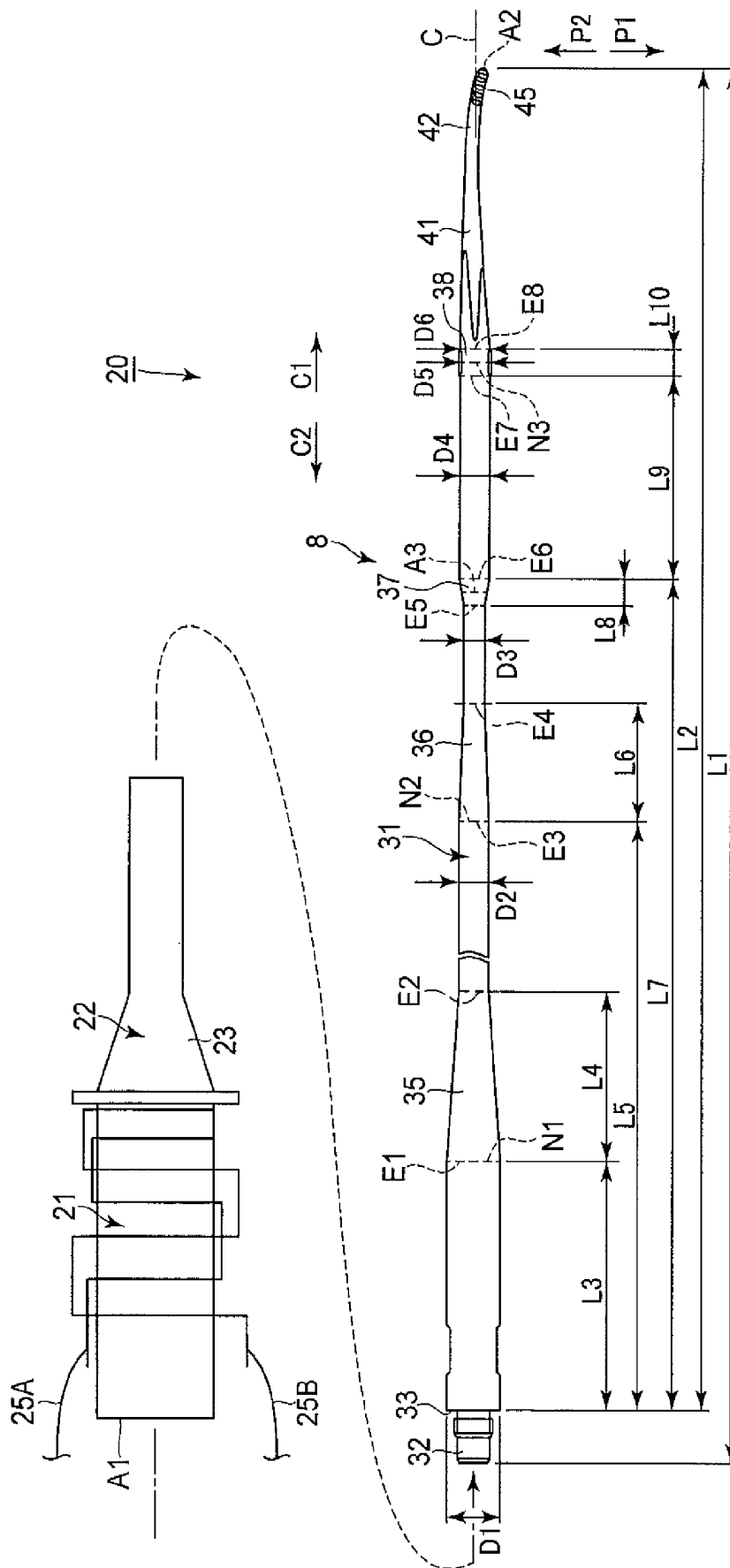


FIG. 2

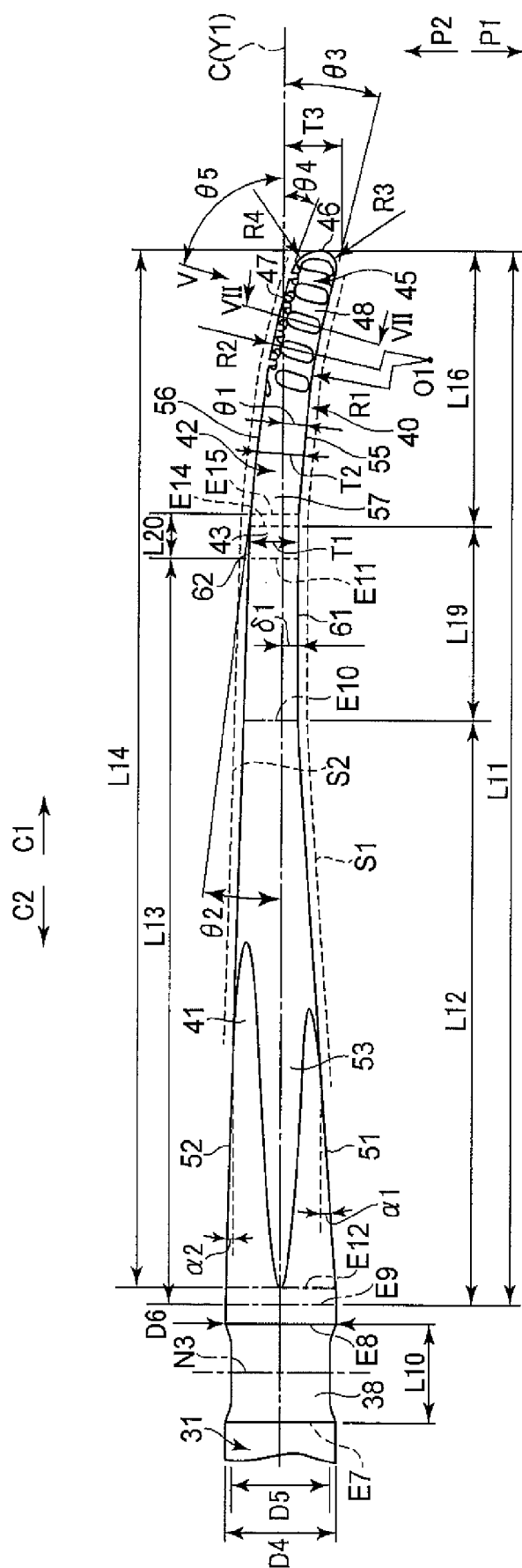


FIG. 3

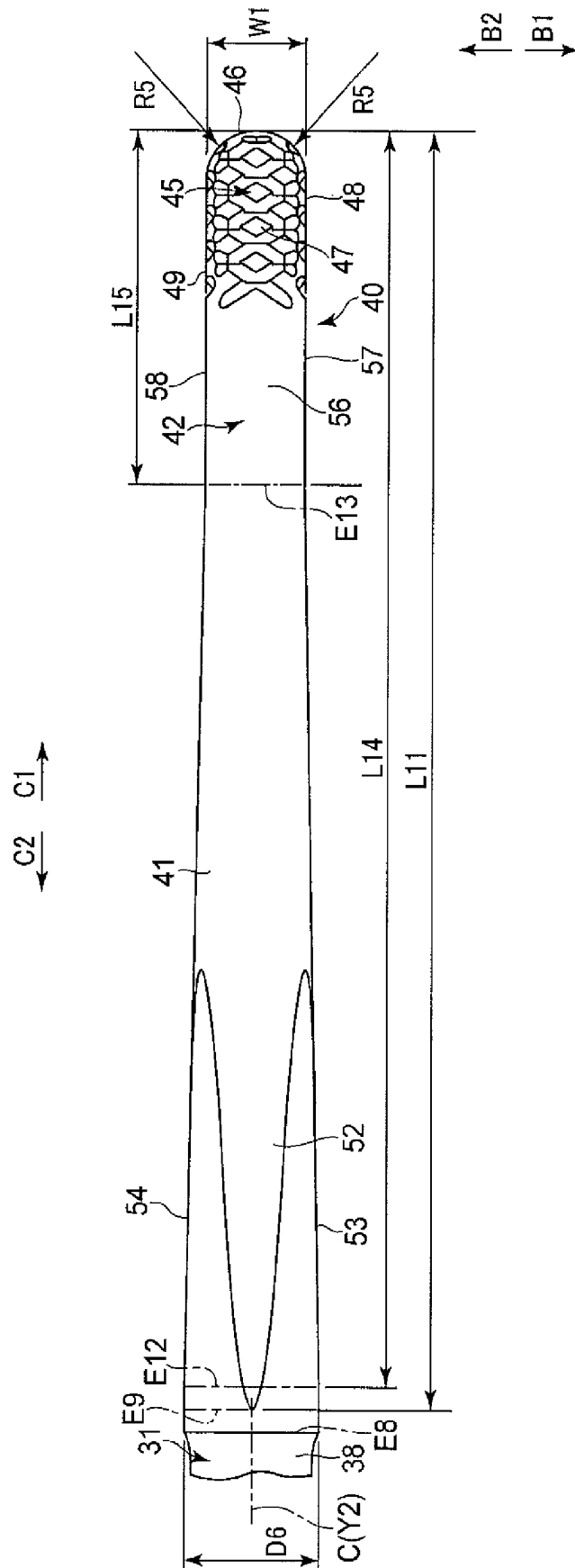


FIG. 4

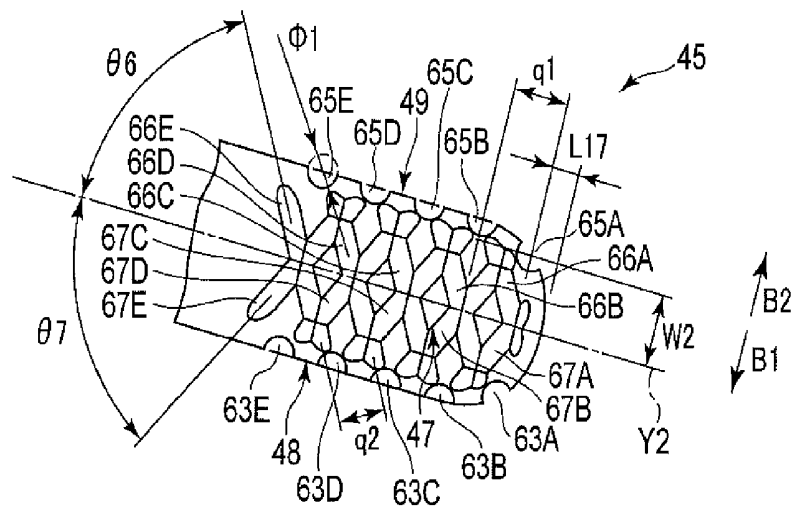


FIG. 5

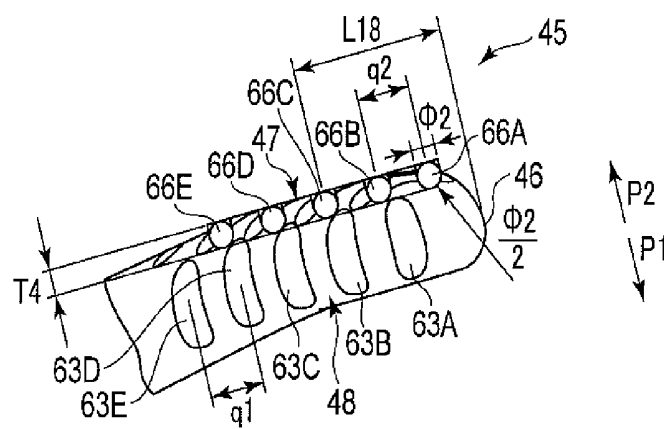


FIG. 6

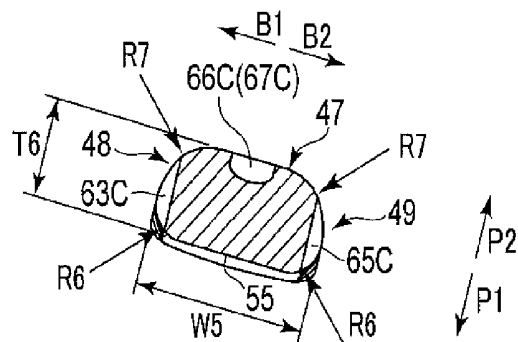


FIG. 7

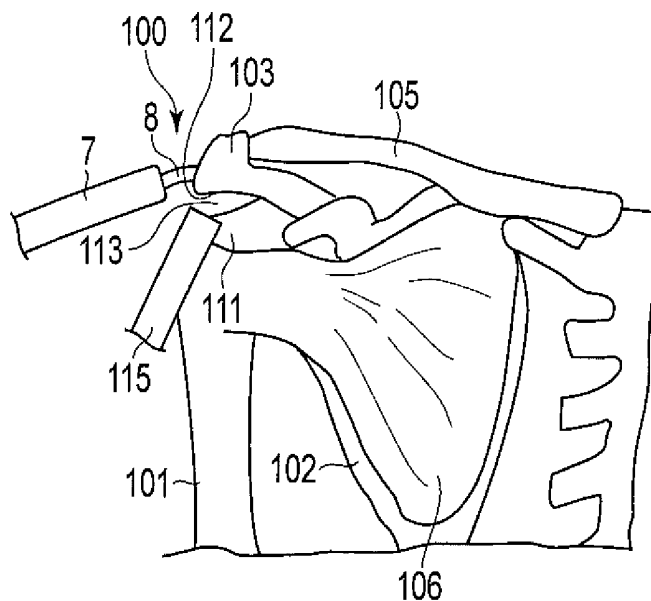


FIG. 8

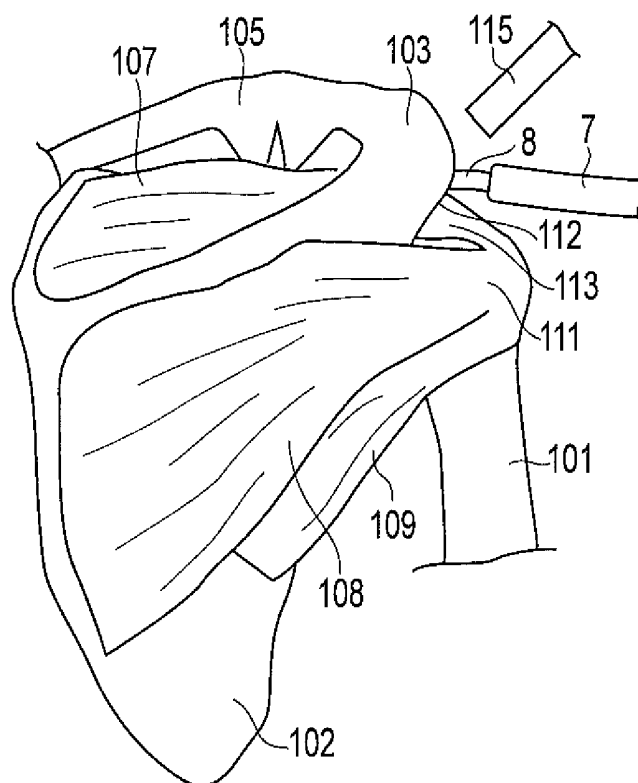


FIG. 9

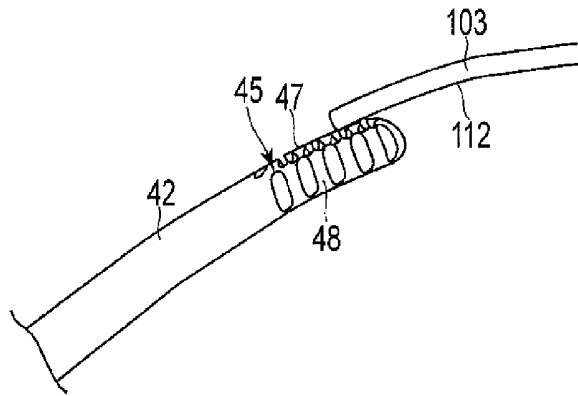


FIG. 10

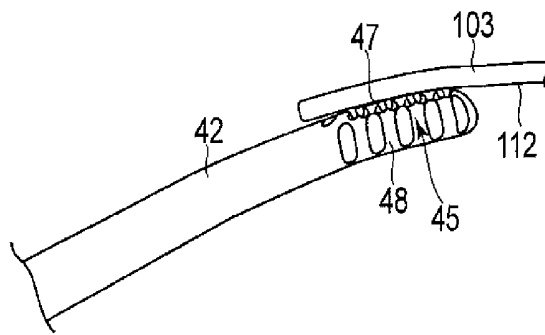


FIG. 11

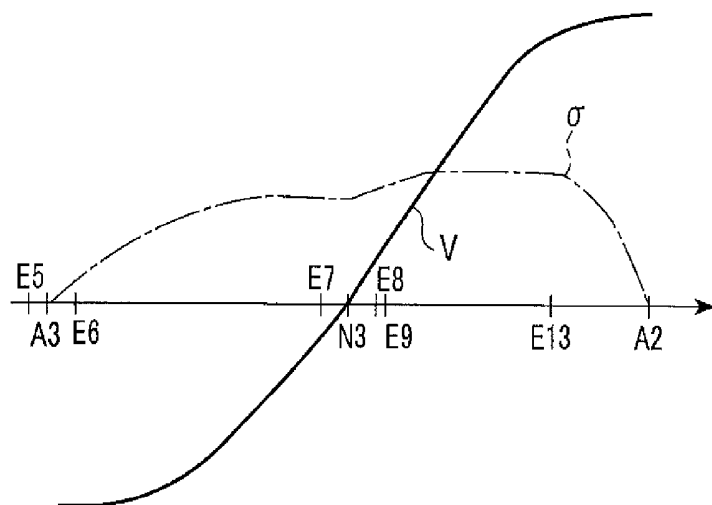


FIG. 12

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ULTRASONIC PROBE AND ULTRASONIC INSTRUMENT

CROSS-REFERENCE TO RELATED APPLICATIONS

This is a Continuation application of PCT Application No. PCT/JP2015/076187, filed Sep. 15, 2015 and based upon and claiming the benefit of priority from prior Japanese Patent Applications No. 2015-001840, filed Jan. 7, 2015, the entire contents of which are incorporated herein by reference.

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to an ultrasonic probe to perform cutting of, for example, a hard bone tissue and a cartilage tissue by ultrasonic vibration.

2. Description of the Related Art

In Jpn. Pat. Appln. KOKAI Publication No. 2005-152098, there is disclosed an ultrasonic treatment device including an ultrasonic probe (an ultrasonic horn). In this ultrasonic treatment device, an ultrasonic vibration generated in a vibration generating section (an ultrasonic vibration mechanism) is transmitted from a proximal side toward a distal side in the ultrasonic probe. In a distal portion of the ultrasonic probe, a scalpel portion is formed as a treating surface. In the scalpel portion, an outer surface of the ultrasonic probe is formed in an uneven state. The ultrasonic vibration is transmitted to the scalpel portion in a state where the scalpel portion is in contact with a treated target, whereby the treated target (e.g., a bone or another hard tissue) is cut.

BRIEF SUMMARY OF THE INVENTION

According to one aspect of the invention, an ultrasonic probe used in a shoulder joint, the ultrasonic probe being configured to transmit an ultrasonic vibration so as to treat the shoulder joint by use of the ultrasonic vibration, the ultrasonic probe including: a probe main body section which is extended along a longitudinal axis, and which is configured to transmit the ultrasonic vibration from a proximal side toward a distal side; a curved extending section which is provided on the distal side with respect to the probe main body section, and which is extended in a state of curving relative to the probe main body section toward a first intersecting direction side in a case where a certain direction intersecting the longitudinal axis is defined as the first intersecting direction; a first curved outer surface which faces the first intersecting direction side in the curved extending section; a second curved outer surface which faces a second intersecting direction side in the curved extending section in a case where an opposite direction of the first intersecting direction is defined as the second intersecting direction; a third curved outer surface which faces a first width direction side in the curved extending section in a case where two directions which intersect the longitudinal axis and are perpendicular to the first intersecting direction and the second intersecting direction are defined as a first width direction and a second width direction; a fourth curved outer surface which faces a second width direction side in the curved extending section; a first cutting surface which forms grooves on the second curved outer surface, and which is configured to cut a treated target; a second cutting surface which forms grooves on the third

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curved outer surface, and which is configured to cut the treated target, the second cutting surface being different from the first cutting surface in extending pattern of the grooves; and a third cutting surface which forms grooves on the fourth curved outer surface, and which is configured to cut the treated target, the third cutting surface being different from the first cutting surface in extending pattern of the grooves.

Advantages of the invention will be set forth in the description which follows, and in part will be obvious from the description, or may be learned by practice of the invention. The advantages of the invention may be realized and obtained by means of the instrumentalities and combinations particularly pointed out hereinafter.

BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWING

The accompanying drawings, which are incorporated in and constitute a part of the specification, illustrate embodiments of the invention, and together with the general description given above and the detailed description of the embodiments given below, serve to explain the principles of the invention.

FIG. 1 is a view showing an ultrasonic treatment device according to a first embodiment of the present invention;

FIG. 2 is a schematic view of a vibrating body unit according to the first embodiment seen from a first width direction side;

FIG. 3 is a schematic view of a distal portion of an ultrasonic probe according to the first embodiment seen from the first width direction side;

FIG. 4 is a schematic view of the distal portion of the ultrasonic probe according to the first embodiment seen from a second intersecting direction side;

FIG. 5 is a schematic view of a second curved extending section according to the first embodiment seen from a direction of an arrow V of FIG. 3;

FIG. 6 is a schematic view of the second curved extending section according to the first embodiment seen from a first width direction side;

FIG. 7 is a cross-sectional view along the VII-VII line of FIG. 3;

FIG. 8 is a schematic view of a state where a bone is cut in a shoulder joint by use of an ultrasonic treatment device according to the first embodiment, which is seen from a front side of the shoulder joint;

FIG. 9 is a schematic view of a state where the bone is cut in the shoulder joint by use of the ultrasonic treatment device according to the first embodiment, which is seen from a rear side of the shoulder joint;

FIG. 10 is a schematic view showing a state where a first cutting surface of a curved extending section of the ultrasonic probe according to the first embodiment is in contact with a lower surface of an acromion;

FIG. 11 is a schematic view showing a state where the first cutting surface of the curved extending section of the ultrasonic probe according to the first embodiment is in contact with a position different from that of FIG. 10 in the lower surface of the acromion; and

FIG. 12 is a schematic view showing an amplitude of a longitudinal vibration and stress due to an ultrasonic vibration between a second distal vibration antinode and a most distal vibration antinode in a state where the vibrating body

unit according to the first embodiment longitudinally vibrates in an established frequency range.

DETAILED DESCRIPTION OF THE INVENTION

First Embodiment

A first embodiment of the present invention will be described with reference to FIG. 1 to FIG. 12. FIG. 1 is a view showing an ultrasonic treatment system 1 of the present embodiment. As shown in FIG. 1, the ultrasonic treatment system 1 includes an ultrasonic treatment instrument (a hand piece) 2, an energy control device 3, and a transducer unit 5. The ultrasonic treatment instrument 2 has a longitudinal axis C. Here, a direction parallel to the longitudinal axis C is a longitudinal axis direction. One side of the longitudinal axis direction is a distal side (an arrow C1 side of FIG. 1), and a side opposite to the distal side is a proximal side (an arrow C2 side of FIG. 1).

The ultrasonic treatment tool 2 includes a holding unit 6, a sheath 7, and an ultrasonic probe 8. The holding unit 6 includes a holding casing 11 to be held by an operator, and an energy operating button 12 that is an energy operation input section attached to the holding casing 11 and configured to be operated by the operator. The sheath 7 that is a hollow tubular member extending along the longitudinal axis C is coupled with the distal side of the holding unit 6. The ultrasonic probe (a vibration transmitting member) 8 is inserted through the sheath 7. It is to be noted that a distal portion of the ultrasonic probe 8 projects from a distal end of the sheath 7 toward the distal side.

Furthermore, the transducer unit 5 having a transducer case 13 is coupled with the proximal side of the holding unit 6. The oscillator unit 5 is connected to one end of a cable 15. The other end of the cable 15 is connected to the energy control device 3. The energy control device 3 includes an electric power source, a conversion circuit to convert an electric power from the electric power source into a vibration generating electric power, a processor (a control section) including a CPU (central processing unit) or an ASIC (application specific integrated circuit), and a storage medium such as a memory. Inside the holding casing 11, there is disposed a switch (not shown) in which an ON/OFF state is changed by an input of an energy operation in the energy operating button 12. The switch is electrically connected to the processor of the energy control device 3 via a signal route extending through the vibrator unit 5 and an inside of the cable 15. Furthermore, in the ultrasonic treatment system 1, a vibrating body unit 20 extends through an inside of the holding casing 11 and an inside of the transducer case 13.

FIG. 2 is a view showing a constitution of the vibrating body unit 20. As shown in FIG. 2, the vibrating body unit 20 includes the ultrasonic probe 8 mentioned above, an ultrasonic transducer 21 that is a vibration generating section constituted of piezoelectric elements, and a relay transmitting member 22. The ultrasonic oscillator 21 and the relay transmitting member 22 are arranged in the oscillator case 13, and the relay transmitting member 22 is supported by the transducer case 13. The ultrasonic transducer 21 is attached to the relay transmitting member 22. Inside the holding casing 11, the ultrasonic probe 8 is connected to the distal side of the relay transmitting member 22. In the relay transmitting member 22, a sectional area changing portion 23 is disposed in which a sectional area perpendicular to the longitudinal axis C decreases toward the distal side. The

sectional area changing portion (a horn portion) 23 is positioned on the distal side with respect to the ultrasonic transducer 21. The ultrasonic transducer 21 is connected to one end of each of electric wires 25A and 25B. The electric wires 25A and 25B extend through the inside of the cable 15, and the other end of the wire is connected to the energy control device 3.

The switch is switched to an ON state by the input of the energy operation in the energy operating button 12, whereby in the energy control device 3, the control section controls the conversion circuit, to supply the vibration generating electric power (a vibration generating current) to the ultrasonic vibrator 21 through the electric wires 25A and 25B. Consequently, in the ultrasonic transducer 21, an ultrasonic vibration occurs, and the generated ultrasonic vibration is transmitted to the ultrasonic probe 8 via the relay transmitting member 22. In this case, an amplitude of the ultrasonic vibration is enlarged in the sectional area changing portion 23 of the relay transmitting member 22.

The ultrasonic probe 8 includes a probe main body section 31 extending along the longitudinal axis C. The probe main body section 31 substantially linearly extends along the longitudinal axis C which is an axial center. On the proximal side of the probe main body section 31, an engagement connecting portion 32 is provided. The engagement connecting portion 32 is engaged in an engagement groove (not shown) disposed in the relay transmitting member 22 (e.g., by screwing an external thread into an internal thread), whereby the probe main body section 31 is connected to the distal side of the relay transmitting member 22. Thus, the relay transmitting member 22 is connected to the probe main body section 31, whereby an abutment surface 33 formed at a proximal end of the probe main body section 31 abuts on the relay transmitting member 22. The ultrasonic vibration is transmitted from the relay transmitting member 22 to the probe main body section 31 through the abutment surface 33.

Thus, the ultrasonic vibration is transmitted to the probe main body section 31, whereby in the probe main body section 31 (the ultrasonic probe 8), the ultrasonic vibration is transmitted from the proximal side toward the distal side. In a state where the ultrasonic vibration is transmitted through the probe main body section 31, the vibrating body unit 20 performs a longitudinal vibration in a vibrating direction parallel to the longitudinal axis direction in an established frequency range including an established frequency. In this case, a vibration antinode (the most proximal vibration antinode) A1 that is one of vibration antinodes of the longitudinal vibration is positioned at a proximal end of the vibrating body unit 20 (a proximal end of the relay transmitting member 22), and a vibration antinode (the most distal vibration antinode) A2 that is one of the vibration antinodes of the longitudinal vibration is positioned at a distal end of the vibrating body unit 20 (a distal end of the ultrasonic probe 8). Here, the vibration antinode A1 is positioned most proximally among the vibration antinodes of the longitudinal vibration, and the vibration antinode A2 is positioned most distally among the vibration antinodes of the longitudinal vibration. In a certain example, the vibrating body unit 20 is designed in a state of transmitting the ultrasonic vibration therethrough, thereby performing the longitudinal vibration at 47 kHz (the established frequency), and the vibrating body unit actually longitudinally vibrates in the frequency range (the established frequency range) of 46 kHz or more and 48 kHz or less.

The ultrasonic probe 8 has a total length L1 from its distal end to its proximal end (a proximal end of the engagement

connecting portion 32) in the longitudinal axis direction. In the certain example, it is preferable that the total length L1 is 182.9 mm. Furthermore, the ultrasonic probe 8 has a longitudinal dimension L2 from the distal end to the abutment surface 33 (the proximal end of the probe main body section 31) in the longitudinal axis direction. In the certain example, it is preferable that the longitudinal dimension L2 is 177.5 mm.

In the probe main body section 31, a horn portion (a first horn portion) 35 is disposed. In the horn portion 35, the sectional area perpendicular to the longitudinal axis C decreases toward the distal side. The horn portion (a sectional area decreasing portion) 35 is positioned on the distal side with respect to the abutment surface 33, and the probe main body section 31 has a longitudinal dimension L3 from the abutment surface 33 to a proximal end (a vibration input end) E1 of the horn portion 35 in the longitudinal axis direction. In the certain example, it is preferable that the longitudinal dimension L3 is 29 mm. Furthermore, the horn portion (the first horn portion) 35 has a horn longitudinal dimension (a first horn longitudinal dimension) L4 from the proximal end (the vibration input end) E1 to a distal end (a vibration output end) E2 in the longitudinal axis direction. In the certain example, it is preferable that the horn longitudinal dimension L4 is 20 mm.

An outer diameter of the probe main body section 31 is kept to be substantially constant from the abutment surface 33 to the proximal end E1 of the horn portion 35 in the longitudinal axis direction. Therefore, the probe main body section 31 has an outer diameter D1 in the abutment surface 33 and at the proximal end E1 of the horn portion 35. In the certain example, it is preferable that the outer diameter D1 is 7 mm. Furthermore, in the horn portion 35, a sectional area decreases toward the distal side, and hence at the distal end E2 of the horn portion 35, the probe main body section 31 has an outer diameter D2 smaller than the outer diameter D1. That is, in the horn portion 35, the outer diameter of the probe main body section 31 decreases from the outer diameter D1 to the outer diameter D2 toward the distal side. In the certain example, it is preferable that the outer diameter D2 is 3.8 mm.

In a state where the vibrating body unit 20 longitudinally vibrates in the predetermined frequency range (e.g., 46 kHz or more and 48 kHz or less), a vibration node N1 that is one of vibration nodes of the longitudinal vibration is positioned at the proximal end E1 of the horn portion 35 or in the vicinity of the proximal end E1, and each of the vibration antinodes of the longitudinal vibration is positioned away from the horn portion 35 in the longitudinal axis direction. Consequently, in the horn portion 35 in which the sectional area decreases toward the distal side, the amplitude of the longitudinal vibration (the ultrasonic vibration) is enlarged. In the certain example, the longitudinal vibration in which the amplitude at the vibration antinode is 18 μ m is transmitted to the proximal end E1 of the horn portion 35, and the amplitude of the longitudinal vibration in the horn portion 35 is enlarged. It is to be noted that in a state where the vibrating body unit 20 longitudinally vibrates at the predetermined frequency (e.g., 47 kHz) included in the predetermined frequency range, the vibration node N1 is positioned at the proximal end E1 of the horn portion 35.

In the probe main body section 31, a horn portion (a second horn portion) 36 is provided. In the horn portion 36, the sectional area perpendicular to the longitudinal axis C decreases toward the distal side. The horn portion (a sectional area decreasing portion) 36 is positioned on the distal side from the horn portion (the first horn portion) 35, and the

probe main body section 31 has a longitudinal dimension L5 from the abutment surface 33 to a proximal end (a vibration input end) E3 of the horn portion 36 in the longitudinal axis direction. In the certain example, it is preferable that the longitudinal dimension L5 is 88.1 mm. Furthermore, the horn portion (the second horn portion) 36 has a horn longitudinal dimension (a second horn longitudinal dimension) L6 from the proximal end (the vibration input end) E3 to a distal end (a vibration output end) E4 in the longitudinal axis direction. In the certain example, it is preferable that the horn longitudinal dimension L6 is 14 mm.

In the probe main body section 31, the outer diameter is kept to be substantially constant from the distal end E2 of the horn portion (the first horn portion) 35 to the proximal end E3 of the horn portion (the second horn portion) 36 in the longitudinal axis direction. Therefore, the probe main body section 31 has the outer diameter D2 at the proximal end E3 of the horn portion 36. That is, at the distal end E2 of the horn portion 35 and the proximal end E3 of the horn portion 36, the outer diameter of the probe main body section 31 becomes the outer diameter D2 and has about the same size. Furthermore, in the horn portion 36, the sectional area decreases toward the distal side, and hence at the distal end E4 of the horn portion 36, the probe main body section 31 has an outer diameter D3 that is smaller than the outer diameter D2. That is, in the horn portion 36, the outer diameter of the probe main body section 31 decreases from the outer diameter D2 to the outer diameter D3 toward the distal side. In the certain example, it is preferable that the outer diameter D3 is 2.7 mm.

In the state where the vibrating body unit 20 longitudinally vibrates in the established frequency range (e.g., 46 kHz or more and 48 kHz or less), a vibration node N2 that is one of the vibration nodes of the longitudinal vibration is positioned at the proximal end E3 of the horn portion 36 or in the vicinity of the proximal end E3, and each of the vibration antinodes of the longitudinal vibration is positioned away from the horn portion 36 in the longitudinal axis direction. Consequently, in the horn portion 36 in which the sectional area decreases toward the distal side, the amplitude of the longitudinal vibration (the ultrasonic vibration) is enlarged. It is to be noted that in the state where the vibrating body unit 20 longitudinally vibrates at the established frequency (e.g., 47 kHz) included in the established frequency range, the vibration node N2 is positioned at the proximal end E3 of the horn portion 36. Furthermore, in the state where the vibrating body unit 20 longitudinally vibrates in the predetermined frequency range, the vibration node N2 is positioned on the distal side with respect to the vibration node N1.

In the probe main body section 31, a sectional area increasing portion 37 is provided. In the sectional area increasing portion 37, the sectional area perpendicular to the longitudinal axis C increases toward the distal side. The sectional area increasing portion 37 is positioned on the distal side with respect to the horn portion (the second horn portion) 36, and the probe main body section 31 has a longitudinal dimension L7 from the abutment surface 33 to a distal end (a vibration output end) E6 of the sectional area increasing portion 37 in the longitudinal axis direction. In the certain example, it is preferable that the longitudinal dimension L7 is 116.7 mm. Furthermore, the sectional area increasing portion 37 has an extending dimension L8 from a proximal end (a vibration input end) E5 to the distal end (the vibration output end) E6 in the longitudinal axis direction. The extending dimension L8 is small, and hence in the

sectional area increasing portion 37, a distance from the proximal end E5 to the distal end E6 decreases.

In the probe main body section 31, the outer diameter is kept to be substantially constant from the distal end E4 of the horn portion (the second horn portion) 36 to the proximal end E5 of the sectional area increasing portion 37 in the longitudinal axis direction. Therefore, the probe main body section 31 has the outer diameter D3 at the proximal end E5 of the sectional area increasing portion 37. That is, at the distal end E4 of the horn portion 36 and the proximal end E5 of the sectional area increasing portion 37, the outer diameter of the probe main body section 31 becomes the outer diameter D3 and has about the same size. Furthermore, in the sectional area increasing portion 37, the sectional area increases toward the distal side, and hence at the distal end E6 of the sectional area increasing portion 37, the probe main body section 31 has an outer diameter D4 that is larger than the outer diameter D3. That is, in the sectional area increasing portion 37, the outer diameter of the probe main body section 31 increases from the outer diameter D3 to the outer diameter D4 toward the distal side. In the certain example, the outer diameter D4 is about the same as the outer diameter D2 at the proximal end E3 of the horn portion 36. In this case, it is preferable that the outer diameter D4 is 3.8 mm.

In the state where the vibrating body unit 20 longitudinally vibrates in the established frequency range, a vibration antinode A3 that is one of the vibration antinodes of the longitudinal vibration is positioned in the sectional area increasing portion 37. The vibration antinode A3 at which stress due to the ultrasonic vibration becomes zero is positioned in the sectional area increasing portion 37, and hence, also in the sectional area increasing portion 37 in which the sectional area increases toward the distal side, the amplitude of the longitudinal vibration (the ultrasonic vibration) hardly decreases. It is to be noted that in the state where the vibrating body unit 20 longitudinally vibrates in the established frequency range, the vibration antinode A3 is positioned on the distal side with respect to the vibration node N2, and in the present embodiment, the vibration antinode A3 is positioned second distally among the vibration antinodes of the longitudinal vibration.

The probe main body section 31 includes a supported portion 38 to be supported by the sheath 7 via an elastic member (not shown). The supported portion 38 is positioned on the distal side with respect to the sectional area increasing portion 37. The probe main body section 31 has a longitudinal dimension L9 from the distal end E6 of the sectional area increasing portion 37 to a proximal end E7 of the supported portion 38 in the longitudinal axis direction. In the certain example, it is preferable that the longitudinal dimension L9 is 24.1 mm. Furthermore, the supported portion 38 has an extending dimension L10 from the proximal end E7 to a distal end E8 in the longitudinal axis direction. The extending dimension L10 is small, and in the certain example, it is preferable that the extending dimension L10 is 3 mm.

In the probe main body section 31, the outer diameter is kept to be substantially constant from the distal end E6 of the sectional area increasing portion 37 to the proximal end E7 of the supported portion 38 in the longitudinal axis direction. Therefore, the probe main body section 31 has the outer diameter D4 at the proximal end E7 of the supported portion 38. That is, at the distal end E6 of the sectional area increasing portion 37 and the proximal end E7 of the supported portion 38, the outer diameter of the probe main body section 31 becomes the outer diameter D4 and has

about the same size. In a proximal portion of the supported portion 38, the outer diameter of the probe main body section 31 decreases from the outer diameter D4 to an outer diameter D5. In the certain example, the outer diameter D5 is about 0.4 mm smaller than the outer diameter D4. In the supported portion 38, the outer diameter of the probe main body section 31 is kept to be substantially constant at the outer diameter D5 along a large part in the longitudinal axis direction. Further, in the distal portion of the supported portion 38, the outer diameter of the probe main body section 31 increases from the outer diameter D5 to an outer diameter D6. In consequence, the probe main body section 31 has the outer diameter D6 at the distal end E8 of the supported portion 38. The outer diameter D6 at the distal end E8 of the supported portion 38 is about the same as the outer diameter D4 at the proximal end E7 of the supported portion 38. Consequently, at the proximal end E7 and the distal end E8 of the supported portion 38, the sectional area of the probe main body section 31 which is perpendicular to the longitudinal axis C becomes about the same. In the certain example, it is preferable that the outer diameter D6 is 3.8 mm.

In the state where the vibrating body unit 20 longitudinally vibrates in the established frequency range, a vibration node N3 that is one of the vibration nodes of the longitudinal vibration is positioned in the supported portion 38. Consequently, the probe main body section 31 (the ultrasonic probe 8), which longitudinally vibrates, is also attached to the sheath 7 via the elastic member in the supported portion 38. Furthermore, the probe main body section is supported by the sheath 7 at the vibration node N3 of the longitudinal vibration, and hence in the state where the vibrating body unit 20 longitudinally vibrates in the predetermined frequency range, transmission of the ultrasonic vibration from the supported portion 38 to the sheath 7 is prevented. In the state where the vibrating body unit 20 longitudinally vibrates in the established frequency range, the vibration node (the most distal vibration node) N3 is positioned on the distal side with respect to the vibration node N2, and is positioned most distally among the vibration nodes of the longitudinal vibration. Furthermore, at the proximal end E7 and the distal end E8 of the supported portion 38, the sectional area of the probe main body section 31 which is perpendicular to the longitudinal axis C becomes about the same, and hence in the supported portion 38, the amplitude of the longitudinal vibration hardly changes.

Furthermore, the distal end of the sheath 7 is positioned on the distal side from the distal end E8 of the supported portion 38. Therefore, in the state where the vibrating body unit 20 longitudinally vibrates in the established frequency range, the vibration node N3 positioned most distally among the vibration nodes is positioned inside the sheath 7.

FIG. 3 and FIG. 4 are views showing a constitution of the distal portion of the ultrasonic probe 8. Here, a certain direction that intersects (is substantially perpendicular to) the longitudinal axis C is a first intersecting direction (a direction of an arrow P1 in each of FIG. 2 and FIG. 3), and an opposite direction to the first intersecting direction (a first vertical direction) is a second intersecting direction (a direction of an arrow P2 in each of FIG. 2 and FIG. 3). Furthermore, one of two directions which intersect the longitudinal axis C (substantially perpendicularly) and are perpendicular to (intersect) the first intersecting direction (the first perpendicular direction) and the second intersecting direction (a second perpendicular direction) is a first width direction (a direction of an arrow B1 in FIG. 4). Further, an opposite direction to the first width direction is a second

width direction (a direction of an arrow B2 in FIG. 4). Here, FIG. 2 and FIG. 3 are views of the ultrasonic probe 8 seen from a first width direction side, and FIG. 4 is a view of the ultrasonic probe 8 seen from a second perpendicular direction side. It is to be noted that in FIG. 3, a range shown by a broken line S1 and a broken line S2 projects from the distal end of the sheath 7 toward the distal side.

As shown in FIG. 3 and FIG. 4, the probe main body section 31 extends to a position located on the distal side with respect to the supported portion 38. That is, a distal end E9 of the probe main body section 31 is positioned on the distal side from the distal end E8 of the supported portion 38. However, a distance between the distal end E8 of the supported portion 38 and the distal end E9 of the probe main body section 31 in the longitudinal axis direction is small, and is about 0.6 mm in the certain example.

As described above, in the probe main body section 31, the amplitude of the longitudinal vibration is enlarged in the horn portion (the first horn portion) 35 and the horn portion (the second horn portion) 36, and the amplitude of the longitudinal vibration hardly changes in the sectional area increasing portion 37 and the supported portion 38. Due to the above-mentioned constitution, in the certain example, the longitudinal vibration of an amplitude of 80 μ m occurs at the distal end E9 of the probe main body section 31, in a case where the longitudinal vibration of an amplitude of 18 μ m at the vibration antinode is transmitted to the proximal end (the abutment surface 33) of the probe main body section 31.

A tapered section (a sectional area decreasing portion) 41 is continuous on the distal side of the probe main body section 31. In the tapered section (a third horn portion) 41, a sectional area perpendicular to a longitudinal axis C decreases toward the distal side. A proximal end of the tapered section 41 is continuous with the distal end E9 of the probe main body section 31. Therefore, the distal end E9 of the probe main body section 31 becomes a boundary position between the probe main body section 31 and the tapered section 41. The ultrasonic probe 8 has a longitudinal dimension L11 from the distal end to the proximal end (E9) of the tapered section 41 in the longitudinal axis direction. In the certain example, it is preferable that the longitudinal dimension L11 is 32.5 mm.

The tapered section 41 includes a first narrowed outer surface 51 facing a first intersecting direction side. In the tapered section 41, a distance (a first distance) δ from the longitudinal axis C to the first narrowed outer surface 51 in a first intersecting direction decreases from a proximal side toward the distal side, between the proximal end (E9) and a first narrowing end position (a first distance decreasing end position) E10 in the longitudinal axis direction. The first narrowing end position E10 is positioned on the distal side with respect to the proximal end (E9) of the tapered section 41. Consequently, the tapered section 41 has a first narrowing dimension (a first distance decreasing dimension) L12 between the proximal end (E9) and the first constricting end position E10 in the longitudinal axis direction. In the certain example, it is preferable that the first narrowing dimension L12 is 18 mm. In the present embodiment, the proximal end (E9) of the tapered section 41 becomes a proximal end of the first narrowed outer surface 51, and the first narrowing end position E10 becomes a distal end of the first narrowed outer surface 51.

Furthermore, the tapered section 41 includes a second narrowed outer surface 52 facing the second intersecting direction side. On the tapered section 41, a distance (a second distance) δ' from the longitudinal axis C to the

second narrowed outer surface 52 in a second intersecting direction decreases from the proximal side toward the distal side, between the proximal end (E9) and a second narrowing end position (a second distance decreasing end position) E11 in the longitudinal axis direction. The second narrowing end position E11 is positioned on the distal side with respect to the first narrowing end position E10. Consequently, the tapered section 41 has a second narrowing dimension (a second distancing decrease dimension) L13 that is larger than the first narrowing dimension L12, between the proximal end (E9) and the second narrowing end position E11 in the longitudinal axis direction. In the certain example, it is preferable that the second constricting dimension L13 is 23 mm. In the present embodiment, the proximal end (E9) of the tapered section 41 becomes a proximal end of the second narrowed outer surface 52, and the second narrowing end position E11 becomes a distal end of the second constricted outer surface 52. Consequently, in the tapered section 41, the distal end of the first constricted outer surface 51 (the first constricting end position E10) is positioned on a proximal side as compared with the distal end of the second narrowed outer surface 52 (the second narrowing end position E11), and the distal end of the first narrowed outer surface 51 is disposed away from the distal end of the second narrowed outer surface 52 in the longitudinal axis direction.

Due to the above-mentioned constitution, in the tapered section 41, a thickness (a dimension) T of the ultrasonic probe 8 in the first intersecting direction and the second intersecting direction decreases toward the distal side, between the proximal end (E9) and the second narrowing end position E11 in the longitudinal axis direction. Therefore, the proximal end (E9) of the tapered section 41 becomes a thickness decreasing start position, and the second narrowing end position E11 becomes a thickness decreasing end position. Furthermore, in projection from a first width direction (one side of a width direction), a first narrowing angle $\alpha 1$ that is a narrowing angle (an acute angle) of the first narrowed outer surface 51 relative to the longitudinal axis direction is larger than a second narrowing angle $\alpha 2$ that is a narrowing angle (an acute angle) of the second narrowed outer surface 52 relative to the longitudinal axis direction, and the first narrowing angle is different from the second narrowing angle $\alpha 2$.

Furthermore, the tapered section 41 includes a third narrowed outer surface 53 directed in the first width direction, and a fourth narrowed outer surface 54 facing a second width direction. In the tapered section 41, between a width decreasing start position E12 and a width decreasing end position E13 in the longitudinal axis direction, a distance from the longitudinal axis C to the third narrowed outer surface 53 in the first width direction and a distance from the longitudinal axis C to the fourth narrowed outer surface 54 in the second width direction decrease from the proximal side toward the distal side. Consequently, in the tapered section 41, a width (a dimension) W of the ultrasonic probe 8 in the first width direction and the second width direction decreases toward the distal side, between the width decreasing start position E12 and the width decreasing end position E13 in the longitudinal axis direction. The ultrasonic probe 8 has a longitudinal dimension L14 from the distal end to the width decreasing start position E12 in the longitudinal axis direction. The longitudinal dimension L14 is smaller than the longitudinal dimension L11 from the distal end of the ultrasonic probe 8 to the proximal end (E9) of the tapered section 41 in the longitudinal axis direction. Therefore, the width decreasing start position E12 is positioned on the distal side with respect to the proximal end (E9) of the

tapered section 41. However, the distance between the proximal end (E9) of the tapered section 41 and the width decreasing start position E12 in the longitudinal axis direction is small. In the certain example, it is preferable that the longitudinal dimension L14 is 32 mm. Further, in this example, the distance between the proximal end (E9) of the tapered section 41 and the width decreasing start position E12 in the longitudinal axis direction is about 0.5 mm. In the present embodiment, the width decreasing start position E12 becomes a proximal end of each of the third constricted outer surface 53 and the fourth constricted outer surface 54, and the width decreasing end position E13 becomes a distal end of each of the third narrowed outer surface 53 and the fourth narrowed outer surface 54.

The ultrasonic probe 8 has a longitudinal dimension L15 from the distal end to the width decreasing end position E13 in the longitudinal axis direction. In the present embodiment, the width decreasing end position E13 is positioned on the distal side with respect to the second narrowing end position E11. Further, the width decreasing end position E13 becomes a distal end of the tapered section 41. However, a distance between the second narrowing end position (the distal end of the second narrowed outer surface 52) E11 and the width decreasing end position E13 in the longitudinal axis direction is small. In the certain example, it is preferable that the longitudinal dimension L15 is 9 mm. Further, in this example, the distance between the second narrowing end position E11 and the width decreasing end position E13 in the longitudinal axis direction is about 0.5 mm.

The distance (the first distance) δ from the longitudinal axis C to the first narrowed outer surface 51 (an outer peripheral surface of the ultrasonic probe 8) in the first intersecting direction (a first perpendicular direction) decreases down to a distance $\delta 1$, between the proximal end (E9) of the tapered section 41 and the first narrowing end position E10 in the longitudinal axis direction. Therefore, at the first narrowing end position (the distal end of the first narrowed outer surface 51) E10, the ultrasonic probe 8 has the distance (the first distance) $\delta 1$ from the longitudinal axis C to the first narrowed outer surface 51 toward the first intersecting direction. The distance $\delta 1$ is smaller than a value of $\frac{1}{2}$ of the outer diameter D6 at the distal end E9 of the probe main body section 31. In the certain example, the distance $\delta 1$ is 0.45 mm or more and 0.5 mm or less.

Between the proximal end (E9) of the tapered section 41 and the second narrowing end position E11 in the longitudinal axis direction, the thickness (the dimension) T of the ultrasonic probe 8 in the first intersecting direction and the second intersecting direction decreases down to a thickness T1. Therefore, at the second narrowing end position (the distal end of the second narrowed outer surface 52) E11, the ultrasonic probe 8 has the thickness T1 in the first intersecting direction (the first perpendicular direction) and the second intersecting direction (a second perpendicular direction). The thickness T1 is smaller than the outer diameter D6 at the distal end E9 of the probe main body section 31. In the certain example, it is preferable that the thickness T1 is 1.65 mm.

Between the width decreasing start position E12 and the width decreasing end position E13 in the longitudinal axis direction, the width (the dimension) W of the ultrasonic probe 8 in the first width direction and the second width direction decreases down to a width dimension W1. Therefore, at the width decreasing end position (the distal end of each of the third constricted outer surface 53 and the fourth constricted outer surface 54) E13, the ultrasonic probe 8 has the width dimension W1 in the first width direction and the

second width direction. The width dimension W1 is smaller than the outer diameter D6 at the distal end E9 of the probe main body section 31. In the certain example, it is preferable that the width dimension W1 is 2.8 mm.

The tapered section 41 is constituted as described above, and hence in the tapered section 41, the sectional area perpendicular to the longitudinal axis C decreases toward the distal side. In the state where the vibrating body unit 20 longitudinally vibrates in the established frequency range (e.g., 46 kHz or more and 48 kHz or less), the vibration node (the most distal vibration node) N3 that is one of the vibration nodes of the longitudinal vibration is positioned in the supported portion 38, and is positioned in the vicinity of the proximal end (E9) of the tapered section 41. Further, in the state where the vibrating body unit 20 longitudinally vibrates in the predetermined frequency range, each of the vibration antinodes of the longitudinal vibration is positioned away from the tapered section 41 in the longitudinal axis direction. Consequently, in the tapered section 41 in which the sectional area decreases toward the distal side, the amplitude of the longitudinal vibration (ultrasonic vibration) is enlarged. In the certain example, in a case where the longitudinal vibration in which the amplitude in the tapered section 41 is 80 μm is transmitted, the amplitude of the longitudinal vibration at the distal end of the ultrasonic probe 8 is 140 μm or more and 150 μm or less.

Furthermore, in the present embodiment, a tapering dimension of the tapered section 41 from the proximal end (E9) to the distal end (E13) in the longitudinal axis direction is larger than a $\frac{1}{8}$ wavelength ($\lambda/8$) in the state where the vibrating body unit 20 longitudinally vibrates in the established frequency range. That is, the $\frac{1}{8}$ wavelength ($\lambda/8$) in the state where the vibrating body unit 20 longitudinally vibrates in the established frequency range is smaller than the tapering dimension of the tapered section 41 from the proximal end (E9) to the distal end (E13) in the longitudinal axis direction. In the certain example, in the state where the vibrating body unit 20 longitudinally vibrates at 46 kHz or more and 48 kHz or less (in the established frequency range), a $\frac{1}{4}$ wavelength ($\lambda/4$) from the vibration node (the most distal vibration node) N3 to the vibration antinode (the most distal vibration antinode) A2 is 34 mm or more and 35 mm or less. On the other hand, in this example, the tapering dimension of the tapered section 41 from the proximal end (E9) to the distal end (E13) in the longitudinal axis direction is about 23.5 mm, and is larger than the $\frac{1}{8}$ wavelength in the state where the vibrating body unit 20 longitudinally vibrates at 46 kHz or more and 48 kHz or less (in the predetermined frequency range). Furthermore, in the tapered section 41, the first narrowing dimension L12 between the proximal end (E9) and the first narrowing end position E10 in the longitudinal axis direction is also 17.9 mm or more and 18 mm or less. Therefore, the first narrowing dimension L12 (i.e., the dimension of the first constricted outer surface 51 in the longitudinal axis direction) is also larger than the $\frac{1}{8}$ wavelength in the state where the vibrating body unit 20 longitudinally vibrates at 46 kHz or more and 48 kHz or less (in the established frequency range). It is to be noted that the first narrowing end position E10 is positioned most proximally among the positions (e.g., E10, E11 and E13) at which the narrowing ends on an outer peripheral surface of the tapered section 41 (the narrowed outer surfaces 51 to 54).

In the ultrasonic probe 8, a curved extending section 40 is disposed on the distal side with respect to the tapered section 41 (and the probe main body section 31).

The curved extending section 40 extends in a state of curving relative to the probe main body section 31 and the

tapered section **41** (i.e., the longitudinal axis C) toward the first intersecting direction side. The curved extending section **40** includes a first curved outer surface **55** facing the first intersecting direction side (a side on which the curved extending section **40** curves), and a second curved outer surface **56** directed on the second intersecting direction side (a side opposite to the side on which the curve extending section **40** curves). Furthermore, the curved extending section **40** includes a third curved outer surface **57** facing the first width direction side, and a fourth curved outer surface **58** facing on a second width direction side. It is to be noted that by transmitting the ultrasonic vibration to the curved extending section **40** from the probe main body section **31** through the tapered section **41**, the curved extending section **40** longitudinally vibrates together with the probe main body section **31** and the tapered section **41** in the established frequency range.

In projection from the first width direction (one side of the width direction), in the first curved outer surface **55** of the curved extending section **40**, a region located on the distal side with respect to a first curve start position **E14** curves relative to the longitudinal axis direction (the probe main body section **31**) toward the first intersecting direction side. Furthermore, in the projection from the first width direction, in the second curved outer surface **56** of the curved extending section **40**, a region located on the distal side with respect to a second curve start position **E15** curves relative to the longitudinal axis direction toward the first intersecting direction side. That is, the first curved outer surface **55** starts curving relative to the longitudinal axis C in the first intersecting direction side at the first curve start position **E14**, and the second curved outer surface **56** starts curving relative to the longitudinal axis C toward the first intersecting direction side at the second curve start position **E15**. In the present embodiment, the second curve start position (a proximal end of the second curved outer surface **56**) **E15** is positioned on the distal side with respect to the first curve start position (a proximal end of the first curved outer surface **55**) **E14**, and is positioned away from the first curve start position **E14** in the longitudinal axis direction. Additionally, in the present embodiment, a distance between the first curve start position **E14** and the second curve start position **E15** in the longitudinal axis direction is small, and is about 0.3 mm in the certain example.

The curved extending section **40** extends toward the distal side from the first curve start position **E14** which is the proximal end (a curve proximal end). The ultrasonic probe **8** has a longitudinal dimension **L16** from the distal end to the proximal end (**E14**) of the curved extending section **40** in the longitudinal axis direction. The longitudinal dimension **L16** is smaller than the longitudinal dimension **L15** from the distal end of the ultrasonic probe **8** to the width decreasing end position **E13** in the longitudinal axis direction. Consequently, the proximal end (**E14**) of the curved extending section **40** is positioned on the distal side with respect to the width decreasing end position **E13**. In the certain example, the longitudinal dimension **L16** is 8.4 mm or more and 8.5 mm or less.

Furthermore, in the ultrasonic probe **8**, a relay extending section **43** is continuous between the tapered section **41** and the curved extending section **40** in the longitudinal axis direction. The relay extending section **43** extends from the width decreasing end position **E13** (the distal end of the tapered section **41**) to the first curve start position **E14** (a proximal end of the curved extending section **40**). Here, a distance between the width decreasing end position **E13** and the proximal end (**E14**) of the curved extending section **40**

in the longitudinal axis direction is small. Consequently, a dimension of the relay extending section **43** in the longitudinal axis direction is small. In the certain example, the dimension of the relay extending section **43** in the longitudinal axis direction is about 0.5 mm.

A first axis parallel outer surface **61** directed in the first intersecting direction is continuous between the first narrowed outer surface **51** and the first curved outer surface **55** in the longitudinal axis direction. The first axis parallel outer surface **61** extends in parallel (substantially parallel) with the longitudinal axis C between the first narrowing end position **E10** and the first curve start position **E14**. Therefore, the first constricting end position **E10** becomes a proximal end of the first axis parallel outer surface **61** and the first curve start position **E14** becomes a distal end of the first axis parallel outer surface **61**. Further, the first axis parallel outer surface **61** has an extending dimension (a first extending dimension) **L19** in the longitudinal axis direction. On the first axis parallel outer surface **61**, the distance δ from the longitudinal axis C toward the first intersecting direction is kept to be substantially constant at the distance $\delta 1$, from the first narrowing end position **E10** to the first curve start position **E14**.

Furthermore, a second axis parallel outer surface **62** facing the second intersecting direction is continuous between the second narrowed outer surface **52** and the second curved outer surface **56** in the longitudinal axis direction. The second axis parallel outer surface **62** extends in parallel (substantially parallel) with the longitudinal axis C, between the second narrowing end position **E11** and the second curve start position **E15**. Therefore, the second constricting end position **E11** becomes a proximal end of the second axis parallel outer surface **62**, and the second curve start position **E15** becomes a distal end of the second axis parallel outer surface **62**. Further, the second axis parallel outer surface **62** has an extending dimension (a second extending dimension) **L20** in the longitudinal axis direction. The extending dimension **L19** of the first axis parallel outer surface **61** is larger than the extending dimension **L20** of the second axis parallel outer surface **62**. On the second axis parallel outer surface **62**, the distance δ' from the longitudinal axis C toward the second intersecting direction is kept to be substantially constant from the second narrowing end position **E11** to the second curve start position **E15**.

Due to such a constitution as described above, between the second narrowing end position **E11** and the first curve start position (the proximal end of the curved extending section **40**) **E14** in the longitudinal axis direction, the thickness **T** of the ultrasonic probe **8** in the first intersecting direction and the second intersecting direction is kept to be substantially constant at the thickness **T1**. Furthermore, between the width decreasing end position **E13** and the distal end of the ultrasonic probe **8** in the longitudinal axis direction, the width **W** of the ultrasonic probe **8** in the first width direction and the second width direction is kept to be substantially constant at the width dimension **W1**. Therefore, in the relay extending section **43** extending from the width decreasing end position **E13** to the first curve start position (the proximal end of the curved extending section **40**) **E14**, the dimension becomes substantially constant at the width dimension **W1** and substantially constant at the thickness **T1** along the total length in the longitudinal axis direction. Further, in the relay extending section **43**, the sectional area perpendicular to the longitudinal axis C becomes substantially constant along the total length in the longitudinal axis direction.

Here, there is stipulated a reference plane (a first reference plane) Y1 passing along the longitudinal axis C and perpendicularly (substantially perpendicularly) to the first intersecting direction and the second intersecting direction. In the relay extending section 43, the distance (the first distance) $\delta 1$ from the longitudinal axis C to the first axis parallel outer surface 61 (the outer peripheral surface of the ultrasonic probe 8) toward the first intersecting direction is smaller than a value of $\frac{1}{2}$ of the thickness T1 of the ultrasonic probe 8 in the first intersecting direction and the second intersecting direction. Consequently, in the tapered section 41 and the relay extending section 43, the ultrasonic probe 8 is non-symmetrical about the reference plane Y1 which is a central plane. Further, in the tapered section 41 and the relay extending section 43, a cross section gravity center in the cross section perpendicular to the longitudinal axis C shifts from the longitudinal axis C toward the second intersecting direction side. Especially, between the first narrowing end position E10 and the first curve start position E14, there increases the shift of the cross section gravity center relative to the longitudinal axis C in the second intersecting direction side. Furthermore, there is stipulated a reference plane (a second reference plane) Y2 passing along the longitudinal axis C and perpendicularly (substantially perpendicularly) to the first width direction and the second width direction. In the tapered section 41 and the relay extending section 43, the ultrasonic probe 8 is substantially symmetric about the reference plane Y2 which is a central plane.

The curved extending section 40 includes a first curved extending section 42 that extends from the first curve start position E14 at the proximal end of the curved extending section 40 toward the distal side and curving relative to the probe main body section 31 and the tapered section 41 toward the first intersecting direction side. In the projection from the first width direction (one side of the width direction), in a region of an outer peripheral surface of the first curved extending section 42 which faces the first intersecting direction side, a tangent line at the first curve start position E14 has an acute angle $\theta 1$ relative to the longitudinal axis direction. Furthermore, in the projection from the first width direction, in a region of the outer peripheral surface of the first curved extending section 42 which is directed on the second intersecting direction side, a tangent line at the second curve start position E15 has an acute angle $\theta 2$ relative to the longitudinal axis direction. The acute angle $\theta 1$ and the acute angle $\theta 2$ are larger than 0° and 10° or less. In the certain example, the acute angle $\theta 1$ is 5° , whereas the acute angle $\theta 2$ is 7.5° . Consequently, the acute angle $\theta 2$ is larger than the acute angle $\theta 1$.

In the curved extending section 40, a second curved extending section 45 is continuous with the distal side of the first curved extending section 42. The second curved extending section 45 extends in a state of curving relative to the first curved extending section 42 toward the first intersecting direction side. In the projection from the first width direction (one side of the width direction), a region of an outer peripheral surface of the second curved extending section 45 which faces the first intersecting direction side extends in a circular shape of a curving radius R1. Furthermore, in the projection from the first width direction, a region of the outer peripheral surface of the second curve extending section 45 which is directed on the second intersecting direction side extends in a circular shape of a curving radius R2.

A center O1 of each of the circle of the curving radius R1 and the circle of the curving radius R2 is positioned on the first intersecting direction side with respect to the curved extending section 40 (the ultrasonic probe 8). Consequently,

in the projection from the first width direction (the second width direction), in a region of the outer peripheral surface of the second curved extending section 45 which faces the first intersecting direction side, an acute angle relative to the longitudinal axis direction increases toward the distal side. Similarly, in the projection from the first width direction (the second width direction), in a region of the outer peripheral surface of the second curved extending section 45 which is directed on the second intersecting direction side, an acute angle relative to the longitudinal axis direction increases toward the distal side. Therefore, in the second curved extending section 45, the acute angle relative to the longitudinal axis direction increases toward the distal side.

In the region of the outer peripheral surface of the second curved extending section 45 which faces the first intersecting direction side, a tangent line at a distal end has an acute angle $\theta 3$ relative to the longitudinal axis direction. Furthermore, in the region of the outer peripheral surface of the second curved extending section 45 which faces the second intersecting direction side, a tangent line at a distal end has an acute angle $\theta 4$ relative to the longitudinal axis direction. That is, at a distal end of the first curved outer surface 55, the curved extending section 40 has the acute angle $\theta 3$ relative to the longitudinal axis direction. Further, at a distal end of the second curved outer surface 56, the curved extending section 40 has the acute angle $\theta 4$ relative to the longitudinal axis direction. In the certain example, the curving radius R1 is 15 mm and the acute angle $\theta 3$ is 15° . Furthermore, the acute angle $\theta 4$ is stipulated in accordance with the curving radius R2. For example, in a case where the curving radius R2 is 12.5 mm, the acute angle $\theta 4$ is 25° , and in a case where the curving radius R2 is 16.5 mm, the acute angle $\theta 4$ is 20° . Further, in a case where the curving radius R2 is 30 mm, the acute angle $\theta 4$ is 15° . In the certain example, on the second curved outer surface 56 (the region of the outer peripheral surface of the second curved extending section 45 which faces the second intersecting direction side), the acute angle $\theta 4$ of the tangent line at the distal end relative to the longitudinal axis direction is 10° or more and 30° or less, and more preferably 20° or more and 25° or less.

Furthermore, a direction that is perpendicular (substantially perpendicular) to an extending direction and that is perpendicular (substantially perpendicular) to the width direction in the ultrasonic probe 8 is a thickness direction. In the curved extending section 40, the extending direction of the ultrasonic probe 8 is not parallel to the longitudinal axis, and hence in the curved extending section 40, the thickness direction is not parallel to the first intersecting direction and the second intersecting direction. The ultrasonic probe 8 is kept to be substantially constant at a thickness dimension T2 in the thickness direction from the second curve start position E15 to the distal end in the longitudinal axis direction. That is, between the second curve start position E15 and the distal end of the ultrasonic probe 8, the thickness dimension T2 that is a distance between the first curved outer surface 55 and the second curved outer surface 56 is kept to be substantially constant. In the certain example, the thickness dimension T2 is 1.5 mm. Therefore, the acute angles $\theta 1$ to $\theta 4$ and the curving radii R1 and R2 are determined in a state where the thickness dimension T2 of the ultrasonic probe 8 is substantially constant from the second curve start position E15 to the distal end.

Furthermore, the region of the outer peripheral surface of the second curved extending section 45 which faces the first intersecting direction side has a separation distance T3 from the longitudinal axis C toward the first intersecting direction

at the distal end. In the certain example, it is preferable that the separation distance T3 is 1.9 mm.

The second curved extending section 45 includes a distal surface 46 that forms the distal end of the ultrasonic probe 8. In the projection from the first width direction (one side of the width direction), a portion between the first curved outer surface 55 (the region of the outer peripheral surface of the second curved extending section 45 which is directed on the first intersecting direction side) and the distal surface 46 is formed into a curved surface of a corner radius R3. Furthermore, in the projection from the first width direction, a portion between the second curved outer surface 56 (the region of the outer peripheral surface of the second curved extending section 45 which faces the second intersecting direction side) and the distal surface 46 is formed into a curved surface of a corner radius R4. In the certain example, the corner radius R3 is 0.5 mm and the corner radius R4 is 0.9 mm. Furthermore, in projection from the second intersecting direction (one side of the intersecting direction), there is formed into a curved surface of a corner radius R5 each of a portion between a third curved outer surface 57 (the region of the outer peripheral surface of the second curved extending section 45 which faces the first width direction side) and the distal surface 46 and a portion between a fourth curved outer surface 58 (the region of the outer peripheral surface of the second curved extending section 45 which is directed on the second width direction side) and the distal surface 46.

FIG. 5 is a view of the second curved extending section 45 (a distal portion of the curved extending section 40) seen from a direction of an arrow V of FIG. 3, and is a view of the second curved extending section 45 seen from one side of the thickness direction. Furthermore, FIG. 6 is a view of the second curved extending section 45 seen from the first width direction side. Further, FIG. 7 is a cross-sectional view along the VII-VII line of FIG. 3, and shows a cross section perpendicular to an extending direction of the second curved extending section 45. Here, the direction of the arrow V matches a direction of rotating as much as an acute angle $\theta 5$ from the distal side toward the second intersecting direction side in the projection from the first width direction. The acute angle $\theta 5$ is, for example, 75° .

As shown in FIG. 3 to FIG. 7, cutting surfaces (treating surfaces) 47 to 49 are disposed in the second curved extending section 45. A first cutting surface 47 is disposed on the second curved outer surface 56 (a region of an outer surface of the curved extending section 40 which faces the second intersecting direction side). Further, a second cutting surface 48 is provided on the third curved outer surface 57 (a region of the outer surface of the curved extending section 40 which is directed on the first width direction side), and a third cutting surface 49 is disposed on the fourth curved outer surface 58 (a region of the outer surface of the curved extending section 40 which faces the second width direction side). After-mentioned grooves are formed in each of the abrading surfaces 47 to 49. Furthermore, each of the cutting surfaces 47 to 49 extends from a distal end (the distal surface 46) of the curved extending section 40 toward the proximal side. The first cutting surface 47 is provided in the second curved extending section 45 and on the second curved outer surface 56. Consequently, in the projection from each of the first width direction and the second width direction, the first abrading surface 47 is formed into a circular shape in which the center (O1) is positioned on the first intersecting direction side with respect to the curved extending section 40.

The second curved extending section 45 has a thickness dimension T6 between the first cutting surface 47 and the

first curved outer surface 55 in the thickness direction of the curved extending section 40. The thickness dimension T6 between the first abrading surface 47 and the first curved outer surface 55 is about the same size as the thickness dimension T2. Furthermore, the second curved extending section 45 has a width dimension W5 between the second cutting surface 48 (the third curved outer surface 57) and the third cutting surface 49 (the fourth curved outer surface 58) in the first width direction and the second width direction. The width dimension W5 between the second abrading surface 48 and the third abrading surface 49 is about the same size as the width dimension W1. Consequently, in a range in which the first cutting surface 47 extends (the second curved extending section 45), the thickness dimension T6 (T2) between the first cutting surface 47 and the first curved outer surface 55 in the thickness direction of the curved extending section 40 is smaller than the width dimension W5 (W1) between the third curved outer surface 57 and the fourth curved outer surface 58 in the first width direction and the second width direction.

In the second cutting surface 48, a plurality of (five in the present embodiment) extending grooves (first extending grooves) 63A to 63E are formed. Each of the extending grooves 63A to 63E extends substantially perpendicularly to the extending direction of the curved extending section 40, and extends along the thickness direction of the curved extending section 40 in the present embodiment. Furthermore, the extending grooves 63A to 63E are lined in parallel in the extending direction of the curved extending section 40, and each of the extending grooves 63A to 63E has a space q1 between the extending groove and the adjacent extending groove (corresponding one or two of the grooves 63A to 63E) in the extending direction of the curved extending section 40. Furthermore, the most distal extending groove 63A positioned most distally among the extending grooves 63A to 63E is stipulated. The second curved extending section 45 has an extending dimension L17 from the distal end of the ultrasonic probe 8 to the most distal extending groove 63A in the extending direction of the curved extending section 40. In the certain example, the space q1 is 0.9 mm and the extending dimension L17 is 0.45 mm.

Furthermore, when there is stipulated the reference plane (the second reference plane) Y2 passing along the longitudinal axis C and perpendicularly to the first width direction and the second width direction, a bottom position of each of the extending grooves 63A to 63E is disposed as much as a width direction distance W2 away from the reference plane Y2 in the first width direction. In the certain example, the width direction distance W2 is 1.1 mm. Furthermore, when seen from one side of the thickness direction (a first cutting surface 47 side), each of the extending grooves (the first extending grooves) 63A to 63E has a semicircular shape formed by a semicircular portion of a circle having a diameter $\phi 1$. In the certain example, the diameter $\phi 1$ is 0.5 mm.

In the third cutting surface 49, a plurality of (five in the present embodiment) extending grooves (second extending grooves) 65A to 65E are formed. Each of the extending grooves 65A to 65E is substantially symmetric with the corresponding extending groove (corresponding one of the grooves 63A to 63E) about the reference plane Y2 which is the central plane. Consequently, similarly to the extending grooves (the first extending grooves) 63A to 63E, each of the extending grooves 65A to 65E extends along the thickness direction of the curved extending section 40, and the space q1, the extending dimension L17, the width direction dis-

tance W2 and the diameter $\phi 1$ are stipulated in connection with the extending grooves (the second extending grooves) 65A to 65E.

Furthermore, the first cutting surface 47 is different in extending pattern of the grooves from the second cutting surface 48 and the third cutting surface 49. In the first cutting surface 47, there are formed a plurality of (five in the present embodiment) inclined grooves (first inclined grooves) 66A to 66E and a plurality of (five in the present embodiment) inclined grooves (second inclined grooves) 67A to 67E. Each of the inclined grooves 66A to 66E extends in a state of inclining as much as an acute angle (a first acute angle) $\theta 6$ relative to the extending direction of the curved extending section 40. That is, each of the inclined grooves (the first inclined grooves) 66A to 66E inclines relative to the longitudinal axis direction in projection from the first cutting surface 47 side. Here, in the projection from the first abrading surface 47 side, one side of an extending direction of each of the inclined grooves 66A to 66E matches a direction of rotating as much as the acute angle $\theta 6$ from the proximal side toward the second width direction side. Furthermore, each of the inclined grooves 67A to 67E extends in a state of inclining as much as an acute angle (a second acute angle) $\theta 7$ relative to the extending direction of the curved extending section 40. That is, each of the inclined grooves (the second inclined grooves) 67A to 67E inclines relative to the longitudinal axis direction toward a side opposite to the inclined grooves (the first inclined grooves) 66A to 66E in the projection from the first cutting surface 47 side. Here, in the projection from the first cutting surface 47 side, one side of the extending direction of each of the inclined grooves 67A to 67E matches a direction of rotating as much as the acute angle $\theta 7$ from the proximal side toward the first width direction side. On the first abrading surface 47, each of the inclined grooves 66A to 66E intersects the corresponding inclined groove (corresponding one of the grooves 67A to 67E), and forms a meshed structure (cross-hatch structure). In the certain example, the acute angle (the first acute angle) $\theta 6$ and the acute angle (the second acute angle) $\theta 7$ are 45° or more and 65° or less, and are preferably about 60° .

Each of the inclined grooves (the first inclined grooves) 66A to 66E has a space q2 between the inclined groove and the inclined groove (corresponding two or one of the grooves 66A to 66E) that is adjacent (in a direction perpendicular to the extending direction of the inclined grooves 66A to 66E). Furthermore, there is stipulated the reference inclined groove (a first reference inclined groove) 66C positioned third distally in the inclined grooves 66A to 66E. The second curved extending section 45 has an extending dimension L18 from the distal end of the ultrasonic probe 8 to a distal position of the reference inclined groove 66C in the extending direction of the curved extending section 40. In the certain example, the space q2 is 0.8 mm and the extending dimension L18 is 2.25 mm. Furthermore, each of the inclined grooves 66A to 66E has a depth T4 and a width $\phi 2$. Furthermore, a bottom surface of each of the inclined grooves 66A to 66E seen from a second cutting surface 48 side (one side of the width direction) is formed into a circular shape of a radius $\phi 2/2$. In the certain example, the depth T4 of each of the inclined grooves 66A to 66E is 0.35 mm and the width $\phi 2$ is 0.35 mm.

Each of the inclined grooves (the second inclined grooves) 67A to 67E is substantially symmetric with the corresponding first inclined groove (corresponding one of the grooves 66A to 66E) about the reference plane Y2 which is the central plane. Consequently, similarly to the inclined

grooves 66A to 66E, the space q2, the extending dimension L18, the depth T4 and the width $\phi 2$ are stipulated in connection with the inclined grooves 67A to 67E.

Furthermore, each of the extending grooves (the first extending grooves) 63A to 63E and each of the extending grooves (the second extending grooves) 65A to 65E match a position of an intersecting portion of the corresponding inclined groove (corresponding one of the grooves 66A to 66E) and the corresponding inclined groove (corresponding one of the grooves 67A to 67E) in the longitudinal axis direction. For example, the respective extending grooves 63C and 65C match a position of an intersecting portion of the inclined groove (the first inclined groove) 66C and the inclined groove (the second inclined groove) 67C in the longitudinal axis direction.

In the cross section of the second curved extending section 45 which is perpendicular to the extending direction, there is formed into a curved surface of a corner radius R6 each of a portion between the first curved outer surface 55 (a region of an outer surface which faces the first intersecting direction side) and the second cutting surface 48 and a portion between the first curved outer surface 55 and the third cutting surface 49. Furthermore, in the cross section of the second curved extending section 45 which is perpendicular to the extending direction, there is formed into a curved surface of a corner radius R7 each of a portion between the first cutting surface 47 and the second cutting surface 48 and a portion between the first cutting surface 47 and the third cutting surface 49.

The curved surface portion of the corner radius R6 is formed along the range S1 of FIG. 3 in the longitudinal axis direction, and the curved surface portion of the corner radius R7 is formed along the range S2 of FIG. 3 in the longitudinal axis direction. That is, the curved surface portion of the corner radius R6 and the curved surface portion of the corner radius R7 extend from the distal end of the ultrasonic probe 8 to the tapered section 41 in the longitudinal axis direction, and the curved surface portion of the corner radius R6 and the curved surface portion of the corner radius R7 are formed in a projecting portion (an exposed portion) of the ultrasonic probe 8 from the distal end of the sheath 7. Consequently, in a part of the tapered section 41 and the curved extending section 40, in the cross section perpendicular to the extending direction, there is formed into the curved surface of the corner radius R6 in each of a portion between a region of an outer surface which faces the first intersecting direction side and a region of an outer surface which faces the first width direction side and a portion between the region of the outer surface which faces the first intersecting direction side and a region of the outer surface which faces the second width direction side. Further, in the part of the tapered section 41 and the curved extending section 40, in the cross section perpendicular to the extending direction, there is formed into the curved surface of the corner radius R7 in each of a portion between a region of the outer surface which is directed on the second intersecting direction side and the region of the outer surface which is directed on the first width direction side and a portion between the region of the outer surface which is directed on the second intersecting direction side and the region of the outer surface which is directed on the second width direction side.

Next, a function and an effect of the ultrasonic probe 8 of the present embodiment will be described. FIG. 8 and FIG. 9 are views showing a state where a bone is cut in a shoulder joint 100 by use of an ultrasonic treatment system 1. FIG. 8 is a view of the shoulder joint 100 seen from a front side (a

chest side), and FIG. 9 is a view of the shoulder joint 100 seen from a rear side (a back side). As shown in FIG. 8 and FIG. 9, the shoulder joint 100 is a joint between a humerus 101 and a scapula 102. The scapula 102 includes an acromion 103. The acromion 103 is coupled with a clavicle 105. From the scapula 102, there origin a subscapularis muscle 106, a supraspinatus muscle 107, an infraspinatus muscle 108 and a teres minor muscle 109. On a lower side of the acromion 103, a rotator cuff 111 is formed as a tendon of the subscapularis muscle 106, the supraspinatus muscle 107, the infraspinatus muscle 108 and the teres minor muscle 109. The humerus 101 extends from the rotator cuff 111. Furthermore, a cavity 113 is formed between a lower surface 112 of the acromion 103 and the rotator cuff 111.

In the present embodiment, when cutting a hard tissue such as a bone in a narrow space of a joint cavity or the like, an ultrasonic treatment instrument 2 is used. For example, when performing the cutting in the cavity 113 between the acromion 103 and the rotator cuff 111, a distal portion of a rigid endoscope (an arthroscope) 115 and a distal portion of the ultrasonic probe 8 are inserted into the cavity 113 between the acromion 103 and the rotator cuff 111. Each of the rigid endoscope 115 and the ultrasonic probe 8 is inserted from the outside of a human body into the cavity 113 through one of an insertion area of the front side, an insertion area of a lateral side and an insertion area of the rear side. However, the insertion area of the rigid endoscope 115 is different from the insertion area of the ultrasonic probe 8. In FIG. 8 and FIG. 9, the rigid endoscope 115 is inserted into the cavity 113 from the insertion area of the front side, and the ultrasonic probe 8 is inserted into the cavity 113 through the insertion area of the lateral side. Further, in the cavity 113 under observation with the rigid endoscope 115, one of the cutting surfaces 47 to 49 of the ultrasonic probe 8 is brought into contact with the lower surface 112 of the acromion 103. The ultrasonic vibration is transmitted to the cutting surfaces 47 to 49 in a state where the one of the abrading surfaces 47 to 49 is in contact with the lower surface 112 of the acromion 103, whereby cutting of a bone spur (a bone) is performed in the lower surface 112 of the acromion 103. It is to be noted that the abrading of the bone spur in the lower surface 112 of the acromion 103 is performed in a state where the second curved extending section 45 is immersed in a liquid (physiological saline).

FIG. 10 and FIG. 11 are views showing a state where the first cutting surface 47 of the second curved extending section 45 of the ultrasonic probe 8 is in contact with the lower surface 112 of the acromion 103. In FIG. 11, the first cutting surface 47 is brought into contact with a position different from that of FIG. 10 in the lower surface 112 of the acromion 103. Here, in the ultrasonic probe 8, the first curved extending section 42 curves toward a first perpendicular direction side relative to the probe main body section 31 extending along the longitudinal axis C, and the second curved extending section 45 curves further toward the first perpendicular direction side relative to the first curved extending section 42. Further, in the second curved extending section 45, an acute angle relative to the longitudinal axis direction increases toward the distal side, and in the second curved extending section 45 and the second curved outer surface 56, the first cutting surface 47 is disposed. Consequently, in the present embodiment, in the projection from each of the first width direction and the second width direction, the first cutting surface 47 is formed into the circular shape in which the center (O1) is positioned on the first intersecting direction side with respect to the curved extending section 40. The cavity 113 between the acromion

103 and the rotator cuff 111 is narrow, and the lower surface 112 of the acromion 103 is formed into a curved surface. The first curved extending section 42 and the second curved extending section 45 are formed as described above, so that the first cutting surface 47 can appropriately be brought into contact with the lower surface 112 of the acromion 103 which is formed into the curved surface.

For example, in FIG. 10 and FIG. 11, the positions which come in contact with the first cutting surface 47 are different from each other in the lower surface 112 of the acromion 103, and hence a contact angle of the first abrading surface 47 with the lower surface 112 of the acromion 103 varies. In the present embodiment, the first curved extending section 42 and the second curved extending section 45 are formed as described above, and hence even when the contact angle of the first cutting surface 47 with the lower surface 112 of the acromion 103 changes, it is possible to appropriately bring the first cutting surface 47 into contact with the lower surface 112 of the acromion 103. For example, in each of FIG. 10 and FIG. 11, the first cutting surface 47 appropriately comes in contact with the lower surface 112 of the acromion 103. That is, at any position of the lower surface 112 of the acromion 103 (i.e., even when the contact angle of the first cutting surface 47 with the lower surface 112 of the acromion 103 is any angle), the first cutting surface 47 can appropriately be brought into contact with the lower surface 112 of the acromion 103.

Furthermore, in the present embodiment, the first cutting surface 47 is provided on the second curved outer surface 56 of the curved extending section 40, and on the second curved outer surface 56 (a region of an outer peripheral surface of the curved extending section 40 which faces the second intersecting direction side), the acute angle $\theta 4$ of the tangent line at the distal end relative to the longitudinal axis direction is 10° or more and 30° or less (preferably 20° or more and 25° or less). By setting the acute angle $\theta 4$ to be 10° or more and 30° or less (especially 20° or more and 25° or less), the first cutting surface 47 has a shape corresponding to the lower surface 112 of the acromion 103, and at any position of the lower surface 112 of the acromion 103, the first cutting surface 47 can further easily and appropriately be brought into contact with the lower surface 112 of the acromion 103.

Furthermore, in the first cutting surface 47, each of the inclined grooves (the first inclined grooves) 66A to 66E intersects the corresponding second inclined groove (corresponding one of the grooves 67A to 67E), and the crosshatch structure is formed. The crosshatch structure is formed on the first cutting surface 47, and hence by longitudinally vibrating the second curved extending section 45 by the ultrasonic vibration in a state where the first cutting surface 47 is in contact with the bone, the bone (the bone spur) is appropriately cut. That is, it is possible to appropriately cut the hard bone. Furthermore, in the present embodiment, the acute angle $\theta 6$ of each of the inclined grooves (the first inclined grooves) 66A to 66E relative to the extending direction of the ultrasonic probe 8 (i.e., a vibrating direction by the longitudinal vibration) and the acute angle $\theta 7$ of each of the inclined grooves (the second inclined grooves) 67A to 67E relative to the extending direction of the ultrasonic probe 8 (i.e., the vibrating direction by the longitudinal vibration) are 45° or more and 65° or less. Thus, each of the acute angles $\theta 6$ and $\theta 7$ is in the above-mentioned range, so that cutting properties of the bone improve in a case where the lower surface 112 of the acromion 103 is cut with the first cutting surface 47 by use of the ultrasonic vibration.

As described above, in the present embodiment, also in a joint cavity such as a cavity 113 between an acromion 103

and a rotator cuff 111, i.e., a narrow space, a first cutting surface 47 is easy to come in contact with a hard tissue, and the hard tissue is appropriately cut with the first cutting surface 47. That is, also in the narrow space, it is possible to acquire an accessibility to the hard tissue and cutting properties of the hard tissue.

In the present embodiment, the bone may be cut by bringing the second cutting surface 48 or the third cutting surface 49 into contact with the lower surface 112 of the acromion 103. Furthermore, in a case where the first cutting surface 47 is brought into contact with the lower surface 112 of the acromion 103 to cut the bone (the bone spur), the bone is cut by the second cutting surface 48 and the third cutting surface 49 in the vicinity of an area to be cut by the first cutting surface 47. Thus, the bone is cut by the cutting surface 48 or 49, thereby preventing only the area cut by the first cutting surface 47 from being concaved and preventing a stepped area from being formed on the lower surface 112 of the acromion 103.

Furthermore, the extending grooves 63A to 63E of the second cutting surface 48 and the extending grooves 65A to 65E of the third cutting surface 49 extend substantially perpendicularly (along the thickness direction of the curved extending section 40) to the extending direction of the ultrasonic probe 8 (i.e., the vibrating direction by the longitudinal vibration). The extending grooves (the first extending grooves) 63A to 63E extend substantially perpendicularly to the vibrating direction by the longitudinal vibration, and hence the cutting properties of the bone improve in a case where the bone is cut with the second cutting surface 48 by use of the ultrasonic vibration. Similarly, the extending grooves (the second extending grooves) 65A to 65E extend substantially perpendicularly to the vibrating direction by the longitudinal vibration, and hence the cutting properties of the bone improve in a case where the bone is cut with the third cutting surface 49 by use of the ultrasonic vibration.

Furthermore, each of the extending grooves (the first extending grooves) 63A to 63E and each of the extending grooves (the second extending grooves) 65A to 65E match in a position of an intersecting portion of the corresponding inclined groove (corresponding one of the grooves 66A to 66E) and the corresponding inclined groove (corresponding one of the grooves 67A to 67E) in the longitudinal axis direction. The extending grooves 63A to 63E and 65A to 65E and the inclined grooves 66A to 66E and 67A to 67E are arranged as described above, so that when the bone is cut with the cutting surfaces 47 to 49, the bone is evenly and uniformly cut and the cutting properties further improve.

Furthermore, in the present embodiment, the distal end of the first narrowed outer surface 51 (the first narrowing end position E10) is positioned on the proximal side with respect to the distal end of the second narrowed outer surface 52 (the second narrowing end position E11), and the extending dimension L19 of the first axis parallel outer surface 61 is larger than the extending dimension L20 of the second axis parallel outer surface 62. Consequently, in a case where the first cutting surface 47 moves to a position to be contactable with the lower surface 112 of the acromion 103, the region of the outer surface which faces the first intersecting direction side (the back-surface-side region) in the curved extending section 40, the tapered section 41 and the relay extending section 43 is hard to come in contact with a biological tissue or the like other than a treated target (the lower surface of the acromion 103). Therefore, the first cutting surface 47 is easily movable to the position at which the surface can come in contact with the lower surface 112 of the acromion 103.

FIG. 12 shows the amplitude V of the longitudinal vibration and stress σ due to the ultrasonic vibration, between the second distal vibration antinode A3 and the most distal vibration antinode A2 in a state where the vibrating body unit 20 longitudinally vibrates in the established frequency range. In FIG. 12, an abscissa shows a position in a longitudinal axis direction and an ordinate shows the amplitude V and the stress σ . Furthermore, in FIG. 12, a solid line shows change of the amplitude V of the longitudinal vibration and a one-dot chain line shows change of the stress σ .

As shown in FIG. 12, in the state where the vibrating body unit 20 longitudinally vibrates in the established frequency range, the tapered section 41 is positioned on the distal side with respect to the most distal side vibration node N3, and an amplitude V of the longitudinal vibration is enlarged in the tapered section 41. For example, the longitudinal vibration in which the amplitude at the vibration antinode is 80 μm is enlarged to the longitudinal vibration in which the amplitude at the vibration antinode is 140 μm or more and 150 μm or less by the tapered section 41. Furthermore, stress σ due to the ultrasonic vibration increases at the vibration node and in a portion in which a sectional area perpendicular to a transmitting direction of the ultrasonic vibration decreases, and the stress becomes zero at the vibration antinode. Therefore, as shown in FIG. 12, the stress σ increases between the vibration node N3 and the distal end (E13) of the tapered section 41.

Here, in the present embodiment, the dimension of the tapered section 41 from the proximal end (E9) to the distal end (E13) in the longitudinal axis direction is larger than the $\frac{1}{8}$ wavelength ($\lambda/8$) in the state where the vibrating body unit 20 longitudinally vibrates in the established frequency range. Further, in the tapered section 41, the first narrowing dimension L12 between the proximal end (E9) and the first narrowing end position E10 in the longitudinal axis direction is also larger than the $\frac{1}{8}$ wavelength in the state where the vibrating body unit 20 longitudinally vibrates in the established frequency range. The dimension of the tapered section 41 from the proximal end (E9) to the distal end (E13) in the longitudinal axis direction increases, so that the stress σ due to the ultrasonic vibration is kept to be substantially constant along the total length between the vibration node N3 and the distal end (E13) of the tapered section 41. That is, between the vibration node N3 and the distal end (E13) of the tapered section 41, the stress is effectively prevented from locally increasing (i.e., generation of a peak is prevented). For example, in the certain example, even when the longitudinal vibration in which the amplitude at the vibration antinode increases (e.g., 80 μm) is transmitted to the proximal end (E9) of the tapered section 41, the stress σ is kept to be substantially uniform at about 300 MPa between the vibration node N3 and the distal end (E13) of the tapered section 41 in the state where the vibrating body unit 20 longitudinally vibrates in the established frequency range (e.g., 46 kHz or more and 48 kHz or less). That is, in the present embodiment, the stress is prevented from locally increasing to about 700 MPa (e.g., at the distal end (E13) of the tapered section 41) between the vibration node N3 and the distal end (E13) of the tapered section 41. The stress σ is prevented from locally increasing, and hence breakage of the ultrasonic probe 8 due to the ultrasonic vibration can effectively be prevented.

Furthermore, in the present embodiment, the cross section gravity center in the cross section perpendicular to the longitudinal axis C shifts from the longitudinal axis C toward the second intersecting direction side in the tapered section 41 and the relay extending section 43. Especially,

between the first narrowing end position E10 and the first curve start position (the curve proximal end) E14, there increases the shift of the cross section gravity center relative to the longitudinal axis C on the second intersecting direction side. Consequently, in the present embodiment, shift of the center of gravity onto the first intersecting direction side which is caused by the curve of the curved extending section 40 relative to the longitudinal axis direction is canceled by the shift of the center of gravity onto the second intersecting direction side which is caused by the tapered section 41 and the relay extending section 43. Consequently, in the state where the ultrasonic vibration of the ultrasonic probe 8 is transmitted toward the distal side, it is possible to decrease generation of irregular vibration (transverse vibration or torsional vibration) except the longitudinal vibration.

In the present embodiment, in the projection from the first width direction (one side of the width direction), the portion between the first curved outer surface 55 and the distal surface 46 is formed into the curved surface of the corner radius R3. Furthermore, in the projection from the first width direction, the portion between the second curved outer surface 56 and the distal surface 46 is formed into the curved surface of the corner radius R4. Further, in the projection from the second intersecting direction (one side of the intersecting direction), each of the portion between the third curved outer surface 57 and the distal surface 46 and the portion between the fourth curved outer surface 58 and the distal surface 46 is formed into the curved surface of the corner radius R5. Consequently, on the distal surface 46 of the ultrasonic probe 8, there decreases a ratio of the surface (the outer surface) perpendicular to the extending direction of the ultrasonic probe 8 (i.e., the vibrating direction of the longitudinal vibration). The ratio of the surface perpendicular to the vibrating direction of the longitudinal vibration decreases, so that even when the ultrasonic probe 8 longitudinally vibrates in the state where the second curved extending section 45 is immersed into the liquid (physiological saline), generation of cavitation in the vicinity of the distal surface 46 is decreased. Due to the decrease of the generation of the cavitation, visibility of an operator in a treatment improves.

Furthermore, in the projecting portion (the exposed portion) of the ultrasonic probe 8 from the distal end of the sheath 7, in the cross section perpendicular to the extending direction, there is formed into the curved surface of the corner radius R6 in each of the portion between the region of the outer surface which faces the first intersecting direction side and the region of the outer surface which faces the first width direction side and the portion between the region of the outer surface which faces the first intersecting direction side and the region of the outer surface which faces the second width direction side. Further, in the projecting portion (the exposed portion) of the ultrasonic probe 8 from the distal end of the sheath 7, in the cross section perpendicular to the extending direction, there is formed into the curved surface of the corner radius R7 in each of the portion between the region of the outer surface which faces the second intersecting direction side and the region of the outer surface which faces the first width direction side and the portion between the region of the outer surface which faces the second intersecting direction side and the region of the outer surface which faces the second width direction side. Consequently, on the outer peripheral surface of the tapered section 41, the relay extending section 43 and the curve extending section 40, any edges are not formed. Therefore, even when the projecting portion (the exposed portion) of the ultrasonic probe 8 from the distal end of the sheath 7

comes in contact with the biological tissue or the like other than the treated target, it is possible to effectively prevent damages on the biological tissue.

(Modification)

Additionally, according to a certain modification, on a second cutting surface 48, extending grooves (first extending grooves) 63A to 63E may extend in a state of being perpendicular to a circular first cutting surface 47, and on a third cutting surface 49, extending grooves (second extending grooves) 65A to 65E may extend in a state of being perpendicular to the circular first cutting surface 47. In this modification, when cutting a bone with the second cutting surface 48 or the third cutting surface 49, it is possible to improve cutting properties of the bone.

Furthermore, according to another modification, a first curve start position E14 of a first curved outer surface 55 may be positioned on a distal side with respect to a second curve start position E15 of a second curved outer surface 56. In this modification, when a first cutting surface 47 moves to a position to be contactable with a lower surface 112 of an acromion 103, in a curved extending section 40 and a tapered section 41, a region of the outer surface which is directed on a first intersecting direction side is harder to come in contact with a biological tissue or the like other than a treated target (the lower surface of the acromion 103). Therefore, the first cutting surface 47 is further easily movable to the position to be contactable with the lower surface 112 of the acromion 103.

In the above-mentioned embodiments or the like, the ultrasonic probe (8) includes the probe main body section (31) which is extended along a longitudinal axis (C), and which is configured to transmit the ultrasonic vibration from a proximal side toward a distal side, and a curved extending section (40) which is provided on the distal side with respect to the probe main body section (31), and which is extended in a state of curving relative to the probe main body section toward a first intersecting direction side in a case where a certain direction intersecting the longitudinal axis (C) is defined as the first intersecting direction (P1). The curved extending section (40) includes a first curved outer surface (55) which faces the first intersecting direction side, a second curved outer surface (57) which faces a second intersecting direction (P2) side in a case where an opposite direction of the first intersecting direction (P1) is defined as the second intersecting direction (P2), a third curved outer surface (57) which faces a first width direction (B1) side in a case where two directions which intersect the longitudinal axis (C) and are perpendicular to the first intersecting direction (P1) and the second intersecting direction (P2) are defined as a first width direction (B1) and a second width direction (B2), and a fourth curved outer surface (58) which faces a second width direction (B2) side. The first cutting surface (47) formed on the second curved outer surface (56) is different from a second cutting surface (48) formed on the third curved outer surface (57) and a third cutting surface (49) formed on the fourth curved outer surface (58) in extending pattern of the grooves.

Additional advantages and modifications will readily occur to those skilled in the art. Therefore, the invention in its broader aspects is not limited to the specific details and representative embodiments shown and described herein. Accordingly, various modifications may be made without departing from the spirit or scope of the general inventive concept as defined by the appended claims and their equivalents.

What is claimed is:

1. An ultrasonic probe used in a joint, the ultrasonic probe being configured to transmit an ultrasonic vibration so as to treat a treated target in a joint cavity by use of the ultrasonic vibration, the ultrasonic probe comprising:
 - a probe main body section which extends along a straight longitudinal axis of the probe, and which is configured to transmit the ultrasonic vibration from a proximal side of the probe toward a distal side of the probe;
 - a curved extending section which is provided on the distal side of the probe main body section, and which extends by curving relative to the longitudinal axis toward one side of the probe in a thickness direction thereof, the thickness direction being transverse to the longitudinal axis,
 - the curved extending section including:
 - a first curved outer surface facing a side of the probe toward which the curved extending section curves relative to the longitudinal axis in the thickness direction;
 - a second curved outer surface facing a side of the probe opposite to the first curved outer surface in the thickness direction;
 - a third curved outer surface facing one side of the probe in a width direction transverse to the longitudinal axis and transverse to the thickness direction;
 - a fourth curved outer surface facing a side of the probe opposite to the third curved outer surface in the width direction;
 - a first cutting surface which forms grooves on the second curved outer surface, and which is configured to cut the treated target;
 - a second cutting surface which forms grooves on the third curved outer surface, and which is configured to cut the treated target, an extending pattern of the grooves in the second cutting surface being different from an extending pattern of the grooves in the first cutting surface; and
 - a third cutting surface which forms grooves on the fourth curved outer surface, and which is configured to cut the treated target, the extending pattern of the grooves in the third cutting surface being different from the extending pattern of the grooves in the first cutting surface;
 - a first narrowed outer surface facing the side toward which the curved extending section curves relative to the longitudinal axis in the thickness direction, the first narrowed outer surface being provided between the probe main body section and the first curved outer surface in a longitudinal axis direction, which is a direction along the longitudinal axis, a distance from the longitudinal axis to the first narrowed outer surface decreasing from the proximal side thereof toward the distal side thereof;
 - a second narrowed outer surface facing a side of the probe opposite to the first narrowed outer surface in the thickness direction, the second narrowed outer surface being provided between the probe main body section and the second curved outer surface in the longitudinal axis direction, a distance from the longitudinal axis to the second narrowed outer surface decreasing from the proximal side thereof toward the distal side thereof;
 - a first axis parallel outer surface facing the side of the probe toward which the curved extending section curves relative to the longitudinal axis in the thickness direction, the first axis parallel outer surface being continuous between the first narrowed outer surface

- and the first curved outer surface in the longitudinal axis direction, the first axis parallel outer surface extending parallel with the longitudinal axis, a distance from the longitudinal axis to the first axis parallel outer surface being constant in a region between a proximal end of the first axis parallel outer surface and a distal end of the first axis parallel outer surface in the longitudinal axis direction; and
 - a second axis parallel outer surface facing a side of the probe opposite to the first axis parallel outer surface in the thickness direction, the second axis parallel outer surface being continuous between the second narrowed outer surface and the second curved outer surface in the longitudinal axis direction, the second axis parallel outer surface extending parallel with the longitudinal axis, a distance from the longitudinal axis to the second axis parallel outer surface being constant in a region between a proximal end of the second axis parallel outer surface and a distal end of the second axis parallel outer surface in the longitudinal axis direction.
2. The ultrasonic probe of claim 1, wherein the first cutting surface includes first inclined grooves which incline relative to the longitudinal axis direction in projection from a first cutting surface side, and second inclined grooves which incline toward a side opposite to the first inclined grooves relative to the longitudinal axis direction in the projection from the first cutting surface side and which intersect the first inclined grooves so as to form a crosshatch structure, the second cutting surface includes first extending grooves extended along the thickness direction, and the third cutting surface includes second extending grooves extended along the thickness direction.
 3. The ultrasonic probe of claim 2, wherein the first extending groove and the second extending groove match in a position of an intersecting portion of the first inclined groove and the second inclined groove in the longitudinal axis direction.
 4. The ultrasonic probe of claim 2, wherein the first inclined grooves incline at an acute angle in a range between 45° and 65° relative to the longitudinal axis direction in the projection from the first cutting surface side, and the second inclined grooves incline at an acute angle in a range between 45° and 65° relative to the longitudinal axis direction toward a side opposite to the first inclined grooves in the projection from the first cutting surface side.
 5. The ultrasonic probe of claim 1, wherein an acute angle of a tangent line at a distal end of the second curved outer surface relative to a longitudinal axis direction is an acute angle in a range between 20° and 25°.
 6. The ultrasonic probe of claim 1, wherein the curved extending section includes:
 - a first curved extending section extending from a proximal end of the curved extending section toward a distal side of the first curved extending section; and
 - a second curved extending section which is continuous with the distal side of the first curved extending section, an acute angle relative to the longitudinal axis direction in the second curved extending section increasing toward the distal side.
 7. The ultrasonic probe of claim 6, wherein the first cutting surface, the second cutting surface and the third cutting surface are provided in the second curved extending section.

8. The ultrasonic probe of claim 1,
wherein in projection from each of both sides of the width
direction, the first cutting surface is formed into a
circular shape, a center of the circular shape being
positioned on the side of the probe toward which the
curved extending section curves relative to the longi-
tudinal axis with respect to the curved extending sec-
tion in the thickness direction.
9. The ultrasonic probe of claim 8,
wherein the second cutting surface includes first extend-
ing grooves which are perpendicular to the circular first
cutting surface in the projection from a second cutting
surface side of the probe, and
the third cutting surface includes second extending
grooves which are perpendicular to the circular first
cutting surface in the projection from a third cutting
surface side of the probe.
10. The ultrasonic probe of claim 1,
wherein in a range in which the first cutting surface
extends, a dimension between the first cutting surface
and the first curved outer surface in the thickness
direction is smaller than a dimension between the third
curved outer surface and the fourth curved outer sur-
face in the width direction.
11. The ultrasonic probe of claim 1,
wherein a first curve start position at which the first
curved outer surface starts curving relative to the
longitudinal axis is positioned on the distal side of a
second curve start position at which the second curved
outer surface starts curving relative to the longitudinal
axis.
12. The ultrasonic probe of claim 1,
wherein the probe main body section and the curved
extending section are configured to vibrate in an estab-
lished frequency range in a state where the ultrasonic
vibration is transmitted from the probe main body
section to the curved extending section, and
in a state where the probe main body section and the
curved extending section vibrate in the established
frequency range, a most distal vibration node posi-
tioned most distally among vibration nodes is posi-
tioned on the proximal side with respect to a proximal
end of the curved extending section.
13. The ultrasonic probe of claim 12, further comprising:
a tapered section which is provided between the probe
main body section and the curved extending section in
the longitudinal axis direction, and in which a sectional
area perpendicular to the longitudinal axis decreases
from the proximal side toward the distal side, the
tapered section being configured to vibrate together
with the probe main body section and the curved
extending section in the established frequency range in
the state where the ultrasonic vibration is transmitted
from the probe main body section to curved extending
section,
wherein in the state where the probe main body section,
the curved extending section and the tapered section
vibrate in the established frequency range, the most
distal vibration node is positioned on the proximal side
with respect to a proximal end of the tapered section,
and a $\frac{1}{8}$ wavelength of the vibration is smaller than a
taper dimension from the proximal end of the tapered
section to a distal end of the tapered section in the
longitudinal axis direction.
14. The ultrasonic probe of claim 1,
wherein a first extending dimension of the first axis
parallel outer surface in the longitudinal axis direction

- is larger than a second extending dimension of the
second axis parallel outer surface in the longitudinal
axis direction.
15. The ultrasonic probe of claim 1,
wherein a first narrowing angle of the first narrowed outer
surface relative to the longitudinal axis direction is
larger than a second narrowing angle of the second
narrowed outer surface relative to the longitudinal axis
direction.
16. The ultrasonic probe of claim 1,
wherein a distal end of the first narrowed outer surface is
positioned on the proximal side of a distal end of the
second narrowed outer surface.
17. An ultrasonic probe used in a joint, the ultrasonic
probe being configured to transmit an ultrasonic vibration so
as to treat a treated target in a joint cavity by use of the
ultrasonic vibration, the ultrasonic probe comprising:
a probe main body section which extends along a straight
longitudinal axis of the probe, and which is configured
to transmit the ultrasonic vibration from a proximal
side of the probe toward a distal side of the probe;
a curved extending section which is provided on the distal
side of the probe main body section, and which extends
by curving relative to the longitudinal axis toward one
side of the probe in a thickness direction thereof, the
thickness direction being transverse to the longitudinal
axis,
the curved extending section including:
a first curved outer surface facing a side of the probe
toward which the curved extending section curves
relative to the longitudinal axis in the thickness
direction,
a second curved outer surface facing a side of the probe
opposite to the first curved outer surface in the
thickness direction,
a third curved outer surface facing one side of the probe
in a width direction transverse to the longitudinal
axis and transverse to the thickness direction,
a fourth curved outer surface facing a side of the probe
opposite to the third curved outer surface in the
width direction,
a first cutting surface which forms grooves on the
second curved outer surface, and which is configured
to cut the treated target,
a second cutting surface which forms grooves on the
third curved outer surface, and which is configured
to cut the treated target, an extending pattern of the
grooves of the second cutting surface being different
from an extending pattern of the grooves of the first
cutting surface, and
a third cutting surface which forms grooves on the
fourth curved outer surface, and which is configured
to cut the treated target, an extending pattern of the
grooves of the third cutting surface being different
from an extending pattern of the grooves of the first
cutting surface;
a first narrowed outer surface facing the side toward
which the curved extending section curves relative to
the longitudinal axis in the thickness direction, the first
narrowed outer surface being provided between the
probe main body section and the first curved outer
surface in a longitudinal axis direction, which is a
direction along the longitudinal axis, a distance from
the longitudinal axis to the first narrowed outer surface
decreasing from the proximal side thereof toward the
distal side thereof;

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a second narrowed outer surface facing a side of the probe opposite to the first narrowed outer surface in the thickness direction, the second narrowed outer surface being provided between the probe main body section and the second curved outer surface in the longitudinal axis direction, a distance from the longitudinal axis to the second narrowed outer surface decreasing from the proximal side thereof toward the distal side thereof;

a third narrowed outer surface facing a side of the probe toward which the third curved outer surface faces in the width direction, the third narrowed outer surface being provided between the probe main body section and the third curved outer surface in the longitudinal axis direction, a distance from the longitudinal axis to the third narrowed outer surface decreasing from the proximal side thereof toward the distal side thereof; and

a fourth narrowed outer surface facing a side of the probe opposite to the third narrowed outer surface in the width direction, the fourth narrowed outer surface being provided between the probe main body section and the fourth curved outer surface in the longitudinal axis direction, a distance from the longitudinal axis to the fourth narrowed outer surface decreasing from the proximal side thereof toward the distal side thereof.

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摘要(译)

用于肩关节的超声探头包括弯曲延伸部分，该弯曲延伸部分朝向与纵轴相交的第一交叉方向弯曲到探头主体。弯曲延伸部分包括面向第一交叉方向的第一弯曲外表面，面向与第一交叉方向相反的第二交叉方向的第二弯曲外表面，面向垂直于第一和第二交叉的第一宽度方向的第三弯曲外表面第四弯曲外表面面向与第一宽度方向相反的第二宽度方向。第二弯曲外表面上的切割表面与凹槽的延伸图案中的第三弯曲外表面和第四弯曲外表面中的每一个上的切割表面不同。

