

(19)



(11)

EP 3 055 020 B1

(12)

EUROPEAN PATENT SPECIFICATION

(45) Date of publication and mention
of the grant of the patent:

20.03.2019 Bulletin 2019/12

(51) Int Cl.:

A61B 18/18 ^(2006.01) **A61B 18/00** ^(2006.01)

(86) International application number:

PCT/GB2014/053015

(21) Application number: **14784349.4**

(22) Date of filing: **07.10.2014**

(87) International publication number:

WO 2015/052502 (16.04.2015 Gazette 2015/15)

**(54) ELECTROSURGICAL FORCEPS FOR DELIVERING MICROWAVE ENERGY FROM A
NON-RESONANT UNBALANCED LOSSY TRANSMISSION LINE STRUCTURE**

ELEKTROCHIRURGISCHE ZANGE ZUR MIKROWELLENENERGIESPEISUNG AUS EINER
UNSYMMETRISCHEN NICHTRESONANTEN VERLUSTBEHAFTETEN
ÜBERTRAGUNGSLEITUNGSSTRUKTUR

PINCE ÉLECTROCHIRURGICALE POUR DÉLIVRER UNE ÉNERGIE MICRO-ONDE D'UNE
STRUCTURE DE LIGNE DE TRANSMISSION À PERTE, NON ÉQUILBRÉE, NON RÉSONANTE

(84) Designated Contracting States:

**AL AT BE BG CH CY CZ DE DK EE ES FI FR GB
GR HR HU IE IS IT LI LT LU LV MC MK MT NL NO
PL PT RO RS SE SI SK SM TR**

(30) Priority: **07.10.2013 GB 201317713**

(43) Date of publication of application:

17.08.2016 Bulletin 2016/33

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WO-A2-03/020339 US-A1- 2012 143 180

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EP 3 055 020 B1

DescriptionFIELD OF THE INVENTION

[0001] The invention relates to electrosurgical forceps for grasping biological tissue and for delivering microwave frequency energy into the grasped tissue to coagulate or cauterise or seal the tissue. In particular, the forceps may be used to seal blood vessels. The forceps may be inserted down the instrument channel of an endoscope or a gastroscope, or may be used in laparoscopic surgery or open surgery.

BACKGROUND TO THE INVENTION

[0002] Forceps capable of delivering heat energy into grasped biological tissue are known. The heat energy may cauterise the grasped tissue and facilitate coagulation or vessel sealing.

[0003] US 6,585,735 describes an endoscopic bipolar forceps in which the jaws of the forceps are arranged to conduct bipolar energy through the tissue held therebetween.

[0004] EP 2 233 098 describes microwave forceps for sealing tissue in which the sealing surfaces of the jaws include one or more microwave antennas for radiating microwave frequency energy into tissue grasped between the jaws of the forceps.

[0005] WO 03/020339 A2 fails to disclose a non-resonant transmission line, as set out in present claims 1 and 5.

SUMMARY OF THE INVENTION

[0006] At its most general, the present invention provides electrosurgical forceps in which microwave energy is delivered into biological tissue from a non-resonant unbalanced lossy transmission line structure located within or formed by the jaws of the forceps. The forceps may be used endoscopically in the gastrointestinal tract or laparoscopically or in open surgery.

[0007] According to a first aspect of the invention, there is provided an electrosurgical forceps according to claim 1.

[0008] Herein the term "non-resonant" may mean that the electrical length of the transmission line (along the microwave energy travelling wave) is set to inhibit multiple reflections of the travelling wave, i.e. to prevent or inhibit the creation of a radiating standing wave. In practice this may mean that the electrical length of the transmission line is substantially different from a multiple of a quarter wavelength of the microwave energy (an odd or even multiple needs to be avoided depending on whether the distal end of the transmission line is an open circuit or a short circuit). It is particularly desirable for the transmission line to be non-resonant when there is biological tissue in the gap, i.e. in contact with the jaw elements. Thus, the electrical length of the transmission line may be set to avoid a multiple of a quarter wavelength of the microwave energy when the transmission line is loaded by the biological tissue in this way. Preferably the distal end of the transmission line is an open circuit, as this may enable the device to operate with radiofrequency (RF) energy as well as microwave energy.

[0009] Forming a non-resonant transmission line may prevent the device from radiating. The microwave energy is therefore delivered into tissue through leakage from the transmission line structure. By setting the length of the transmission line with knowledge of the loss level into biological tissue at the frequency of the microwave energy, the electrosurgical forceps of the invention can be arranged to deliver substantially all of the power received at the proximal end of the transmission line in a single transit of the travelling wave along the transmission line.

[0010] In other words, the geometry of the transmission line is selected, e.g. on the basis of simulations or the like, such that it exhibits high loss in biological tissue at the frequency of the microwave energy. Similarly, the geometry of the transmission line may ensure that much less power is lost when there is no tissue in the gap, but air instead. For example, the device may exhibit about 1 dB return loss, i.e. 80% of power reflected back to the generator, compared to 20% when there is tissue there. Thus, four times as much power can be delivered when tissue is present in the gap. Biological tissue is lossy, i.e. it is a good absorber of microwave energy.

[0011] The magnitude of the electric field produced by the forceps of the invention may be considerably lower than that produced by conventional bipolar RF forceps. The microwave frequency electric field used in the invention damages tissue in a fundamentally different way from RF energy, i.e. by denaturing tissue rather than cell rupture. The potential for accidental localised extreme damage is therefore much smaller than with RF devices that may generate a plasma or arc and burn. Moreover, the peak voltage required to produce effective dielectric heating with microwave energy may be less than 50 V, which is a factor of 10 lower than required for bipolar RF devices and a factor of 100 less than that required for monopolar RF devices. In the latter, the path for the RF current to flow is through the body via a return plate placed on the surface of the patient's skin. This presents a risk to the patient in terms of the high voltage requirement and also lack of control due to the current always wanting to take the path of least resistance. It could also cause an explosion to occur within the body due to a build-up of gases being ignited due to a spark, arc, micro plasma or breakdown

occurring because of the high voltage levels associated with monopolar RF energy, e.g. 4,500 V peak, or bipolar RF energy, e.g. 500 V peak or greater. The high voltages associated with bipolar or monopolar RF instruments present as risk of explosion. In comparison, voltages associated with microwave coagulation may be between 5 V and 70 V peak. The device is therefore safer for the patient when in use in the environment found inside the patient's body.

[0012] The magnitude of the field may be controlled e.g. by controlling the power delivered to the forceps based on the size of the gap. This control may permit the magnitude of the electric field to be independent of the size of the vessel or the thickness of the tissue located in the gap. This may present an advantage over conventional bipolar RF forceps.

[0013] Herein, "microwave frequency" may be used broadly to indicate a frequency range of 400 MHz to 100 GHz, but preferably the range 1 GHz to 60 GHz, more preferably 2.45 GHz to 30 GHz or 5 GHz to 30 GHz. Specific frequencies that have been considered are: 915 MHz, 2.45 GHz, 3.3 GHz, 5.8 GHz, 10 GHz, 14.5 GHz and 24 GHz.

[0014] The electrosurgical forceps of the invention may be configured for insertion down an instrument channel of an endoscope, or may be arranged for use in laparoscopic surgery or in a NOTES procedure or in a general open procedure.

[0015] Herein, the term "non-uniform" transmission line is used to designate an arrangement in which the conductive elements on opposing surfaces of the jaws are not in a uniform spatial relationship with each other along the length of the pair of jaw elements. For example, the conductive elements may comprise a first conductive plate mounted in one of the pair of jaw elements and a second conductive plate mounted in the other one of the pair of jaw elements, wherein the signal transition portion is arranged to connect the first conductive plate to an outer conductor of the coaxial cable and to connect the second conductive plate to an inner conductor of the coaxial cable. The conductive plates may each include a flat surface at or aligned with the surface of one of the jaw elements facing into the gap. This configuration may ensure an optimal power density in the gap between the plates, to ensure that the energy is delivered into biological tissue present in the gap.

[0016] The transmission line may form a parallel transmission line or parallel plate transmission line when the opposing surfaces of the conductive plates are parallel. However, this is not essential. Over a wide range of angles between the jaws, e.g. $\pm 20^\circ$ or more, the power will travel up between the jaws. The jaws might not be parallel for a number of reasons, such as because they are pivoted at one end or because the tissue held between them is not of the uniform thickness.

[0017] Each conductive plate may have a flat elongate structure, e.g. having a width of 1 to 6 mm and a length of 3 to 12 mm. For endoscopic use, each plate may have a width of 1 to 3 mm and a length of 3 to 6 mm. Preferably, each plate has identical dimensions. The preferred dimensions may depend on the microwave frequency. Where 5.8 GHz energy is used, the plates may have a width of 2 mm and a length of 4 mm. The conductive plates may have curved distal ends. Removing sharp corners may reduce the risk of bowel wall perforation when operating in the GI tract, and may prevent unwanted concentrations of microwave energy. The conductive plates may have curved proximal ends, e.g. at the point at which they connect to the signal transition portion. The thickness of the plates may be 0.5 mm or less.

[0018] The signal transition portion may include a linking member that extends from a distal end of the coaxial cable, the linking member comprising an extension of the inner conductor of the coaxial cable surrounded by a dielectric cover, wherein a distal end of the extension of the inner conductor of the coaxial cable is connected to the second conductive plate. The linking member may have a length of 3 mm or more. The linking member itself may form a non-uniform transmission line.

[0019] The signal transition portion may include an outer connector that extends from the outer conductor of the coaxial cable and electrically connects the outer conductor of the coaxial cable to the first conductive plate. The proximal end of the outer connector may be curved to wrap around the outer conductor of the coaxial cable. The outer connector may taper (i.e. decrease in width) as it extends away from the outer conductor of the coaxial cable.

[0020] In another aspect of the invention, each jaw element may comprise its own lossy transmission line, as defined in claim 5.

[0021] Each of the first transmission line structure and the second transmission line structure is a parallel transmission line or a coaxial transmission line. The power splitter may comprise an arrangement of flexible microstrip transmission lines or coaxial transmission lines. For example, the signal transition may comprise any of a Wilkinson power divider, an arrangement of two quarter wavelength transformers, a 3 dB power splitter or the like. If a Wilkinson power divider is used to split the power available at the distal end of the coaxial cable into two equal parts, then the signal transition may comprise two semi-circular or straight sections that are each a quarter wavelength long at the frequency of operation, i.e. the overall length of the splitter is a half wavelength at the operating frequency. In this arrangement the impedance of the transmission lines that form the two semi-circular or straight sections is set as

$$Z_W = \sqrt{2}Z_0,$$

where Z_W is the impedance of the line that forms the Wilkinson power divider and Z_0 is the characteristic impedance of

the of the coaxial cable. In a preferred embodiment, the impedance of the coaxial cable is set to be the same as the transmission line inside the jaws, which in turn is set to be the same as the biological tissue to be treated.

[0022] In an arrangement where two quarter wavelength transformers are used, a virtual impedance exists at the proximal end of each quarter wavelength arm that has a value which is twice the impedance of the characteristic impedance of the transmission line that feeds this point, i.e. the impedance 'seen' at the end of the transmission line is equal to half the value of the virtual impedance. This assumes that the two quarter wave transformer sections are the same impedance, the impedance of the transmission line inside each of the two jaws is the same, and that each jaw makes good contact with the biological tissue, which is homogeneous and has a value of impedance that is the same or close to that of the impedance of the transmission lines inside the two jaws.

[0023] A further arrangement could use a transmission line cable with a characteristic impedance of Z_0 feeding a

Wilkinson power divider, whose lines have an impedance of $\sqrt{2}Z_0$, where each arm is connected to a quarter wavelength transformer, which impedance matches the characteristic impedance Z_0 to the impedance of the transmission lines within the jaws, which is well matched to the impedance of the tissue Z_t .

[0024] The pair of jaw elements may be biased apart, e.g. using springs or the like. The springs may be made from plastic or other suitable material that does not interfere with the manner in which the microwave frequency energy is lost between the conductive plates. Alternatively, the jaw elements may also be wholly or partially made from memory metal, e.g. Nitinol wire, and be opened and closed based on the application of heat applied to the structure (wire). This heat may be generated using a DC power source (resistive heating), which may involve the use of additional feed lines, or generated when the microwave field is applied to the jaws. For the latter, it may be desirable to include, i.e. paint or deposit, a section of lossy material within the jaws or on the jaws such that some of the microwave field is absorbed by the lossy material to produce local heat, which causes the jaws to close (or open).

[0025] The forceps may be mounted in a cylindrical sheath, i.e. an enclosure for the coaxial cable and the pair of jaw elements. The sheath may be retractable to expose the pair of jaw elements. The sheath may act as a protective cover to facilitate insertion of the forceps through the instrument channel of an endoscope. The diameter of the cylindrical sheath may be less than 2.8 mm.

[0026] The forceps may include a jaw closing mechanism in mechanical communication with the pair of jaw elements. For example, the jaw closing mechanism may include a handle and pull trigger in communication with the pair of jaw elements via one or more pull wires. The pull wires may extend alongside the coaxial cable through the sheath if the forceps are inserted through an endoscope. In one embodiment, the jaw closing mechanism may include a pantograph arranged to ensure that the jaw elements close together in such a way that their surfaces meet simultaneously along their length.

[0027] The pair of jaw elements may be rotatable, e.g. by rotating the sheath.

BRIEF DESCRIPTION OF THE DRAWINGS

[0028] Embodiments of the invention are discussed below in detail with reference to the accompanying drawings, in which:

- Fig. 1 is a modelled structure for an electrosurgical forceps that is an embodiment of the invention;
- Fig. 2 is a graph showing return loss for a modelled example of an electrosurgical forceps that is an embodiment of the invention;
- Fig. 3 is a side view of the modelled structure shown in Fig. 1 showing simulated power loss density in blood;
- Fig. 4 is a graph showing return loss for another modelled example of an electrosurgical forceps that is an embodiment of the invention;
- Fig. 5 is a side view of the modelled structure of Fig. 3 showing simulated power loss density in blood with a smaller spacing between jaw elements; and
- Fig. 6 is a schematic drawing of an electrosurgical forceps that is an embodiment of the invention;
- Fig. 7 is a schematic drawing of an endoscopic microwave forceps that is an embodiment of the invention;
- Fig. 8A shows a Wilkinson power divider arrangement that can be realised using flexible microstrip transmission line;
- Fig. 8B shows a Wilkinson power divider arrangement that may be realised using coaxial transmission lines;
- Fig. 9A shows a first design for electrosurgical forceps that uses a Wilkinson power divider realised using transmission lines;
- Fig. 9B shows a second design for electrosurgical forceps that uses a Wilkinson power divider realised using transmission lines; and
- Fig. 9C shows a third design for electrosurgical forceps that uses a Wilkinson power divider realised using transmission lines.

DETAILED DESCRIPTION; FURTHER OPTIONS AND PREFERENCES

[0029] The present invention provides a microwave coagulating forceps that can be operated through the channel of an endoscope. The diameter of the channel in the endoscope may be 2.2 mm, 2.8 mm or 3.2 mm. The purpose of the forceps is to grasp a thin section of tissue and to coagulate or cauterise the portion held between the forceps using microwave energy, e.g. at a frequency of 5.8 GHz or more.

[0030] Unlike known microwave forceps, the present invention is not designed to radiate microwave energy. Instead, one or preferably both jaws of the forceps are designed to act as unbalanced lossy transmission lines. This function may arise from the selected geometry of the jaws.

[0031] An advantage of the lossy transmission line structure is that the delivery of power into tissue can be more accurately focussed in areas of contact with tissue. In known radiating devices, efficient antenna functionality may be based on contact between the whole antenna structure and the tissue, whereby the absence of tissue contact along the whole antenna length can prevent the antenna from operating efficiently which in turns affects the amount of energy that is delivered (and reflected back into the instrument). In this design, power will be delivered into the part that is held in the jaw elements, even if it only occupies (touches) part of the jaw elements. Most of the remaining power will be reflected back to the generator rather than being radiated out into the patient. This structure also offers clinical benefit in terms of the reflected microwave energy being reflected back along the jaws of the instrument may be utilised to produce enhanced tissue coagulation as it returns along a path back to the generator. At the distal end of the transmission line formed by the two jaws in contact with tissue, a total mismatch occurs due to the fact that the line is either in air or some other mismatched medium at this point, hence the reflection coefficient is unity or close to unity, i.e. all of the wave begins to travel back along the jaws back to the source). The transmission line structure works on the basis of reflection coefficient or impedance match, whereby if the impedance of the contact tissue is well matched to the impedance of the transmission line (reflection coefficient zero or close to zero). Ideally, all of the energy is absorbed by the biological tissue that makes contact with the jaws and so all of the energy is dissipated by the time it reaches the distal end of the jaws, hence no energy is reflected back along the transmission line structure within the jaws back to the generator. Since no resonance is required for the energy to be delivered, the electrical length of the transmission line on the jaw element is not constrained in the same way as it would be e.g. for an antenna. Accordingly, the electrical length of the transmission lines used in the present invention may be non-resonant at the frequency of the microwave energy (when the transmission line is loaded by biological tissue), i.e. not a multiple of a quarter loaded wavelength of the microwave energy.

[0032] The power delivered into the biological tissue at any point is given by:

$$P_t = P_i(1 - \Gamma^2),$$

where P_t is the power transmitted into the tissue at a particular point, P_i is the incident power at the point where the transmission line makes contact with the tissue load, and Γ is the reflection coefficient at that point, which is related to the impedance of the transmission line (Z_0) and the impedance of the tissue load (Z_L) by

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}.$$

[0033] The present invention may find particular use in the polypectomy procedures in the gastrointestinal (GI) tract, where the stem of a polyp needs to be sealed and cut. In such situations, the stem of the polyp may not contact all of the jaws of the forceps.

[0034] Fig. 1 shows a basic representative design for a microwave coagulating forceps that is an embodiment of the invention. The design is a model created using CST Microwave Studio®, which was then used to simulate the performance as various modifications were made to the structure to optimise the return loss and power density in biological tissue.

[0035] Although the examples below discuss the use of the forceps in an endoscope, the present invention need not be limited in this way. It may be applicable to laparoscopic techniques or used in open surgery.

[0036] Fig. 1 shows a pair of microwave coagulating forceps 100 that is an embodiment of the invention. The forceps 100 comprise a coaxial cable 102 for conveying microwave energy from a suitable generator (not shown) down an endoscope instrument channel to a pair of jaw elements 104, 106. The generator may be any device capable of delivering a controllable and stable microwave signal. For example, the apparatus disclosed in WO 2012/076844 may be used.

[0037] The coaxial cable 102 may be about 1.2 mm or 2.2mm in diameter in order to allow room for a jaw operation mechanism in the instrument channel of the endoscope. Sucoform 47 manufactured by Huber+Suhner is a suitable cable that is 1.2 mm in diameter and is flexible enough to allow full manipulation of the endoscope with the cable within its channel.

[0038] In this embodiment, the jaw elements 104, 106 of the forceps are modelled as two conductive (e.g. metal) plates 0.5 mm thick and 2 mm wide with curved front and back ends. A first jaw element 104 is electrically connected to the outer conductor 108 of the coaxial cable 102 via an angled tapered connector 110. A second jaw element 106 is electrically connected to the inner conductor (not shown) of the coaxial cable by a linking member 112, which is an extension of the inner conductor and the dielectric 114 that surrounds it beyond the end of the outer conductor 108.

[0039] The jaw elements 104, 106 are movable relative to each other to open and close the gap between them. For example, the jaw elements 104, 106 may be connected to a hinge or pivot (not shown). The forceps 100 may thus include a jaw operation mechanism, which provided mechanical communication between the jaw elements and the distal end of the device. For example, the jaw operation mechanism may comprise one or more pull wires extending alongside the coaxial cable 102 through the instrument channel of the endoscope. Such jaw operation mechanisms are well known. In other embodiments, a pantograph arrangement may be used to open and close the jaw elements in such a way that their surfaces simultaneously meet all the way along their length.

[0040] The jaw elements 104, 106 may have a maximum separation of 2 mm, e.g. set by a stopper on the hinge. When pressed together, the jaw elements 104, 106 would present a distal cross-section area that measures 2.23 mm across the diagonal. This is small enough for an outer sheath (not shown) to fit around the jaw elements and still allow passage through the instrument channel of the endoscope. The sheath may act to protect the forceps (e.g. from damage or contamination) as it is inserted down the instrument channel of the endoscope, or to stop snagging or other damage as the tool is manipulated into position inside the patient. The sheath may be torque stable to assist rotation of the forceps. The sheath may be retractable to expose the jaw elements when the forceps are in position of use. Alternatively, the forceps may be extendable to protrude beyond the end of the sheath. In practice it is possible for the conductive plates that form the jaw elements to be thinner, e.g. 0.4 mm or less, as long as they retain sufficient stiffness to prevent unwanted flexing in use.

[0041] According to the invention, the function of the conductive plates is as unbalanced lossy transmission lines, whereby microwave frequency energy delivered to the jaw element leaks out into the surrounding environment. To optimise the geometry of the blades, the return loss of the modelled structure was simulated whilst varying a number of parameters, as shown in Table 1.

Table 1. Parameters varied simulations

Run No.	Wire length (mm)	Plate length (mm)	Jaw width (mm)	Other
0	9	5	2	
1	6	5	2	
2	4	5	2	
3	3 to 5	5	2	
4	4	3 to 6	2	
5	3	4	2	
6	3	4	2	With balun
7	3	4	0.75:to 3.25	
8	3	4	2	
9	3	4	2	Gap 1mm

[0042] The parameter wire length corresponds to the length of the wire joining the coaxial cable to the conductive plates, e.g. the length of the connector 110 and linking member 112. In practice it is desirable for the wires to have a similar length. Any difference in length should be a small part, e.g. less than one eighth of a wavelength at the operating microwave frequency. It was found that with 3 mm wire length and 4 mm blade length the return loss was better than 7 dB at 5.8 GHz, as shown in Fig. 2. This means that less than 20% of the power is reflected back towards the generator, and over 80% is available for use at the conductive plates. This is reasonable efficiency, as any improvements could only increase the power available at the plates by less than 25%.

[0043] Fig. 3 shows the results of simulating power absorption in the region between the jaw elements for a 3 mm wire length and a 4 mm plate length when biological tissue (in this case blood) is present in that region. The power loss density differs between end regions 116 at the distal and proximal ends of the plates and a central region 114.

[0044] In the central region 114 the power loss density is about 65 dBW/m³ for 1 W input power. In practice, it is expected that the device would be used with an input power of 10 W, whereby the power loss density (heating power)

in this region would be 15 dBW/cm³. This is about 30 W/cm³ which is enough to raise the temperature of blood by about 7 Ks⁻¹, assuming that the specific heat capacity of tissue is about 4.2 J/g/K, and that the density of tissue is about 1 g/cm³ so that the heat capacity of tissue is about 4.2 J/cm³/K.

[0045] In the end regions 116, the heating rate will be about three times this, i.e. 20 Ks⁻¹.

[0046] In this example, the volume of the region between the plates is 4 mm long by 2 mm wide and 2 mm high, i.e. 16 mm³. The average power density is about 90 W/cm³, so the total power absorbed in this region is about 1.5 W. It is expected that blood or tissue that intrudes into the triangular gap where the connector 110 and linking member 112 flare out towards the plates would also be heated.

[0047] Fig. 4 shows the return loss when the separation of the plates is reduced to 1 mm. The return loss at 5.8 GHz changes from just more than 7 dB to just more than 6 dB. But despite this change, more than 75% of the incident power is available to heat the tissue.

[0048] Fig. 5 shows the results of simulating power absorption in the region between the jaw elements for the smaller plate spacing, and it can be seen that the power loss density is higher, which might be expected because the slightly lower total power is concentrated in half the tissue thickness. The indicated power density in a central region 118 of the gap for 1 W incident power is about 66 dBW/m³, which corresponds to about 38 W/cm³ for 10 W incident power, which corresponds to a temperature rise of about 9 Ks⁻¹.

[0049] In a practical device, the jaw elements may be biased apart, e.g. using springs or the like. Such springs may be made from plastic, which will not affect the results of the simulations discussed above.

[0050] The shape of the connector 110 can be optimised to improve the transfer of microwave energy to the jaw elements 104, 106. In particular, it is desirable to hollow out the proximal end of the connector 110 at the coaxial cable 112 so that it curves around the dielectric 112. This geometry improves the return loss by making more gradual the change from the coaxial transmission line of the coaxial cable 112 to the twin transmission lines of the jaw elements 104, 106.

[0051] Fig. 6 shows a schematic view of an endoscopic microwave forceps 300 that is an embodiment of the invention. The forceps 300 comprises a body 308 having a flexible feed cable 306 extending from it. The feed cable 306 is not drawn to scale; it has a length and diameter suitable for insertion down the instrument channel of an endoscope (not shown). This cable may be less than 2.8 mm in overall diameter to allow it to be inserted down the instrument channel of an endoscope or a gastroscope. The feed cable 306 comprises a outer sleeve that contains the coaxial cable and jaw opening mechanism discussed above. At a distal end of the cable 306 are a pair of jaw elements 302, 304, which are pivotable relative to each other about a hinge 305 to open and close a space between opposing surfaces thereof under the control of the jaw opening mechanism.

[0052] The body 308 includes a handle 310 and pull trigger 312 which operates the jaw closing mechanism in a conventional manner. The pull trigger 312 may alternatively be a mechanical slider or any other suitable mechanism that allow the jaws to be opened and closed. The body 308 is connected to a microwave signal generator (not shown) by a suitable cable 314.

[0053] The geometry of the jaw elements 302, 304 is selected so that they function as lossy transmission lines as discussed above.

[0054] Fig. 7 shows another embodiment of the invention, where the microwave forceps are inserted through the instrument channel 402 of an endoscope 400. The proximal end of the feed cable 404 terminates at a handle 406, which includes a pull trigger 408 for operating the jaw mechanism as discussed above. A hand grip 410 is clamped onto the feed cable to provide a means of rotating cable, and therefore controlling the orientation of the jaws 412 at the distal end of the cable. The outer sleeve of the feed cable may include internal braids which provide torque stability, i.e. resist twisting of the sleeve relative to the coaxial cable. Ideally, the translation between rotation of the handle at the proximal end of the device and the circular movement of the jaws at the distal end will be 1:1, but lesser translation ratios, e.g. 1:2 may be sufficient.

[0055] Fig. 8A shows a first configuration of a Wilkinson power divider 500, which functions to split an input power P_I into two equal parts (P₂ and P₃) using two quarter wavelength semi-circular lines or arms. Each arm may also function as an impedance transformer. Thus, the complete physical length of the structure is a half of the electrical wavelength at the frequency of operation. In order for this power splitting design to be used in practice, it may be preferable for the structure to be fabricated onto a flexible microwave substrate, where the tracks may be printed or photo etched. In order to balance the two output ports (P₂ and P₃), it is preferable to include a balancing resistor 502; the impedance value of this balancing resistor should preferably be twice the characteristic impedance.

[0056] Figure 8B gives a second configuration of a Wilkinson power divider 600. In this configuration, coaxial lines 602, 604 are used to realise the divider. If standard 75 Ω coaxial cable is used for the quarter wavelength sections 602, 604, the divider will provide a reasonable match for 50 Ω input and output ports. Ideally, if the input and output ports are

50 Ω, then the impedance of each of the quarter wavelength arms is $70.71\ \Omega\ (= \sqrt{2} \times 50)$. In practice, the coaxial impedance transformer should be as small and as flexible as possible in order to fit in the endoscope.

[0057] Fig. 9A shows a schematic outline for a first example microwave forceps device 700 that uses a Wilkinson power divider 702, where the impedance Z_t of the biological tissue 704 at the frequency of operation is the same as the impedance of the transmission line 706 within the jaws and is also the same as the impedance of the coaxial cable 708 that connects the microwave energy generator to the device. In Fig. 9A a quarter wave transformer 710 is used at the proximal end between the output of the generator 712 and the coaxial cable 708 to match the output impedance Z_s of the generator 712 to the impedance of the coaxial cable 708 (which in this embodiment is also the impedance of the biological tissue 704 and the impedance of the transmission line 706 within the jaws). The impedance of the quarter

wavelength transformer 710 is set as $\sqrt{Z_s \times Z_t}$. Normally, the output impedance of the microwave energy generator 712 will be 50 Ω and if it is assumed that the impedance of blood is 25 Ω at the preferred frequency of operation, then the impedance of the quarter wavelength transformer 710 will need to be 35.36 Ω . This transformer could be realised in practice using a standard 50 Ω co-axial transmission line with the diameter of the inner conductor increased, the inner diameter of the outer conductor reduced, the value of relative permittivity (dielectric constant) of the material that separates the inner and outer conductors increased, or by varying a combination of these parameters. It would be relatively straightforward to manufacture 25 Ω co-axial transmission line.

[0058] Fig. 9B shows a schematic outline for a second example microwave forceps device 800 that uses a Wilkinson power divider 802, where the impedance Z_0 of the coaxial cable 808 that connects the generator 812 to the instrument is the same as the output impedance Z_s of the generator, which is nominally 50 Ω . In Fig. 9B there is a quarter wavelength transformer 810, 811 located between the distal end of each arm of the Wilkinson power divider 802 and the proximal end of a respective transmission line 806 that couples to the biological tissue 804. In this example, if it is assumed that the impedance Z_t of the biological tissue is well matched to the impedance of the transmission lines 806 within the jaws,

then the impedance of the quarter wavelength matching transformers 810 is $\sqrt{Z_0 \times Z_t}$.

[0059] Fig. 9C shows a schematic outline for a third example microwave forceps device 900 that uses a pair of quarter wavelength transmission line transformer sections 902, 903 to match the impedance of the biological tissue 904 to the impedance of the coaxial cable 908 and the microwave energy generator 912 to ensure efficient power transfer between the generator and the tissue load. Again, in this configuration it is assumed that the impedance of the transmission line 906 within the jaws is well matched to the impedance of the biological tissue Z_t . In this arrangement, each transformer 902, 903 transforms the impedance 'seen' at the jaws to a virtual impedance that has a value equal to twice the characteristic impedance of the coaxial cable 908, such that the proximal end of the two arms of the transformers are connected in parallel to give an impedance that is equal to the characteristic impedance of the feed cable (main microwave transmission line). The impedance Z_0 of the coaxial cable 908 may be the same as the output impedance Z_s of the generator 912, and so the function of the two quarter wavelength impedance transformers is to match Z_0 to Z_t . It may also be noted that the two transformers are connected in parallel at this point, therefore, the impedance seen at the proximal end of each of the quarter wavelength impedance transformers is $2Z_0$. Thus, the impedance of the quarter

wavelength matching sections 902, 903 is $\sqrt{2Z_0 \times Z_t}$.

Claims

1. Electrosurgical forceps comprising:

- a pair of jaw elements pivotable relative to each other to open and close a gap therebetween;
 - a first conductive element mounted in one of the pair of jaw elements adjacent to the gap;
 - a second conductive element mounted in the other one of the pair of jaw elements adjacent to the gap opposite the first conductive element;
 - a coaxial cable for conveying microwave energy having a specific frequency; and
 - a signal transition portion at a distal end of the coaxial cable, the signal transition portion being arranged to connect the first conductive element to an outer conductor of the coaxial cable and to connect the second conductive element to an inner conductor of the coaxial cable,
- wherein the first conductive element and the second conductive element and the gap between the pair of jaws constitute a transmission line to support the microwave energy as a travelling wave,
- wherein the conductive elements on opposing surfaces of the pair of jaw elements are not in a uniform spatial relationship with each other along the length of the pair of jaw elements,

wherein the transmission line formed by the first conductive element and the second conductive element is designed to couple electrical energy into biological tissue in the gap between the pair of jaw elements to prevent multiple reflections of the travelling wave, whereby the transmission line is non-resonant for the microwave energy along the travelling wave in the presence of biological tissue, and

wherein the transmission line has a geometry selected to exhibit high loss at the specific frequency of the microwave energy when the biological tissue is present in the gap, whereby power received at the proximal end of the transmission line is deliverable into the biological tissue in the gap during a single transit of the travelling wave along the transmission line.

2. Electrosurgical forceps according to claim 1, wherein, when biological tissue is present in the gap, 80% of power received at the proximal end of the transmission line is delivered into the biological tissue during a single transit of the travelling wave along the transmission line.

3. Electrosurgical forceps according to any preceding claim, wherein each of the first conductive element and the second conductive element comprises a flat conductive plate having a curved distal end and/or a curved proximal end.

4. Electrosurgical forceps according to any preceding claim, wherein the signal transition portion includes a linking member that extends from a distal end of the coaxial cable, the linking member comprising an extension of the inner conductor of the coaxial cable surrounded by a dielectric cover, wherein a distal end of the extension of the inner conductor of the coaxial cable is connected to the second conductive element, and wherein the signal transition portion includes an outer connector that extends from the outer conductor of the coaxial cable and electrically connects the outer conductor of the coaxial cable to the first conductive element.

5. Electrosurgical forceps comprising:

a pair of jaw elements pivotable relative to each other to open and close a gap therebetween;
a first transmission line structure mounted in one of the pair of jaw elements adjacent to the gap;
a second transmission line structure mounted in the other one of the pair of jaw elements adjacent to the gap opposite the first transmission line structure;

a coaxial cable for conveying microwave energy having a specific frequency; and
a power splitter at a distal end of the coaxial cable, the power splitter being arranged to divide the microwave frequency energy conveyed by the coaxial cable between the first transmission line structure and the second transmission line structure,

wherein each of the first transmission line structure and the second transmission line structure consists of a transmission line arranged to support the microwave energy as a travelling wave, wherein the transmission line of each of the first transmission line structure and the second transmission line structure is designed to couple electrical energy into biological tissue in the gap between the pair of jaw elements to prevent multiple reflections of the travelling wave, whereby the transmission line is non-resonant for the microwave energy in the presence of biological tissue, and

wherein the transmission line has a geometry selected to exhibit high loss at the specific frequency of the microwave energy when the biological tissue is present in the gap, whereby power received at the proximal end of the transmission line is deliverable into the biological tissue in the gap during a single transit of the travelling wave along the transmission line.

6. Electrosurgical forceps according to any preceding claim, wherein, when biological tissue is present in the gap, 80% of power received at the proximal end of the transmission line is delivered into the biological tissue during a single transit of the travelling wave along the transmission line.

7. Electrosurgical forceps according to any preceding claim, wherein the geometry of the transmission line is selected to exhibit a return loss of 1 dB at the specific frequency of the microwave energy when air is present in the gap.

8. Electrosurgical forceps according to any preceding claim, wherein the specific frequency is any one of 915 MHz, 2.45 GHz, 3.3 GHz, 5.8 GHz, 10 GHz, 14.5 GHz and 24 GHz.

9. Electrosurgical forceps according to any one of claims 5 to 8, wherein the transmission line of each of the first transmission line structure and the second transmission line structure is a parallel transmission line or a coaxial transmission line.

10. Electrosurgical forceps according to any one of claims 5 to 9, wherein the power splitter comprises a pair of quarter wavelength transmission lines arranged to match the impedance of the coaxial cable to the impedance of the first transmission line structure and second transmission line structure.
11. Electrosurgical forceps according to any preceding claim including a quarter wavelength impedance transformer at the proximal end of the coaxial cable, the quarter wavelength impedance transformer being arranged to match the impedance of the coaxial cable to a generator for delivering the microwave frequency energy into the coaxial cable.
12. Electrosurgical forceps according to any preceding claim, wherein the pair of jaw elements are biased apart.
13. Electrosurgical forceps according to any preceding claim including a sheath for enclosing the coaxial cable and the pair of jaw elements, wherein the sheath is retractable to expose the pair of jaw elements.
14. Electrosurgical forceps according to claim 21, wherein the sheath is cylindrical and has a diameter less than 2.8 mm.
15. Electrosurgical forceps according to any preceding claim including a jaw closing mechanism in mechanical communication with the pair of jaw elements, wherein the jaw closing mechanism includes a pantograph arranged to ensure that the jaw elements close together in such a way that their surfaces meet simultaneously along their length.

Patentansprüche

1. Elektrochirurgische Zange, Folgendes umfassend:

ein Paar von Klauenelementen, die relativ zu einander schwenkbar sind, um einen Spalt dazwischen zu öffnen und zu schließen;
 ein erstes leitfähiges Element, das in einem des Paares von Klauenelementen benachbart zu dem Spalt angebracht ist;
 ein zweites leitfähiges Element, das in dem anderen des Paares von Klauenelementen benachbart zum Spalt, dem ersten leitfähigen Element gegenüberliegend angebracht ist;
 ein Koaxialkabel zum Übertragen von Mikrowellenenergie, die eine spezifische Frequenz aufweist; und
 einen Signalübergangsabschnitt an einem distalen Ende des Koaxialkabels, wobei der Signalübergangsabschnitt angeordnet ist, um das erste leitfähige Element mit einem Außenleiter des Koaxialkabels zu verbinden und das zweite leitfähige Element mit einem Innenleiter des Koaxialkabels zu verbinden, wobei
 das erste leitfähige Element und das zweite leitfähige Element und der Spalt zwischen dem Paar von Klauen eine Übertragungsleitung bilden, um die Mikrowellenenergie als Wanderwelle zu unterstützen, wobei die leitfähigen Elemente auf gegenüberliegenden Oberflächen des Paares von Klauenelementen entlang der Länge des Paares von Klauenelementen miteinander nicht in einem einheitlichen räumlichen Verhältnis stehen, wobei
 die durch das erste und das zweite leitfähige Element ausgebildete Übertragungsleitung konzipiert ist, um elektrische Energie in biologisches Gewebe im Spalt zwischen dem Paar von Klauenelementen zu koppeln, um mehrfache Reflexionen der Wanderwelle zu verhindern, wodurch die Übertragungsleitung für die Mikrowellenenergie entlang der Wanderwelle in Anwesenheit von biologischem Gewebe nichtresonant ist, und wobei die Übertragungsleitung eine Geometrie aufweist, die ausgewählt ist, um bei der spezifischen Frequenz der Mikrowellenenergie einen hohen Verlust aufzuweisen, wenn das biologische Gewebe im Spalt vorhanden ist, wodurch Leistung, die am proximalen Ende der Übertragungsleitung empfangen wird, während eines einzelnen Durchgangs der Wanderwelle entlang der Übertragungsleitung in das biologische Gewebe im Spalt zuführbar ist.

2. Elektrochirurgische Zange nach Anspruch 1, wobei, wenn biologisches Gewebe im Spalt vorhanden ist, 80 % der Leistung, die am proximalen Ende der Übertragungsleitung empfangen wird, während eines einzelnen Durchgangs der Wanderwelle entlang der Übertragungsleitung in das biologische Gewebe zugeführt wird.
3. Elektrochirurgische Zange nach einem der vorhergehenden Ansprüche, wobei jedes des ersten und des zweiten leitfähigen Elements eine flache leitfähige Platte umfasst, die ein gekrümmtes distales und/oder ein gekrümmtes proximales Ende aufweist.
4. Elektrochirurgische Zange nach einem der vorhergehenden Ansprüche, wobei der Signalübergangsabschnitt ein Verbindungselement umfasst, das sich von einem distalen Ende des Koaxialkabels erstreckt, wobei das Verbindungs-

5 dungelement eine Verlängerung des Innenleiters des Koaxialkabels, der von einer dielektrischen Abdeckung umgeben ist, umfasst, wobei ein distales Ende der Verlängerung des Innenleiters des Koaxialkabels mit dem zweiten leitfähigen Element verbunden ist, und wobei der Signalübergangsabschnitt einen Außenverbinder umfasst, der sich vom Außenleiter des Koaxialkabels erstreckt und den Außenleiter des Koaxialkabels elektrisch mit dem ersten leitfähigen Element verbindet.

5. Elektrochirurgische Zange, Folgendes umfassend:

10 ein Paar von Klauenelementen, die relativ zu einander schwenkbar sind, um einen Spalt dazwischen zu öffnen und zu schließen;
 eine erste Übertragungsleitungsstruktur, die in einem des Paares von Klauenelementen benachbart zum Spalt angebracht ist;
 eine zweite Übertragungsleitungsstruktur, die in dem anderen des Paares von Klauenelementen benachbart zum Spalt, der ersten Übertragungsleitungsstruktur gegenüberliegend angebracht ist;
 15 ein Koaxialkabel zum Übertragen von Mikrowellenenergie, die eine spezifische Frequenz aufweist;
 einen Leistungsteiler an einem distalen Ende des Koaxialkabels, wobei der Leistungsteiler angeordnet ist, um die durch das Koaxialkabel geleitete Mikrowellenfrequenzenergie auf die erste Übertragungsleitungsstruktur und die zweite Übertragungsleitungsstruktur aufzuteilen,
 wobei jede der ersten und der zweiten Übertragungsleitungsstruktur aus einer Übertragungsleitung besteht,
 20 die angeordnet ist, um die Mikrowellenenergie als Wanderwelle weiterzuleiten, wobei die Übertragungsleitung von jeder der ersten und der zweiten Übertragungsleitungsstruktur konzipiert ist, um elektrische Energie in biologisches Gewebe im Spalt zwischen dem Paar von Klauenelementen zu koppeln, um mehrfache Reflexionen der Wanderwelle zu verhindern, wodurch die Übertragungsleitung für die Mikrowellenenergie entlang der Wanderwelle in Anwesenheit von biologischem Gewebe nichtresonant ist, und wobei
 25 die Übertragungsleitung eine Geometrie aufweist, die ausgewählt ist, um bei der spezifischen Frequenz der Mikrowellenenergie einen hohen Verlust aufzuweisen, wenn das biologische Gewebe im Spalt vorhanden ist, wodurch Leistung, die am proximalen Ende der Übertragungsleitung empfangen wird, während eines einzelnen Durchgangs der Wanderwelle entlang der Übertragungsleitung in das biologische Gewebe im Spalt zuführbar ist.

30 6. Elektrochirurgische Zange nach einem der vorhergehenden Ansprüche, wobei, wenn biologisches Gewebe im Spalt vorhanden ist, 80 % der Leistung, die am proximalen Ende der Übertragungsleitung empfangen wird, während eines einzelnen Durchgangs der Wanderwelle entlang der Übertragungsleitung in das biologische Gewebe zugeführt wird.

35 7. Elektrochirurgische Zange nach einem der vorhergehenden Ansprüche, wobei die Geometrie der Übertragungsleitung ausgewählt ist, um bei der spezifischen Frequenz der Mikrowellenenergie eine Reflexionsdämpfung von 1 dB aufzuweisen, wenn Luft im Spalt vorhanden ist.

8. Elektrochirurgische Zange nach einem der vorhergehenden Ansprüche, wobei die spezifische Frequenz eine beliebige aus 915 MHz, 2,45 GHz, 3,3 GHz, 5,8 GHz, 10 GHz, 14,5 GHz und 24 GHz ist.

40 9. Elektrochirurgische Zange nach einem der Ansprüche 5 bis 8, wobei die Übertragungsleitung von jeder der ersten und der zweiten Übertragungsleitungsstruktur eine Parallel-Übertragungsleitung oder eine Koaxial-Übertragungsleitung ist.

45 10. Elektrochirurgische Zange nach einem der Ansprüche 5 bis 9, wobei der Leistungsteiler ein Paar von Viertelwellenlängen-Übertragungsleitungen umfasst, die angeordnet sind, um die Impedanz des Koaxialkabels an die Impedanz der ersten und der zweiten Übertragungsleitungsstruktur anzupassen.

50 11. Elektrochirurgische Zange nach einem der vorhergehenden Ansprüche, umfassend einen Viertelwellenlängen-Impedanzwandler am proximalen Ende des Koaxialkabels, wobei der Viertelwellenlängen-Impedanzwandler angeordnet ist, um die Impedanz des Koaxialkabels an einen Generator anzupassen, um die Mikrowellenenergie in das Koaxialkabel zuzuführen.

55 12. Elektrochirurgische Zange nach einem der vorhergehenden Ansprüche, wobei das Paar von Klauenelementen voneinander weg vorgespannt ist.

13. Elektrochirurgische Zange nach einem der vorhergehenden Ansprüche, umfassend eine Ummantelung zum Einkapseln des Koaxialkabels und des Paares von Klauenelementen, wobei die Ummantelung zurückgezogen werden

kann, um das Paar von Klauenelementen freizulegen.

14. Elektrochirurgische Zange nach Anspruch 21, wobei die Ummantelung zylindrisch ist und einen Durchmesser von weniger als 2,8 mm aufweist.

15. Elektrochirurgische Zange nach einem der vorhergehenden Ansprüche, umfassend einen Klauenverschlussmechanismus, der in mechanischer Kommunikation mit dem Paar von Klauenelementen steht, wobei der Klauenverschlussmechanismus einen Pantografen umfasst, der angeordnet ist, um zu gewährleisten, dass sich die Klauenelemente derart gegeneinander schließen, dass ihre Oberflächen entlang ihrer Länge gleichzeitig aufeinandertreffen.

Revendications

1. Pince électrochirurgicale comprenant :

une paire d'éléments de mâchoire pouvant pivoter l'un par rapport à l'autre pour ouvrir et fermer un espace entre eux ;
un premier élément conducteur monté dans un de la paire d'éléments de mâchoire adjacent à l'espace ;
un second élément conducteur monté dans l'autre de la paire d'éléments de mâchoire adjacent à l'espace opposé au premier élément conducteur ;
un câble coaxial pour acheminer une énergie micro-onde ayant une fréquence spécifique ; et
une partie de transition de signal à une extrémité distale du câble coaxial, la partie de transition de signal étant conçue pour connecter le premier élément conducteur à un conducteur externe du câble coaxial et pour connecter le second élément conducteur à un conducteur interne du câble coaxial,
dans laquelle le premier élément conducteur et le second élément conducteur et l'espace entre la paire de mâchoires constituent une ligne de transmission pour supporter l'énergie micro-onde sous forme d'une onde progressive,
dans laquelle les éléments conducteurs sur les surfaces opposées de la paire d'éléments de mâchoire ne sont pas dans une relation spatiale uniforme l'un avec l'autre le long de la paire d'éléments de mâchoire,
dans laquelle la ligne de transmission formée par le premier élément conducteur et le second élément conducteur est conçue pour coupler l'énergie électrique dans le tissu biologique dans l'espace entre la paire d'éléments de mâchoire pour empêcher de multiples réflexions de l'onde progressive, moyennant quoi la ligne de transmission est non résonante pour l'énergie micro-onde le long de l'onde progressive en la présence de tissu biologique, et
dans laquelle la ligne de transmission a une géométrie choisie pour présenter une perte élevée à la fréquence spécifique de l'énergie micro-onde lorsque le tissu biologique est présent dans l'espace,
moyennant quoi la puissance reçue à l'extrémité proximale de la ligne de transmission peut être délivrée dans le tissu biologique dans l'espace pendant un seul transit de l'onde progressive le long de la ligne de transmission.

2. Pince électrochirurgicale selon la revendication 1, dans laquelle, lorsqu'un tissu biologique est présent dans l'espace, 80 % de la puissance reçue à l'extrémité proximale de la ligne de transmission est délivrée dans le tissu biologique pendant un seul transit de l'onde progressive le long de la ligne de transmission.

3. Pince électrochirurgicale selon l'une quelconque des revendications précédentes, dans laquelle chacun du premier élément conducteur et du second élément conducteur comprend une plaque conductrice plate ayant une extrémité distale incurvée et/ou une extrémité proximale incurvée.

4. Pince électrochirurgicale selon l'une quelconque des revendications précédentes, dans laquelle la partie de transition de signal inclut un élément de liaison qui s'étend à partir d'une extrémité distale du câble coaxial, l'élément de liaison comprenant un prolongement du conducteur interne du câble coaxial entouré par une protection diélectrique, dans laquelle une extrémité distale du prolongement du conducteur interne du câble coaxial est connectée au second élément conducteur, et dans laquelle la partie de transition de signal inclut un connecteur externe qui s'étend à partir du conducteur externe du câble coaxial et connecte électriquement le conducteur externe du câble coaxial au premier élément conducteur.

5. Pince électrochirurgicale comprenant :

une paire d'éléments de mâchoire pouvant pivoter l'un par rapport à l'autre pour ouvrir et fermer un espace

entre eux ;

une première structure de ligne de transmission montée dans un de la paire d'éléments de mâchoire adjacente à l'espace ;

une seconde structure de ligne de transmission dans l'autre de la paire d'éléments de mâchoire adjacente à l'espace opposée à la première structure de ligne de transmission ;

un câble coaxial pour acheminer une énergie micro-onde ayant une fréquence spécifique ; et

un répartiteur de puissance à une extrémité distale du câble coaxial, le répartiteur de puissance étant conçu pour diviser l'énergie de fréquence micro-onde acheminée par le câble coaxial entre la première structure de ligne de transmission et la seconde structure de ligne de transmission,

dans laquelle chacune de la première structure de ligne de transmission et de la seconde structure de ligne de transmission est constituée d'une ligne de transmission conçue pour supporter l'énergie micro-ondes sous forme d'une onde progressive, dans laquelle la ligne de transmission de chacune de la première structure de ligne de transmission et de la seconde structure de ligne de transmission est conçue pour coupler l'énergie biologique dans le tissu biologique dans l'espace entre la paire d'éléments de mâchoire pour empêcher de multiples réflexions de l'onde progressive, moyennant quoi la ligne de transmission est non résonnante pour l'énergie micro-onde en la présence de tissu biologique, et

dans laquelle la ligne de transmission a une géométrie sélectionnée pour présenter une perte élevée à la fréquence spécifique de l'énergie micro-onde lorsque le tissu biologique est présent dans l'espace, moyennant quoi une puissance reçue à l'extrémité proximale de la ligne de transmission peut être délivrée dans le tissu biologique dans l'espace pendant un seul transit de l'onde progressive le long de la ligne de transmission.

6. Pince électrochirurgicale selon l'une quelconque des revendications précédentes, dans laquelle, lorsqu'un tissu biologique est présent dans l'espace, 80 % de la puissance reçue à l'extrémité proximale de la ligne de transmission est délivrée dans le tissu biologique pendant un seul transit de l'onde progressive le long de la ligne de transmission.

7. Pince électrochirurgicale selon l'une quelconque des revendications précédentes, dans laquelle la géométrie de la ligne de transmission est choisie pour présenter une perte de retour de 1 dB à la fréquence spécifique de l'énergie micro-onde lorsque de l'air est présent dans l'espace.

8. Pince électrochirurgicale selon l'une quelconque des revendications précédentes, dans laquelle la fréquence spécifique est l'une quelconque de 915 MHz, 2,45 GHz, 3,3 GHz, 5,8 GHz, 10 GHz, 14,5 GHz et 24 GHz.

9. Pince électrochirurgicale selon l'une quelconque des revendications 5 à 8, dans laquelle la ligne de transmission de chacune de la première structure de ligne de transmission et de la seconde structure de ligne de transmission est une ligne de transmission parallèle ou une ligne de transmission coaxiale.

10. Pince électrochirurgicale selon l'une quelconque des revendications 5 à 9, dans laquelle le répartiteur de puissance comprend une paire de lignes de transmission quart d'onde conçues pour faire correspondre l'impédance du câble coaxial à l'impédance de la première structure de ligne de transmission et de la seconde structure de ligne de transmission.

11. Pince électrochirurgicale selon l'une quelconque des revendications précédentes, incluant un transformateur d'impédance quart d'onde à l'extrémité proximale du câble coaxial, le transformateur d'impédance quart d'onde étant conçu pour faire correspondre l'impédance du câble coaxial à un générateur pour délivrer l'énergie de fréquence micro-onde dans le câble coaxial.

12. Pince électrochirurgicale selon l'une quelconque des revendications précédentes, dans laquelle la paire d'éléments de mâchoire sont écartés de manière oblique.

13. Pince électrochirurgicale selon l'une quelconque des revendications précédentes, incluant une gaine pour enfermer le câble coaxial et la paire d'éléments de mâchoire, dans laquelle la gaine est rétractable pour exposer la paire d'éléments de mâchoire.

14. Pince électrochirurgicale selon la revendication 21, dans laquelle la gaine est cylindrique et a un diamètre inférieur à 2,8 mm.

15. Pince électrochirurgicale selon l'une quelconque des revendications précédentes, incluant un mécanisme de fermeture de mâchoire en communication mécanique avec la paire d'éléments de mâchoire, dans laquelle le mécanisme

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de fermeture de mâchoire inclut un pantographe conçu pour s'assurer que les éléments de mâchoire se ferment ensemble de telle manière que leurs surfaces se rencontrent simultanément le long de leur longueur.

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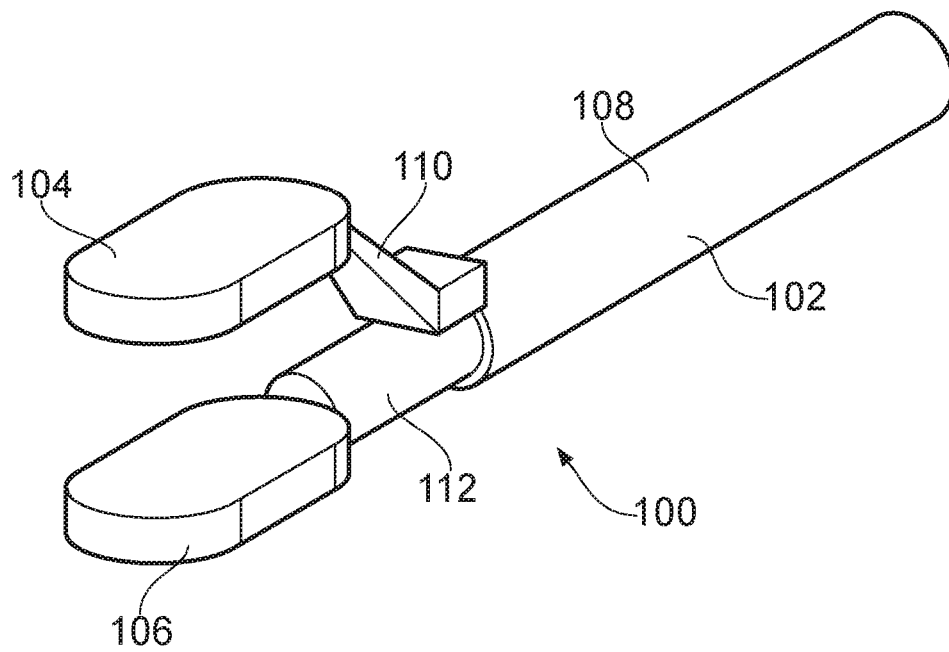


FIG. 1

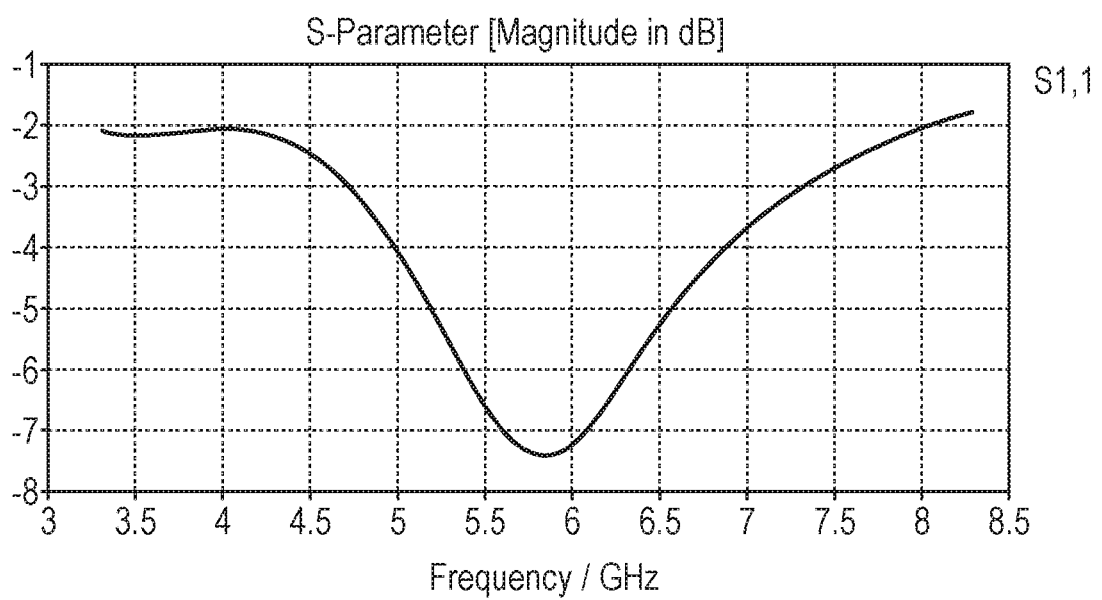


FIG. 2

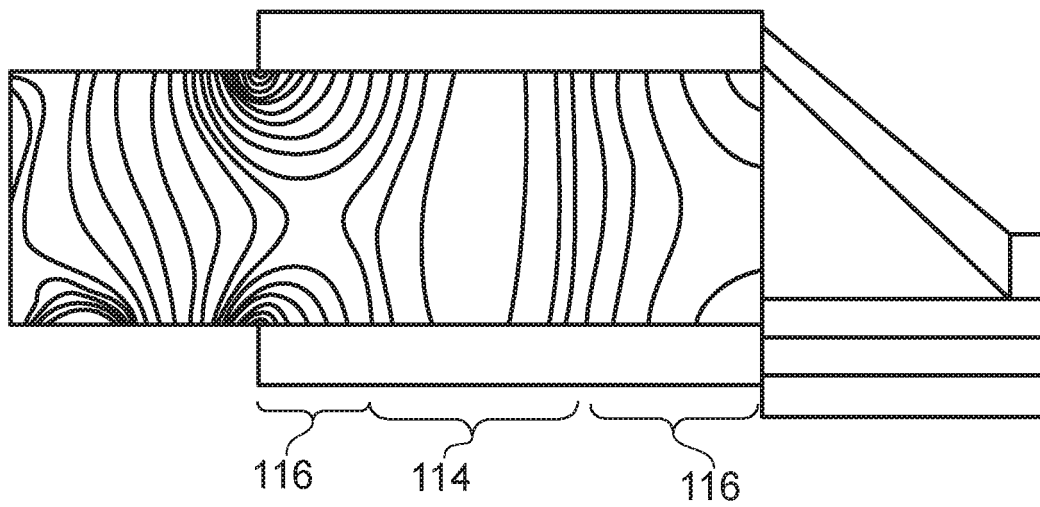


FIG. 3

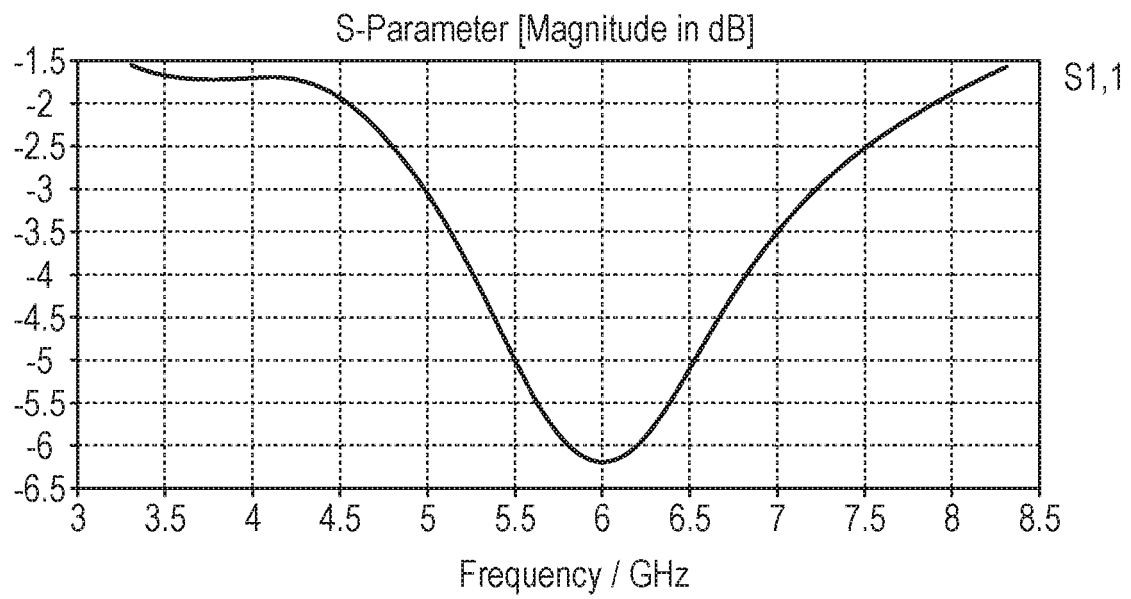


FIG. 4

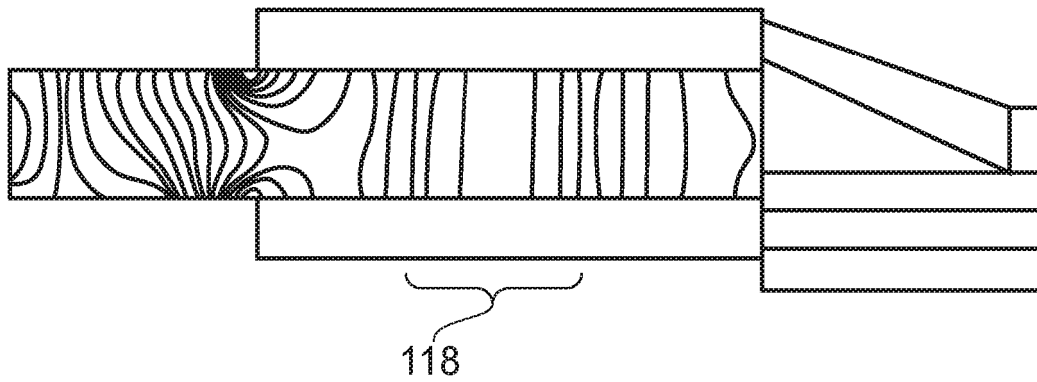


FIG. 5

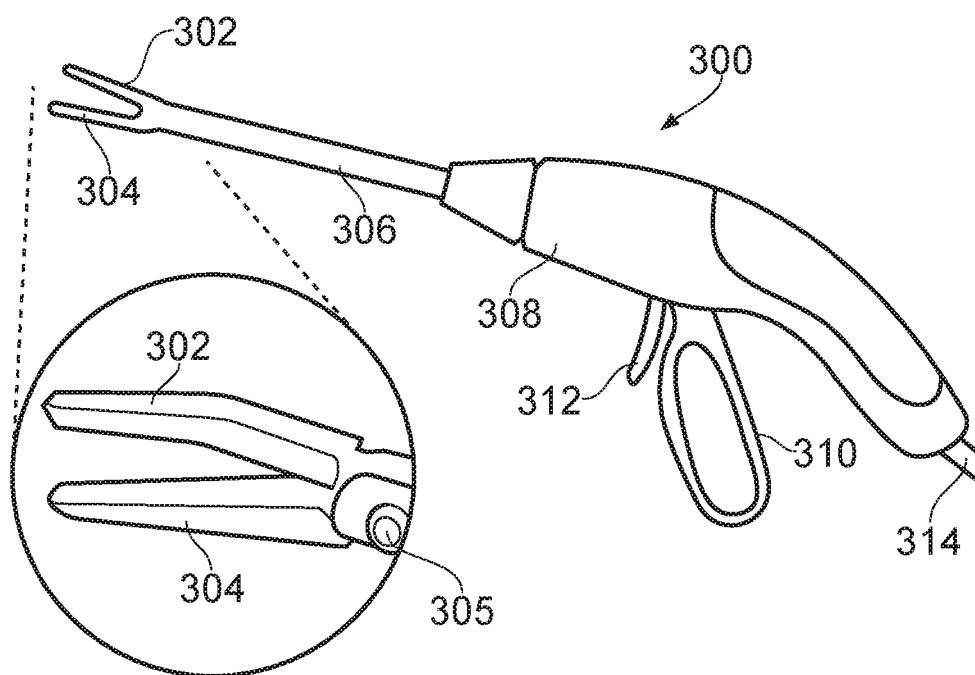


FIG. 6

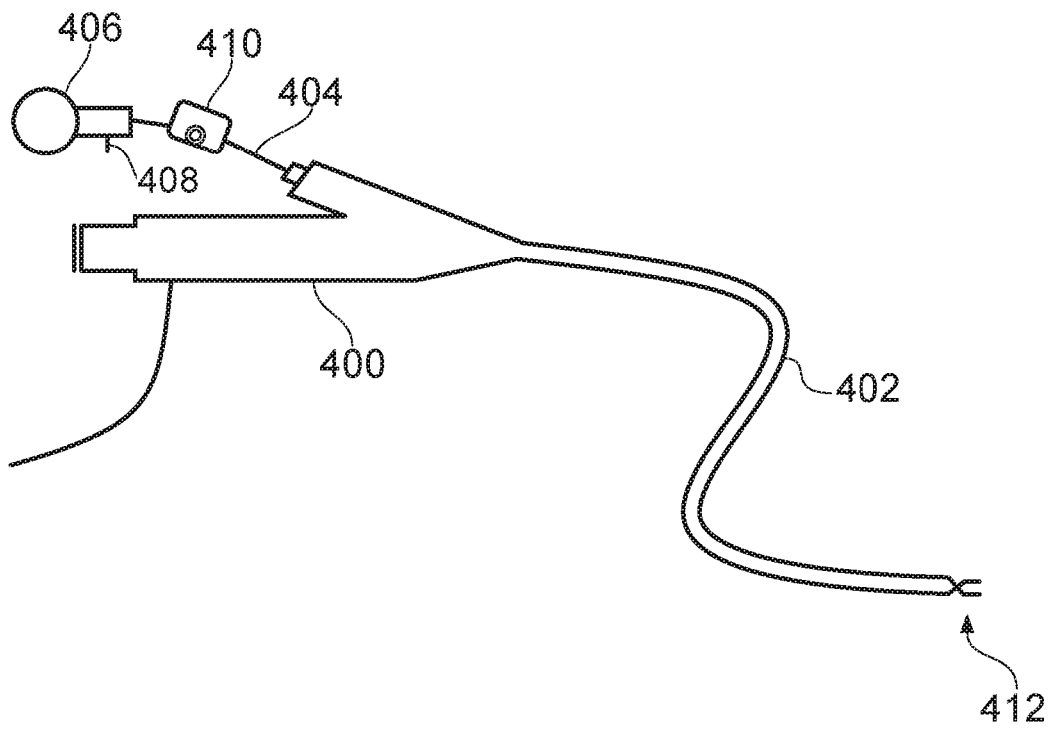


FIG. 7

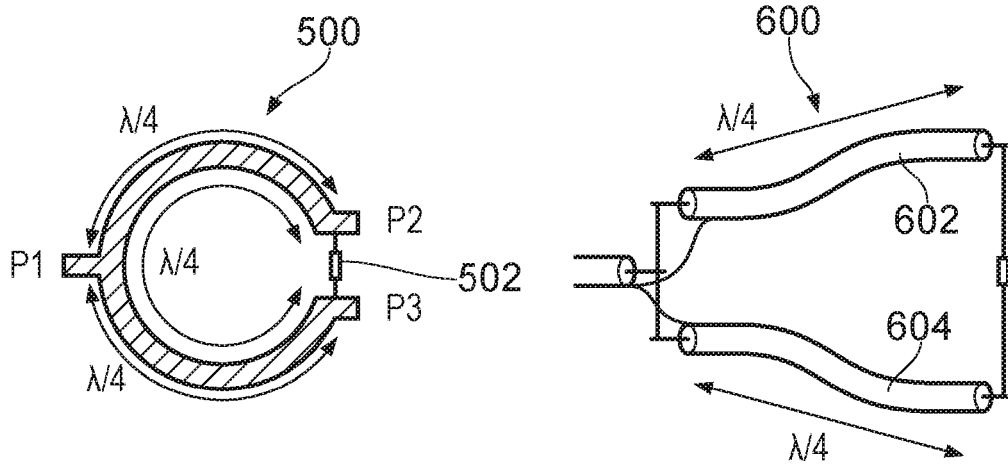


FIG. 8A

FIG. 8B

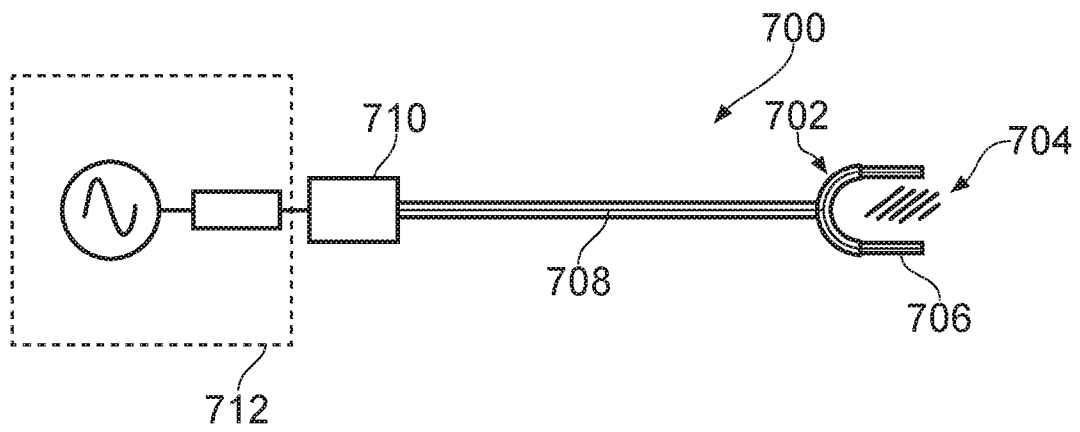


FIG. 9A

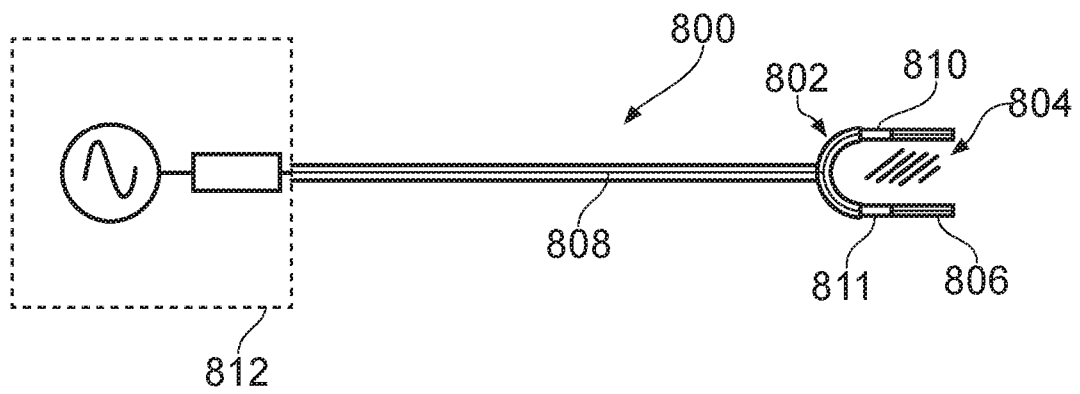


FIG. 9B

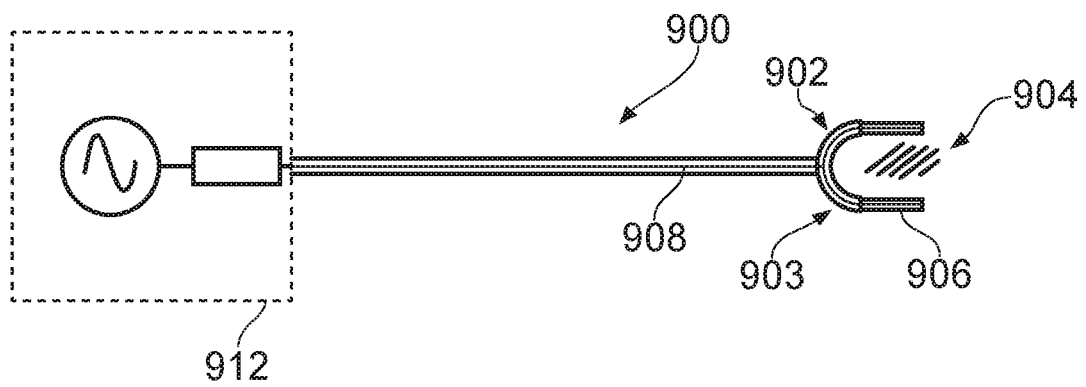


FIG. 9C

REFERENCES CITED IN THE DESCRIPTION

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Patent documents cited in the description

- US 6585735 B [0003]
- EP 2233098 A [0004]
- WO 03020339 A2 [0005]
- WO 2012076844 A [0036]

专利名称(译)	用于从非共振不平衡无损传输线结构传递微波能量的电外科钳		
公开(公告)号	EP3055020B1	公开(公告)日	2019-03-20
申请号	EP2014784349	申请日	2014-10-07
[标]申请(专利权)人(译)	科瑞欧医疗有限公司		
申请(专利权)人(译)	CREO医药有限		
当前申请(专利权)人(译)	CREO医药有限		
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IPC分类号	A61B18/18 A61B18/00		
CPC分类号	A61B18/1815 A61B2018/00404 A61B2018/00482 A61B2018/00589 A61B2018/00595 A61B2018/0063 A61B2018/1861		
代理机构(译)	MEWBURN ELLIS LLP		
优先权	2013017713 2013-10-07 GB		
其他公开文献	EP3055020A1		
外部链接	Espacenet		

摘要(译)

电外科手术钳，用于从位于钳子的钳口内或由钳子的钳口形成的非共振不平衡无损传输线结构将微波能量传递到生物组织中。传输线结构可以通过相对的导电元件形成在钳口元件之间的间隙上，所述导电元件分别电连接到同轴电缆的内导体和外导体。或者，每个钳口元件可以包括其自身的无损传输线，由此使用功率分配器来分配来自同轴电缆的微波能量。钳子可以在胃肠道内窥镜检查或腹腔镜或开放手术中使用。

$$Z_W = \sqrt{2} Z_0$$