



US 20090118615A1

(19) **United States**(12) **Patent Application Publication****Kato et al.**(10) **Pub. No.: US 2009/0118615 A1**(43) **Pub. Date: May 7, 2009**(54) **ULTRASONIC DIAGNOSTIC APPARATUS****Publication Classification**

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(51) **Int. Cl.**
A61B 8/00 (2006.01)
 (52) **U.S. Cl.** 600/438

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(21) Appl. No.: **11/995,993**

(22) PCT Filed: **Jul. 20, 2006**

(86) PCT No.: **PCT/JP2006/314427**

§ 371 (c)(1),
 (2), (4) Date: **Jan. 17, 2008**

(30) **Foreign Application Priority Data**

Jul. 20, 2005 (JP) 2005-210233

ABSTRACT

The present invention aims at providing an ultrasonic diagnostic apparatus capable of displaying a stable spatial distribution of elastic characteristics for each hear beat without depending on the accuracy or stability of measurement of blood pressure and without involvement of measurement of blood pressure.

In an ultrasonic diagnostic apparatus of the present invention, an ultrasonic reflected wave transmitted from an ultrasonic probe 13 and reflected by biomedical tissue is input to a computing section 19 by way of a receiving section 15, a delay time control section 16, a phase detection section 17, and a filter section 18. In accordance with the phase detection signal acquired from the phase detection section 17, the computing section 19 computes a relative elastic characteristic which is an elastic characteristic normalized by an elastic characteristic of an arbitrary reference area in the biomedical tissue. A distribution of relative elastic characteristics computed by the computing section is displayed on a display section 21.

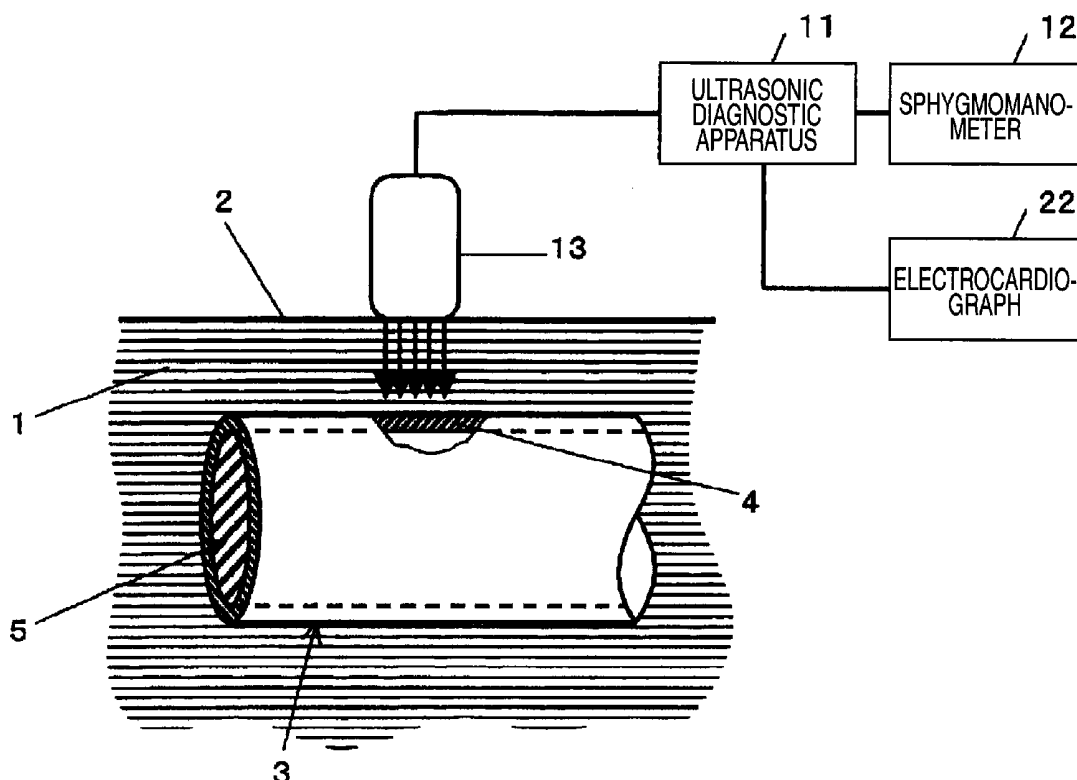


FIG. 1

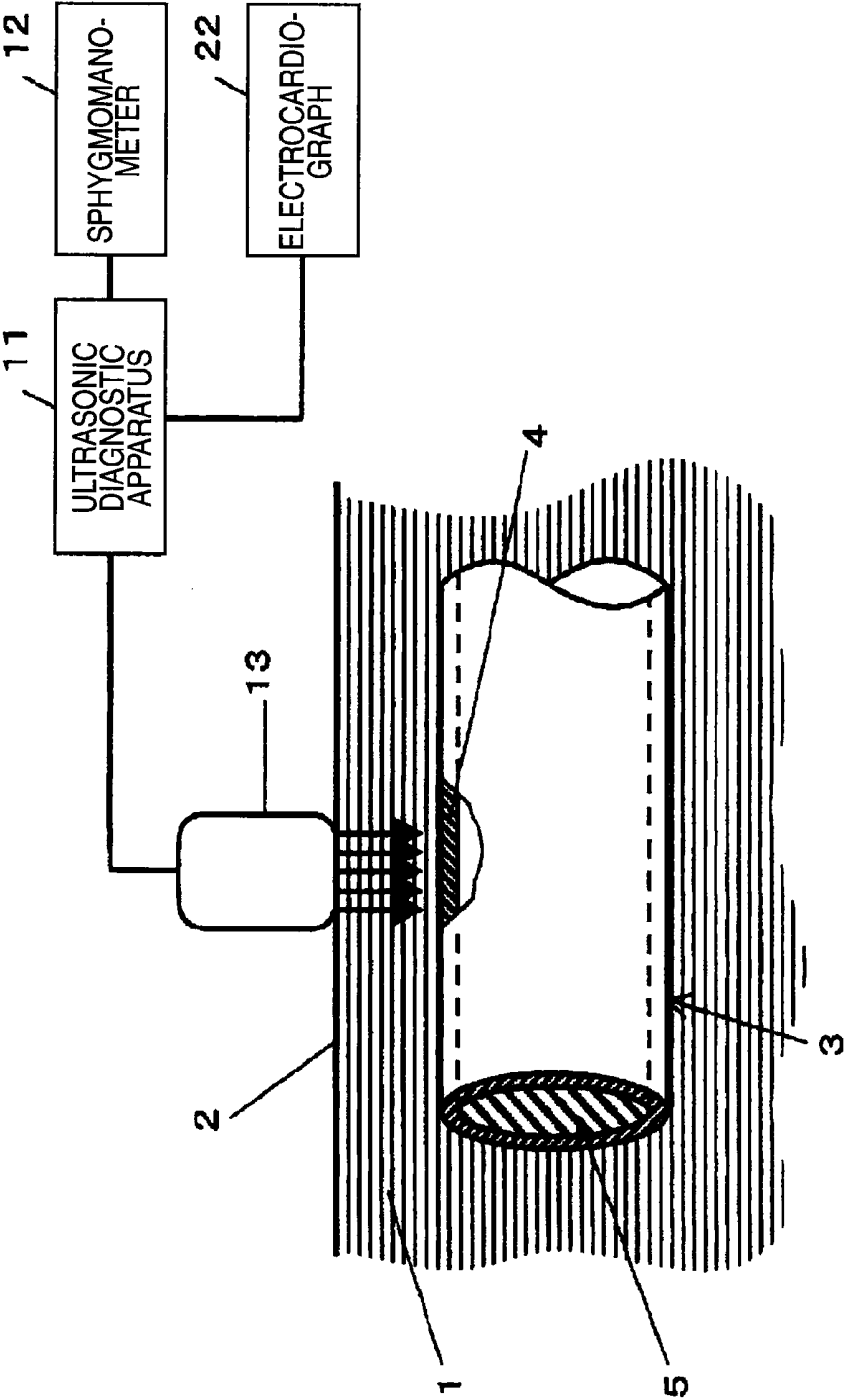


FIG. 2

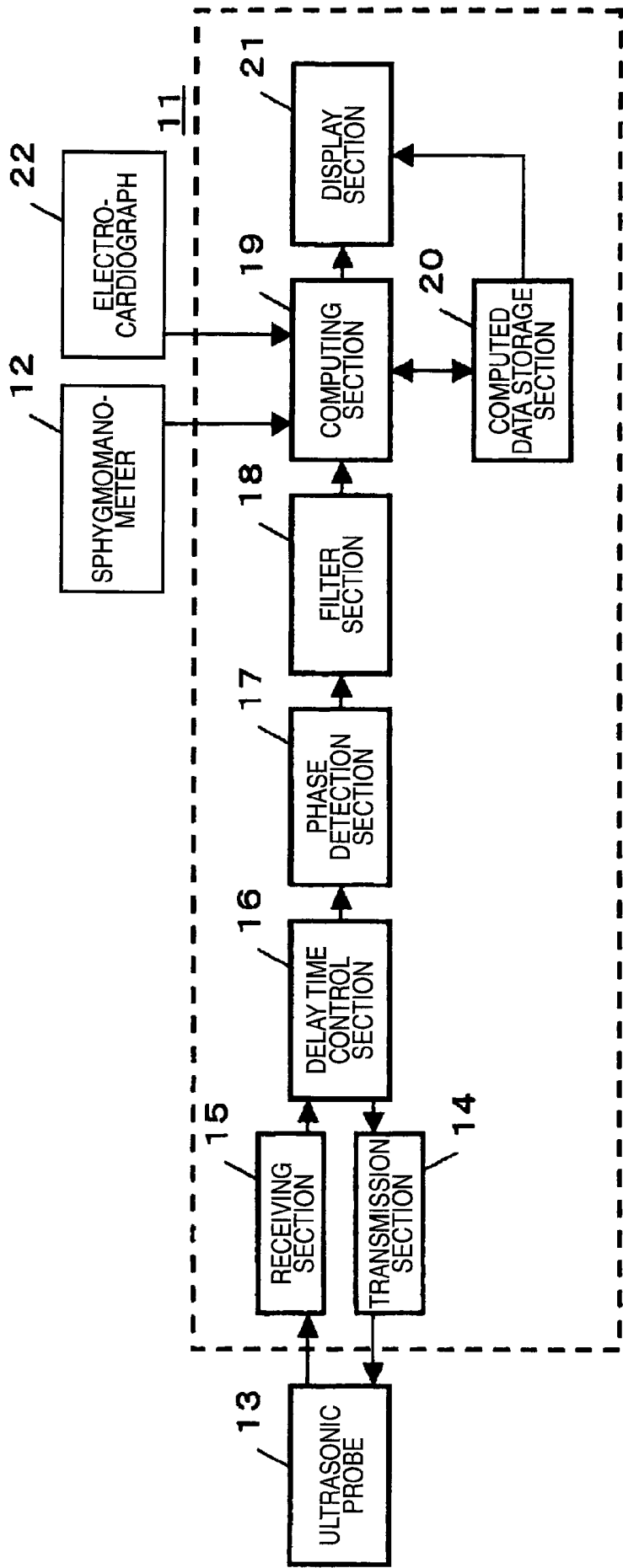


FIG. 3

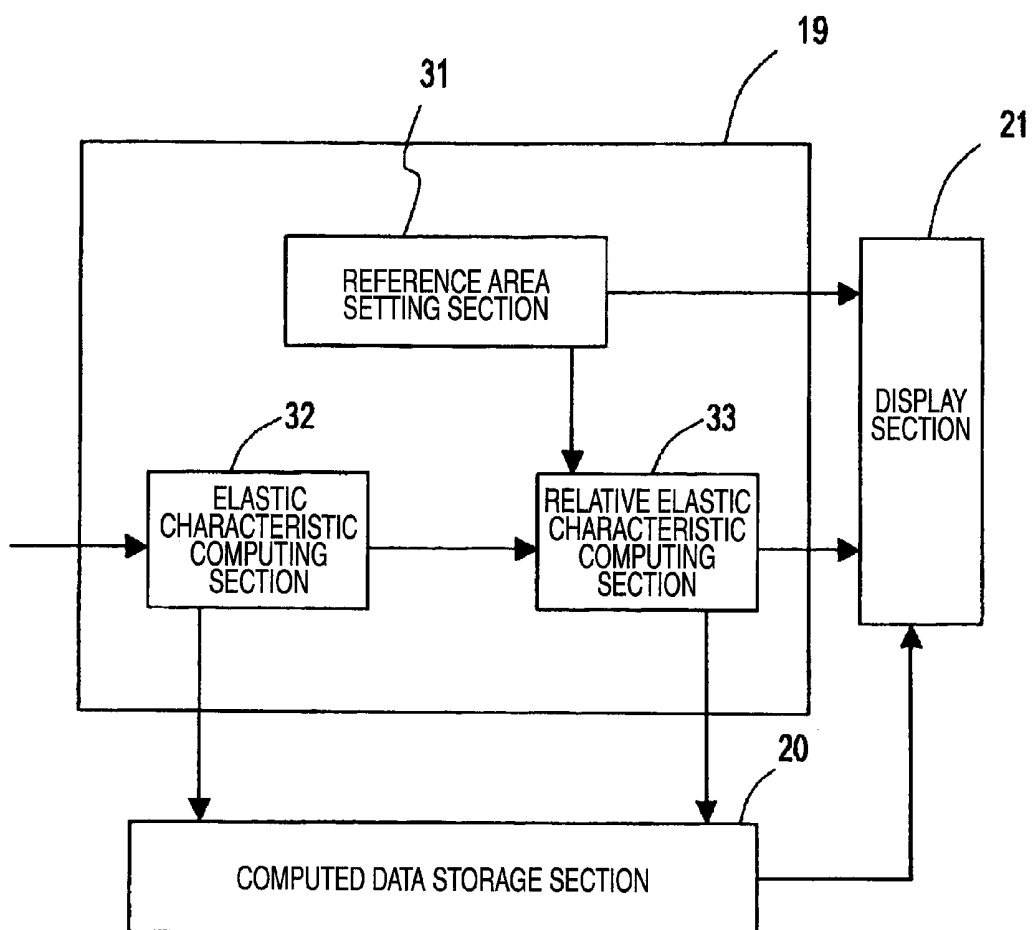


FIG. 4

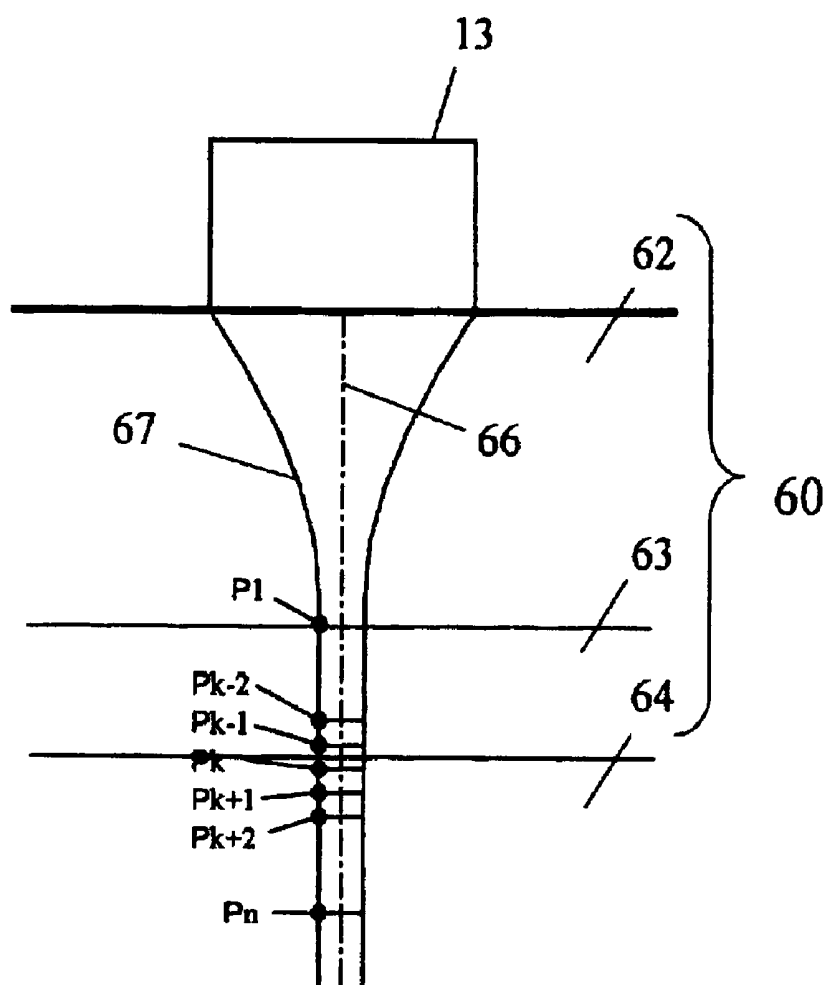


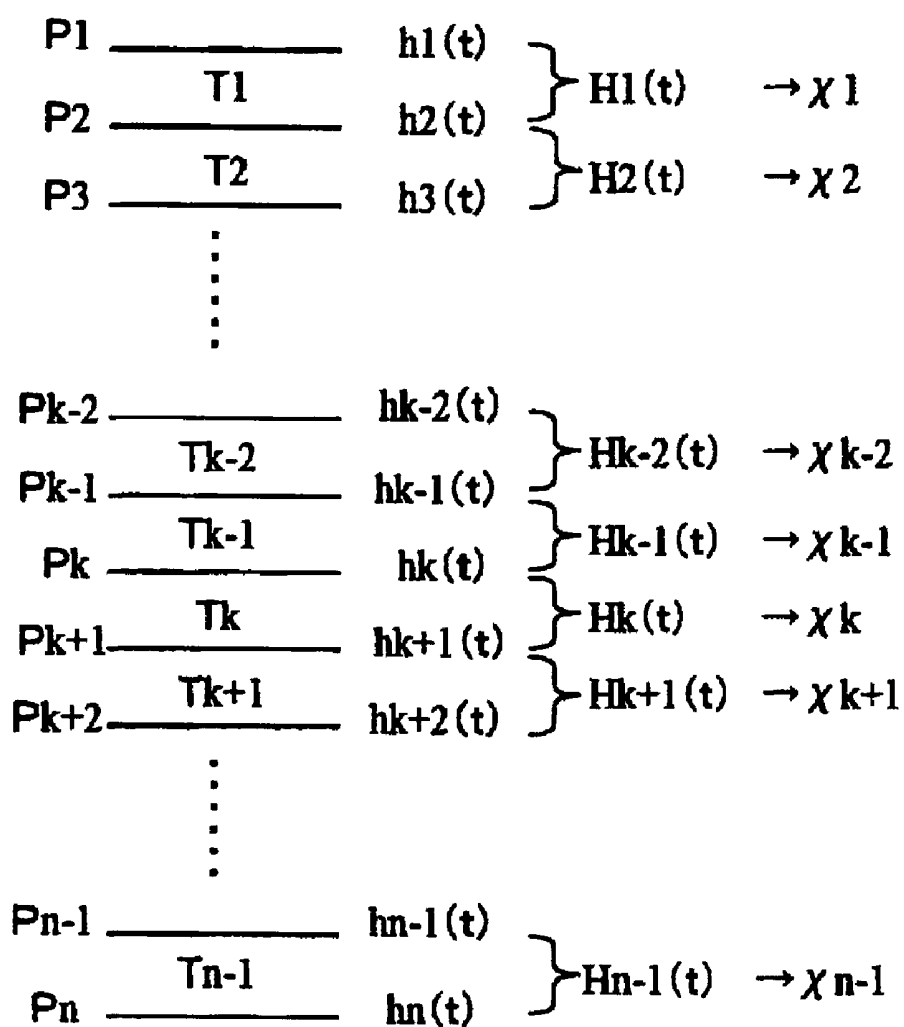
FIG. 5

FIG. 6

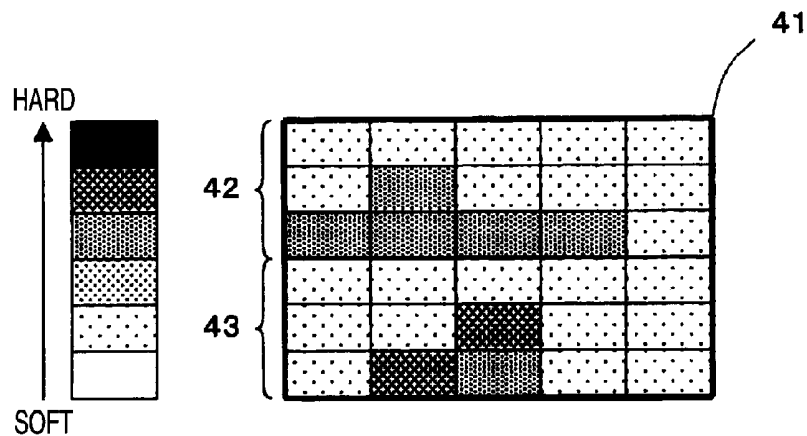


FIG. 7

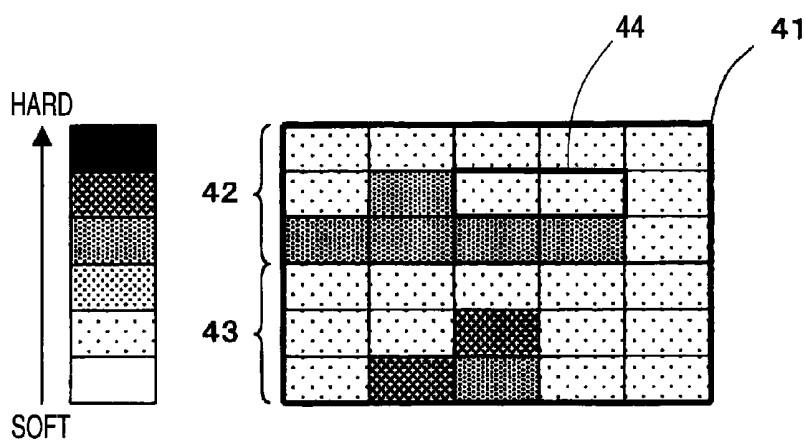
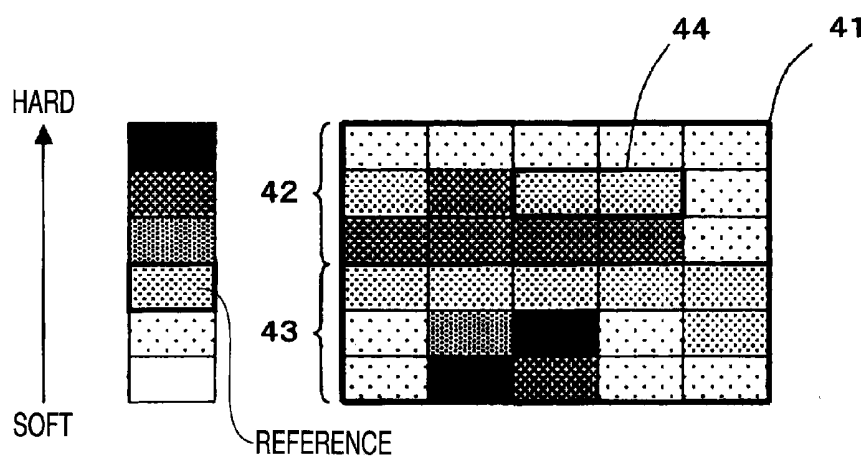


FIG. 8



ULTRASONIC DIAGNOSTIC APPARATUS

TECHNICAL FIELD

[0001] The present invention relates to an ultrasonic diagnostic apparatus for measuring a character of a tissue in a living body, more particularly, an elastic characteristic of a vascular wall tissue.

BACKGROUND ART

[0002] The number of patients suffering from circulatory diseases, such as cardiac infarction or brain infarction, is increasing recently, and prevention and treatment of these diseases has posed a big problem.

[0003] Arterial sclerosis has a close relationship with the onset of cardiac infarction and brain infarction. Specifically, when an atheroma is formed on an arterial wall or when new cells of an arterial wall are created for various reasons, such as high blood pressure, the artery loses elasticity, to thus become hard and fragile. As a result of a blood vessel being closed at a position where the atheroma is formed or a vascular tissue covering the atheroma becoming ruptured, the atheroma flows into the blood vessel, to thus close another location of the artery or rupture a hardened region of the artery. In this way, the diseases are induced. Therefore, early diagnosis of arterial sclerosis becomes important for prevention or treatment of these diseases.

[0004] Manifestation of arterial sclerosis has recently been diagnosed by means of direct observation of an internal state of the blood vessel through use of a vessel catheter. However, this diagnosis involves a problem of a necessity for insertion of a vessel catheter into a blood vessel, thereby imposing heavy load on a subject. Therefore, observation involving the use of the vessel catheter is employed for a subject who is sure to have a lesion into which arterial sclerosis has developed, to thus locate the lesion. This method has never been used as; for example, a test for health care.

[0005] Measurement of a cholesterol level, which is one cause of arterial sclerosis, or a blood pressure level is a test which imposes a small burden on the subject and which can be practiced readily. However, these values do not directly indicate the degree of arterial sclerosis.

[0006] So long as arterial sclerosis can be early diagnosed and a therapeutic medicine for arterial sclerosis can be administered to the subject, the medicine becomes effective for treatment of arterial sclerosis. Once arterial sclerosis has progressed, further progress of arterial sclerosis can be inhibited by the therapeutic medicine. However, complete recovery of a hardened artery is said to be difficult to be made.

[0007] For these reasons, there has been sought a diagnostic method or a diagnostic apparatus which diagnoses arterial sclerosis in its early stage with involvement of a small burden on the subject before it progresses.

[0008] In the meantime, an ultrasonic diagnostic apparatus and an X-ray diagnostic apparatus have heretofore been used as a noninvasive medical diagnostic apparatus which imposes a small burden on the subject. Geometrical information about the inside of a body or information about a chronological change in the internal shape of the body can be acquired without causing pain in the subject by radiation of an ultrasonic wave or an X ray onto the body from the outside. As a result of acquisition of the information about a chronological change in the shape of an object of measurement in the body (i.e., motion information), information about the character of

the object of measurement can be obtained. Specifically, an elastic characteristic of the blood vessel in the body can be determined, and the degree of arterial sclerosis can be ascertained directly. In particular, when compared with the X-ray diagnosis, the ultrasonic diagnosis enables performance of measurement by means of bringing an ultrasonic probe into contact with the subject. Accordingly, the ultrasonic diagnosis is superior because it obviates a necessity for administration of a contrast medium or a risk of X-ray exposure.

[0009] Recent advancement of electronics technology enables remarkable enhancement of the accuracy of measurement of the ultrasonic diagnostic apparatus. In association with this, development of an ultrasonic diagnostic apparatus which measures micromotion of biomedical tissue is in progress. For instance, use of a technique described in Patent Document 1 enables high-precision measurement of a vibrational component of vasomotion whose amplitude is of several microns and which is as fast as several hundreds of hertz, and hence high-precision measurement of a change in the thickness of the vascular wall or the distortion of the wall to an order of microns is reported to become practicable.

[0010] Patent Document 1 discloses a technique for noninvasively measuring a waveform of motion speed of each location in biomedical tissue through use of an ultrasonic wave, thereby determining an elastic modulus of a microarea. Since use of a tissue tracking technique described in Patent Document 1 enables high-precision measurement of vasomotion, a chronological change $h(t)$ in the thickness of an arterial wall can be measured high accuracy. Provided that the thickness of the arterial wall acquired at the time of measurement of low blood pressure is “ h ”; that the maximum amount of change in the thickness of the arterial wall acquired in one cardiac cycle is Δh ; and that pulse pressure is Δp , a radial elastic modulus E of an arterial wall is determined as follows:

$$E = \Delta p \cdot h / \Delta h \quad (\text{Eq. 1})$$

[0011] Use of such a high-precision measurement technique enables detailed measurement of a two-dimensional distribution of elastic characteristics of the arterial wall. For instance, Non-Patent Document 1 describes an example illustration showing a two-dimensional distribution of elastic modulus of a carotid arterial wall superimposed on a B-mode tomogram. The degree of hardness of the arterial wall is not uniform, and the hardness of the arterial wall is present in the form of a certain distribution. Accurately grasping a localized distribution of elastic modulus, which is a feature quantity representing the degree of hardness of an artery, is important for diagnosing arterial sclerosis.

[0012] Patent Document 1: JP-A-10-5226

[0013] Non-Patent Document 1: Hiroshi Kanai et al., “Elasticity Imaging of Atheroma With Transcutaneous Ultrasonic Preliminary Study,” *Circulation*, Vol. 107, pp. 3018 to 3021, 2003.

DISCLOSURE OF THE INVENTION

Problem that the Invention is to Solve

[0014] However, the disclosed technique encounters a problem provided below. In order to determine the elastic modulus E of the arterial wall as indicated by (Eq. 1), the pulse pressure Δp must be measured. Although an elastic modulus determined from the maximum amount of change in thickness achieved during one cardiac cycle can be measured once in one cardiac cycle, actual blood pressure slightly

changes for each heart beat. In order to determine a more accurate elastic modulus, pulse pressure must be measured once in one cardiac cycle. However, a commonly-used intermittent method, typified by a cuff-type sphygmomanometer, cannot determine pulse pressure for each heart beat. Moreover, since a blood flow of the subject is temporarily closed by the cuff-type blood pressure measurement method, the method is unsuitable for long hours of use. Further, according to a continuous method, typified by a tonometer capable of measuring blood pressure for each heart beat, pulse pressure can be measured for each heart beat. However, additional equipment is required, which in turn complicates measurement of an elastic modulus. Another problem of an increase in burden imposed on the subject is also encountered.

[0015] In light of the above, the present invention aims at providing an ultrasonic diagnostic apparatus capable of displaying a stable spatial distribution of elastic characteristics for each heart beat without depending on the accuracy and stability of measurement of blood pressure and without involvement of measurement of blood pressure.

Means for Solving the Problem

[0016] An ultrasonic diagnostic apparatus of the present invention includes:

[0017] a transmission section for driving an ultrasonic probe for transmitting an ultrasonic transmission wave to biomedical tissue;

[0018] a receiving section which amplifies a reflected ultrasonic wave acquired as a result of reflection of the ultrasonic transmission wave from the biomedical tissue and received by the ultrasonic probe, to thus generate a received signal;

[0019] a phase detection section for subjecting the received signal to phase detection;

[0020] a computing section which determines an amount of change in thickness arising at a plurality of positions within the biomedical tissue from a phase detection signal acquired from the phase detection section and which computes a relative elastic characteristic from a value determined by dividing a maximum amount of change in thickness acquired from an arbitrary reference area in the biomedical tissue by a maximum amount of change in thickness acquired from another area; and

[0021] a display section for displaying a distribution of the relative elastic characteristics computed by the computing section. According to the present invention, an accurate, stable distribution of elastic characteristics can be determined without measuring pulse pressure of a subject at all.

[0022] An ultrasonic diagnostic apparatus of the present invention includes:

[0023] a transmission section for driving an ultrasonic probe for transmitting an ultrasonic transmission wave to biomedical tissue;

[0024] a receiving section which amplifies a reflected ultrasonic wave acquired as a result of reflection of the ultrasonic transmission wave from the biomedical tissue and received by the ultrasonic probe, to thus generate a received signal;

[0025] a phase detection section for subjecting the received signal to phase detection;

[0026] a computing section which determines distortions appearing at a plurality of positions within the biomedical tissue from a phase detection signal acquired from the phase detection section and which computes a relative elastic characteristic from a value determined by dividing distortion arising

in an arbitrary reference area in the biomedical tissue by a distortion appearing in another area; and

[0027] a display section for displaying a distribution of the relative elastic characteristics computed by the computing section. According to the present invention, an accurate, stable distribution of elastic characteristics can be determined without measuring pulse pressure of a subject at all.

[0028] An ultrasonic diagnostic apparatus of the present invention includes:

[0029] a transmission section for driving an ultrasonic probe for transmitting an ultrasonic transmission wave to biomedical tissue;

[0030] a receiving section which amplifies a reflected ultrasonic wave acquired as a result of reflection of the ultrasonic transmission wave from the biomedical tissue and received by the ultrasonic probe, to thus generate a received signal;

[0031] a phase detection section for subjecting the received signal to phase detection;

[0032] a computing section which determines elastic characteristics of a plurality of positions within the biomedical tissue from a phase detection signal acquired from the phase detection section and which computes a relative elastic characteristic from a value determined by dividing an elastic characteristic of another area by an elastic characteristic of an arbitrary reference area in the biomedical tissue; and

[0033] a display section for displaying a distribution of the relative elastic characteristics computed by the computing section. According to the present invention, an accurate, stable distribution of elastic characteristics can be determined without depending on the accuracy of measurement of blood pressure of the subject.

[0034] In the ultrasonic diagnostic apparatus of the present invention, the computing section has a reference area setting section for setting the reference area. According to the present invention, an arbitrary area in a spatial elastic characteristic distribution image can be designated, to thus take the designated area as a reference area used for computing a relative elastic characteristic.

[0035] In the ultrasonic diagnostic apparatus, the display section displays the reference area set by the computing section so as to be superimposed on at least one of an ultrasonic tomogram image or an elastic characteristic image. According to the present invention, the reference area can be ascertained without fail, and a diagnosis based on the distribution of elastic characteristics can be performed easily.

[0036] In the ultrasonic diagnostic apparatus, the display section displays positional coordinates of the reference area set by the computing section in the form of numerals. According to the present invention, the reference area can be ascertained without fail, and a diagnosis based on the distribution of elastic characteristics can be performed easily.

[0037] As mentioned above, an ultrasonic diagnostic apparatus of the present invention includes a transmission section for driving an ultrasonic probe for transmitting an ultrasonic transmission wave to biomedical tissue; a receiving section which amplifies a reflected ultrasonic wave acquired as a result of reflection of the ultrasonic transmission wave from the biomedical tissue and received by the ultrasonic probe, to thus generate a received signal; a phase detection section for subjecting the received signal to phase detection; a computing section for computing a relative elastic characteristic, which is a normalized elastic characteristic, from a phase detection signal acquired from the phase detection section; and a display

play section for displaying a distribution of the relative elastic characteristics computed by the computing section.

[0038] According to the present invention, a stable spatial distribution of elastic characteristics can be displayed for each heart beat without depending on the accuracy and without involvement of measurement of blood pressure.

ADVANTAGE OF THE INVENTION

[0039] According to the present invention, an arbitrary area in a spatial elastic characteristic distribution image is designated, and another elastic characteristic is computed as an elastic characteristic ratio while an elastic characteristic value of the area or an average of elastic characteristics is taken as a reference, and the thus-computed ratio is displayed as a spatially-distributed image. As a result, there can be embodied an ultrasonic diagnostic apparatus capable of displaying a stable spatial distribution of elastic characteristics for each heart beat without depending on the accuracy and stability of measurement of blood pressure and without involvement of measurement of blood pressure.

BRIEF DESCRIPTION OF THE DRAWINGS

[0040] FIG. 1 is a view showing a state achieved when a character of a vascular wall tissue is diagnosed by use of an ultrasonic diagnostic apparatus of a first embodiment of the present invention.

[0041] FIG. 2 is a block diagram showing the configuration of the ultrasonic diagnostic apparatus of the first embodiment of the present invention.

[0042] FIG. 3 is a block diagram showing, in detail, the configuration of a computing section in the ultrasonic diagnostic apparatus of the first embodiment of the present invention.

[0043] FIG. 4 is a view schematically showing an ultrasonic beam propagating through a living body when the character of the vascular wall tissue is diagnosed by use of the ultrasonic diagnostic apparatus of the first embodiment of the present invention.

[0044] FIG. 5 is a view showing a relationship between a position of measurement and a tissue, which is an object to be subjected to computation of an elastic characteristic, when the character of the vascular wall tissue is diagnosed by use of the ultrasonic diagnostic apparatus of the first embodiment of the present invention.

[0045] FIG. 6 is a view schematically showing an example distribution of elastic characteristics in a region of interest achieved when the region of interest is set in a portion of a vascular wall in a case where the character of the vascular wall tissue is diagnosed by use of the ultrasonic diagnostic apparatus of the first embodiment of the present invention.

[0046] FIG. 7 is a view schematically showing an example of setting, in the distribution of elastic characteristics in the region of interest, a reference area defining an area where an elastic characteristic serving as a reference is to be determined, when the character of the vascular wall tissue is diagnosed by use of the ultrasonic diagnostic apparatus of the first embodiment of the present invention.

[0047] FIG. 8 is a view schematically showing an example distribution of a relative elastic characteristic which is determined by normalization of respective elastic characteristics in the region of interest through use of the reference elastic characteristic, when the character of the vascular wall tissue is

diagnosed by use of the ultrasonic diagnostic apparatus of the first embodiment of the present invention.

DESCRIPTIONS OF THE REFERENCE NUMERALS

- [0048] 1 EXTRAVASCULAR TISSUE
- [0049] 2 BODY SURFACE
- [0050] 3 BLOOD VESSEL
- [0051] 4 VASCULAR ANTERIOR WALL
- [0052] 5 BLOOD
- [0053] 11 ULTRASONIC DIAGNOSTIC APPARATUS
- [0054] 12 SPHYGMOMANOMETER
- [0055] 13 ULTRASONIC PROBE
- [0056] 14 TRANSMISSION SECTION
- [0057] 15 RECEIVING SECTION
- [0058] 16 DELAY TIME CONTROL SECTION
- [0059] 17 PHASE DETECTION SECTION
- [0060] 18 FILTER SECTION
- [0061] 19 COMPUTING SECTION
- [0062] 20 COMPUTED DATA STORAGE SECTION
- [0063] 21 DISPLAY SECTION
- [0064] 22 ELECTROCARDIOGRAPH
- [0065] 31 REFERENCE AREA SETTING SECTION
- [0066] 32 ELASTIC CHARACTERISTIC COMPUTING SECTION
- [0067] 33 RELATIVE ELASTIC CHARACTERISTIC COMPUTING SECTION
- [0068] 41 REGION OF INTEREST
- [0069] 42 ADVENTITIA
- [0070] 43 INTIMA-MEDIA COMPLEX
- [0071] 44 REFERENCE AREA
- [0072] 60 LIVING BODY
- [0073] 62 BIOMEDICAL TISSUE
- [0074] 63 VASCULAR WALL
- [0075] 64 BLOOD
- [0076] 66 ACOUSTIC LINE
- [0077] 67 ULTRASONIC BEAM
- [0078] Embodiments of the present invention will be described hereunder by reference to the drawings.

First Embodiment

[0079] FIG. 1 is a view showing a state achieved when a character of a vascular wall tissue is diagnosed by use of an ultrasonic diagnostic apparatus 11 of a first embodiment of the present invention. An ultrasonic probe 13 connected to the ultrasonic diagnostic apparatus 11 is set so as to come into intimate contact with a body surface 2 of a subject and transmits an ultrasonic wave into an extra vascular tissue 1. The transmitted ultrasonic wave undergoes reflection and scattering on a blood vessel and blood 5; a portion of reflected and scattered waves returns to the ultrasonic probe 13; and the thus-returned wave is received as an echo (a reflected ultrasonic wave). The ultrasonic diagnostic apparatus 11 analyzes and computes a received signal, to thus determine geometrical information and motion information about a vascular anterior wall 4. The ultrasonic diagnostic apparatus 11 is also connected to a sphygmomanometer 12 and an electrocardiograph 22, and blood pressure data pertaining to the subject measured by the sphygmomanometer 12 and an electrocardiographic waveform measured by the electrocardiograph 22 are input to the ultrasonic diagnostic apparatus 11.

[0080] According to a method described in; for example, Patent Document 1, the ultrasonic diagnostic apparatus 11

uses both an amplitude and a phase of a detection signal acquired by detection of a received ultrasonic wave signal, thereby determining an instantaneous position of an object by means of a limited least square method. The thickness of a microarea in the vascular anterior wall **4** and the amount of a chronological change in thickness can be measured with sufficient accuracy by means of high-precision phase tracking (the measurement accuracy of an amount of positional change is ± 0.2 microns). Moreover, an elastic characteristic of the microarea in the vascular anterior wall **4** by use of the blood pressure data acquired from the sphygmomanometer **12**. Further, the electrocardiographic waveform measured by the electrocardiograph **22** is used as a trigger signal for determining timing for acquisition of data or resetting data. The electrocardiograph **22** can be replaced with a cardiometer or an arterial pulse wave detector which serves as another biomedical signal detection means, and a cardiac sound waveform or an arterial pulse waveform can also be used in place of the electrocardiographic waveform. Moreover, use of a waveform pertaining to the amount of motion or a waveform pertaining to the amount of change in thickness, which is measured by the ultrasonic diagnostic apparatus **11**, obviates a necessity for inputting a trigger signal from the outside.

[0081] The configuration and operation of the ultrasonic diagnostic apparatus **11** will now be described in detail. FIG. 2 is a block diagram showing the configuration of the ultrasonic diagnostic apparatus **11**. The ultrasonic diagnostic apparatus **11** has a transmission section **14**, a receiving section **15**, a delay time control section **16**, a phase detection section **17**, a filter section **18**, a computing section **19**, a computed data storage section **20**, and a display section **21**. These sections are controlled by means of an unillustrated computer.

[0082] The transmission section **14** generates a predetermined drive pulse signal which drives the ultrasonic probe **13**, and outputs the thus-generated signal to the ultrasonic probe **13**. An ultrasonic transmission wave transmitted from the ultrasonic probe **13** driven by the drive pulse signal undergoes reflection and scattering on biomedical tissue, such as the blood vessel **3**, and a resultant reflected ultrasonic wave is received by the ultrasonic probe **13**. The frequency of the drive pulse used for generating an ultrasonic wave is determined such that a preceding ultrasonic pulse and a subsequent ultrasonic pulse, which are adjacent to each other along a time axis, do not overlap each other, in consideration of the depth of an object of measurement and the acoustic velocity of the ultrasonic wave.

[0083] The receiving section **15** amplifies the reflected ultrasonic wave received by the ultrasonic probe **13**, to thus generate a received signal. The receiving section **15** includes an amplification section and an A/D conversion section (neither of these sections are illustrated); amplifies the reflected ultrasonic wave; and converts the amplified wave further into a digital signal. The transmission section **14** and the receiving section **15** are built from an electronic component or the like.

[0084] The delay time control section **16** is connected to the transmission section **14** and the receiving section **15**, and controls a delay time of a drive pulse signal imparted from the transmission section **14** to a group of ultrasonic transducers of the ultrasonic probe **13**. As a result, the direction of an acoustic line of an ultrasonic beam of the ultrasonic transmission wave transmitted from the ultrasonic probe **13** and a focal depth of the ultrasonic beam are changed. An aperture diameter or the position of a focal point can be changed by means

of controlling the delay time of the received signal which is received by the ultrasonic probe **13** and which is generated by the receiving section **15**. An output from the delay time control section **16** is input to the phase detection section **17**.

[0085] The phase detection section **17** subjects the received signal delay-controlled by the delay time control section **16** to phase detection, thereby generating a phase detection signal including an actual-section signal and an imaginary-section signal. The phase detection signal is input to a filter section **18**. The filter section **18** eliminates high-frequency components, components reflected from substances other than the object of measurement, noise components, and the like. The phase detection section **17** and the filter section **18** can also be formed from software or hardware.

[0086] The actual-section signal and the imaginary-section signal of the phase detection signal passed through the filter section **18** are input to the computing section **19**. FIG. 3 is a block diagram showing a detailed configuration of the computing section **19**. The computing section **19** includes a reference area setting section **31**, an elastic characteristic computing section **32**, and a relative elastic characteristic computing section **33**. The computing section **19** can also be formed from software or hardware.

[0087] The elastic characteristic computing section **32** computes, from the actual-section signal and the imaginary-section signal of the phase detection signal, the motion speed of the biomedical tissue achieved at a plurality of points of measurement and integrates the motion speed, thereby determining the amount of movement (chronological displacements of respective points of measurement). The amount of change in the thickness of the biomedical tissue (the amount of expansion and contraction) among the points of measurement is determined from the thus-determined amount of movement. Information about one cardiac cycle is received from the electrocardiograph **22**, the maximum amount of change in thickness—a difference between the maximum amount of change in thickness and the minimum amount of change in thickness acquired during one cardiac cycle—and the maximum thickness are determined. Distortion of the biomedical tissue is determined from the maximum amount of change in thickness and the maximum thickness, and an elastic characteristic of the biomedical tissue located between the respective points of measurement is determined by use of blood pressured at a acquired from the sphygmomanometer **12**.

[0088] The thus-determined elastic characteristic of the biomedical tissue is mapped in correspondence to a measurement area, and the mapping is output to the display section **21** as a spatially-distributed image acquired during each cardiac cycle. When an operator of the ultrasonic diagnostic apparatus **11** has not caused the reference area setting section **31** to set a reference area, the relative elastic characteristic computing section **33** performs no processing. Processing performed when the reference area setting section **31** is caused to set a reference area will be described later.

[0089] These computing operations performed by the computing section **19** will be described in a further detailed manner by reference to FIGS. 4 and 5. FIG. 4 schematically shows an ultrasonic beam **67** propagating through a living body **60**. FIG. 4 shows biomedical tissue **62**, a vascular wall **63**, and blood **64** other than the blood vessel. An ultrasonic transmission wave transmitted from the ultrasonic probe **13** located on the surface of the living body **60** propagates through the living body **60**. The ultrasonic transmission wave propagates

through the living body 60 as the ultrasonic beam 67 having a certain finite width. During the course of propagation of the beam, the ultrasonic beam undergoes reflection or scattering on the vascular wall 63, the blood 64, and the like, and a portion of the reflected or scattered ultrasonic wave returns to the ultrasonic probe 13 and is received as a reflected ultrasonic wave. The reflected ultrasonic wave is detected as a discrete time-series signal $r_k(t)$. As the reflected time-series signal is acquired from a tissue closer to the ultrasonic probe 13, the signal is located closer to the point of origin along the time axis. The width (beam size) of the ultrasonic beam 67 can be controlled by means of changing a delay time.

[0090] At the time of commencement of measurement, a plurality of points of measurement P_n ($P_1, P_2, P_3, \dots, P_k, \dots, P_n$, where “n” is a natural number of three or more) located along an acoustic line 66 that is a center axis of the ultrasonic beam are arranged at given intervals L in sequence of $P_1, P_2, P_3, \dots, P_k, \dots, P_n$ from the ultrasonic probe 13. The phase detection section 17 subjects the reflected wave signal $r_k(t)$ to orthogonal detection by use of a predetermined detection frequency, thereby determining a detection signal $R_k(t)$ consisting of an actual-section signal and an imaginary-section signal, and the thus-determined signal is caused to pass through the filter section 18. Under the constraint that the amplitude of the detection signal $R_k(t)$ and the amplitude of a detection signal $R_k(t+\Delta t)$ acquired after elapse of a minute time Δt remain unchanged and that only the phase of the signal and a reflection point change, the elastic characteristic computing section 32 of the computing section 19 performs correlation computation of the detection signal $R_k(t)$ and $R_k(t+\Delta t)$, and a correlation signal $Q_k(t)$ of the position P_k is determined by (Eq. 2).

$$Q_k(t) = R_k(t+\Delta t) \times R_k^*(t) \quad (* \text{ designates a complex conjugate}) \quad (\text{Eq. 2})$$

[0091] An angle $\theta_k(t)$ formed from an actual section and an imaginary section of the correlation signal $Q_k(t)$ is determined, and a chronological change in a point of measurement P_k ; that is, the amount of movement $h_k(t)$ of the position P_k , is determined from the angle $\theta_k(t)$.

[0092] FIG. 5 shows a relationship between the point of measurement P_n and tissue T_n which is an object of elastic characteristic computation. The tissue T_n is situated at a position sandwiched between adjacent points of measurement P_k and P_{k+1} while assuming a thickness L. (n-1) target tissues $T_1 \dots T_{n-1}$ are defined on the basis of “n” points of measurement $P_1 \dots P_n$.

[0093] An amount of change $H_k(t)$ which is the amount of expansion and contraction of the target tissue T_k is determined as $H_k(t) = h_{k+1}(t) - h_k(t)$ from the points of measurement P_k and P_{k+1} and amounts of movement $h_k(t)$ and $h_{k+1}(t)$.

[0094] A change in the thickness of the tissue T_k of the vascular wall 63 arises according to a change in blood pressure caused by a heart rate and is iterated essentially in synchronism with the cardiac cycle. Consequently, the elastic characteristic is preferably determined as a numeral for each cardiac cycle in synchronism with the cardiac cycle. The maximum value and the minimum value are extracted from the amount of change $H_k(t)$ in thickness achieved during one cardiac cycle, and a difference between the maximum value and the minimum value is taken as the maximum amount of change in thickness ΔH_k . A difference between the maximum blood pressure and the minimum blood pressure is taken as pulse pressure Δp . When the maximum value (or an initial value) of the thickness of the target tissue is taken as H_m, H_m

is expressed as $L \times \{(k+1) - k\} = L$, and hence a distortion s_k and an elastic characteristic χ_k can be determined by (Eq. 3) and (Eq. 4).

$$S_k = \Delta H_k / H_m = \Delta H_k / L \quad (\text{Eq. 3})$$

$$\chi_k = \Delta p / S_k = \Delta p \cdot H_m / \Delta H_k \quad (\text{Eq. 4})$$

[0095] The number of points of measurement P_n and an interval between the points of measurement can be set arbitrarily in accordance with a characteristic of living tissue which is an objective of measurement or a target of measurement.

[0096] The following problem exists in the elastic characteristic which is determined by the above-mentioned method and which is displayed on the display section 21. The elastic characteristic is determined by means of dividing the pulse pressure Δp by the distortion S_k , and pulse pressure must be measured for each heart beat in order to determine an accurate elastic characteristic. In general, many subjects have essentially-constant pulse pressure. Handling the pulse pressure measured immediately before measurement of an elastic characteristic as being non-changing for several minutes to several tens of minutes is very preferable in terms of ease of measurement. However, for instance, when the pulse pressure of the subject is unstable for each heart beat, measurement of pulse pressure for each heart beat is required. Use of a tonometer, or the like, enables measurement of pulse pressure measured for each heart beat, but raises a problem of a necessity for another device or complication of a measurement system.

[0097] A technique for solving the problem will be described in detail hereunder. FIG. 6 is a view schematically showing the distribution of elastic characteristics in the region of interest when the region of interest 41 is set in a portion on the vascular wall. The region of interest 41 is set so as to simultaneously include an adventitia 42 of the vascular wall and an intima-media complex 43, and elastic characteristic values of respective microareas determined by the computing section 19 are coded according to a preset color scheme, whereby a spatially-distributed image is formed.

[0098] FIG. 7 is a view schematically showing that a reference area 44 defining an area where an elastic characteristic taken as a reference is set in the distribution of elastic characteristics shown in FIG. 6. The operator of the ultrasonic diagnostic apparatus 11 can arbitrarily determine the size and position of the reference area 44. Specifically, it is desirable that the reference area should be set at a position on the adventitia 42 or in the intima-media complex 43 of the subject which has been diagnosed by the operator as a healthy area. Although the reference area 44 is set on the adventitia 42 in FIG. 7, the reference area 44 may also be provided on the intima-media complex 43. The elastic characteristic values achieved within the reference area 44 are averaged, and a resultant average is taken as a reference elastic characteristic χ_s .

[0099] FIG. 8 is a view schematically showing the distribution of relative elastic characteristics determined by normalization (normalizing operation) of the respective elastic characteristics acquired within the region of interest 41 by means of the reference elastic characteristic χ_s . Arbitrary elastic characteristics χ_k acquired within the region of interest 41 are divided by the reference elastic characteristic χ_s . Namely, χ_k / χ_s is determined, and a result is taken as a relative elastic characteristic χ_k' . The respective relative elastic characteristics χ_k' are coded in accordance with a predetermined color scheme, to thus generate a spatially-distributed image.

So long as the same pulse pressure Δp is used for determining the reference elastic characteristic χ_s and the elastic characteristic χ_k , the influence of the pulse pressure Δp is canceled during computation of the relative characteristic $\chi_k' = \chi_k / \chi_s$. Resultantly, the relative elastic characteristic χ_k' does not depend on a change or error in pulse pressure Δp , and a relative distribution of hardness and softness compared with the healthy area can be determined accurately, stably.

[0100] Operation of the ultrasonic diagnostic apparatus **11** performed when the relative elastic characteristic is determined will be described by reference to FIG. 3. The operator finds a healthy area from an image pertaining to the distribution of elastic characteristics appearing on the display section **21**, and activates the reference area setting section **41**, to thus set the reference area **44** such as that shown in FIG. 7. Setting is performed by way of an interface section (not shown) of the ultrasonic diagnostic apparatus **11**. The reference area setting section **31** sends reference area information specified by the operator to the relative elastic characteristic computing section **33**. The relative elastic characteristic computing section **33** first determines an elastic characteristic χ_s in the reference area by use of the elastic characteristic χ_k sent from the elastic characteristic computing section **32**, and subsequently determines the relative elastic characteristic χ_k' . The relative elastic characteristic χ_k' is output as a spatially-distributed image to the display section **21**, as well as being stored in the computed data storage section **20**. It is desirable that the reference area setting section **31** should send the reference position information to the display section **21** so that the operator can set the reference area **44** at an arbitrary position while viewing the display section **21**, to thus display the reference position information. Now, although a display of the reference area **44** is preferably displayed so as to be superimposed on a B-mode tomogram or an elastic characteristic image, positional coordinates of the reference area **44** may also be displayed as numerals.

[0101] As mentioned above, even when the pulse pressure of the subject is unstable or measurement of pulse pressure performed for each heart beat is inaccurate, an accurate, stable distribution of elastic characteristics can be determined by performing computation described in connection with the embodiment for each heart beat. Moreover, an accurate, stable distribution of elastic characteristics can be determined without measurement of pulse pressure for each heart beat.

[0102] Although the relative elastic characteristic is determined as $\chi_k' = \chi_k / \chi_s$ in the present embodiment, it may also be possible to arbitrarily set a constant A and a constant B provided that $\chi_k' = A \times (\chi_k / \chi_s) + B$, so long as the setting falls within the scope of gist of the present invention.

[0103] It is desirable that the reference area **44** should be set in the middle of measurement of an elastic characteristic. However, even when data stored in the computed data storage section **20** are read after completion of measurement, to thus display an image, and when setting is performed in that state, an analogous advantage is yielded.

[0104] It is desirable that the reference area **44** should be set manually by way of the interface section of the ultrasonic diagnostic apparatus **11** after the operator has determined whether or not tissue is healthy. However, for instance, an adventitia located in the region of interest **41** maybe extracted by means of an automatic adventitia extraction function, and the thus-extracted membrane may also be set as the reference area **44**.

[0105] Moreover, when the operator has determined that a healthy area is not present within the region of interest **41**, an elastic characteristic of the same area acquired in the past or an elastic characteristic of another region (a region other than the region of interest **41**) may also be used. In this case, however, a difference exists between the times when the areas which are objects of comparison have been measured, and hence attention must be paid to the possibility of occurrence of a change in pulse pressure.

Second Embodiment

[0106] A second embodiment of the present invention will now be described. The ultrasonic diagnostic apparatus of the second embodiment has the analogous structure and function as the structure and function of the ultrasonic diagnostic apparatus **11** of the first embodiment excluding the function of the computing section **19**. The same reference numerals are used unless otherwise particularly explained.

[0107] As described in connection with the first embodiment, the computing section **19** first determines the amount of change in thickness $H_k(t)$ of a plurality of micro-biomedical tissues T_k which are objects of measurement, and determines the maximum amount of change ΔH_k in thickness from the thus-determined amount of change. Next, a distortion S_k is computed from the maximum thickness (or initial value) H_m and ΔH_k of the target tissue, thereby computing the elastic characteristic χ_k from the distortion S_k and the pulse pressure Δp . A relative elastic characteristic $\chi_k' = \chi_k / \chi_s$ by use of the predetermined reference elastic characteristic χ_s .

[0108] The relative elastic characteristic χ_k' can also be determined as shown in (Eq. 5), provided that an average value of distortion acquired in the reference area **44** is taken as reference distortion S_s .

$$\chi_k' = \chi_k / \chi_s = (\Delta p / S_k) / (\Delta p / S_s) = S_s / S_k \quad (\text{Eq. 5})$$

[0109] (Eq. 5) shows that the pulse pressure Δp does not need to be measured during computation of the relative elastic characteristic χ_k' . Specifically, even in the case of a subject who has unstable pulse pressure Δp and when the pulse pressure Δp is not measured at all, an accurate, stable distribution of relative elastic characteristics can be determined.

[0110] Moreover, the relative elastic characteristic χ_k' can also be expressed as (Eq. 6) when an average of amounts of maximum changes in thickness acquired within the reference area **44** is taken as a reference maximum thickness change level ΔH_s .

$$\chi_k' = S_s / S_k = (\Delta H_s / H_m) / (\Delta H_k / H_m) = \Delta H_s / \Delta H_k \quad (\text{Eq. 6})$$

[0111] Although, in the present embodiment, the relative elastic characteristic χ_k' is determined by use of (Eq. 5) and (Eq. 6), $\chi_k'' = A \times \chi_k' + B$ (A and B are constants which are arbitrarily set) may also be computed, to thus utilize χ_k'' , so long as utilization of χ_k'' falls within the scope of gist of the present invention. In particular, the elastic characteristic χ_k can be determined without determination of the elastic characteristic χ_k by means of using the reference elastic characteristic χ_s for the constant A and 0 for the constant B, so long as the maximum amount of change in thickness ΔH_k and the distortion S_k are determined. The reference elastic characteristic χ_s may also be an actually-measured value or a general value, or the like, acquired from an area, such as an adventitia, where an individual different is less likely to arise.

[0112] As described above, computation described in connection with the second embodiment is performed for each

hear beat, whereby an accurate, stable distribution of elastic characteristics can be measured without measuring pulse pressure of the subject at all.

[0113] Although the present invention has been described in detail by reference to the specific embodiments, it is manifest to persons skilled in the art that the present invention is susceptible to various alterations or modifications without departing from the spirit and scope of the present invention.

[0114] The present invention is based on Japanese Patent Application (JP-A-2005-210233) filed on Jul. 20, 2005 in Japan, the contents of which are hereby incorporated by reference.

INDUSTRIAL APPLICABILITY

[0115] The ultrasonic diagnostic apparatus of the present invention can be utilized for an ultrasonic diagnostic apparatus, or the like, capable of displaying a stable spatial distribution of elastic characteristics for each hear beat without depending on the accuracy or stability of measurement of blood pressure and without involvement of measurement of blood pressure.

1. An ultrasonic diagnostic apparatus for diagnosing a blood vessel by an ultrasonic wave comprising:

a transmission section for driving an ultrasonic probe for transmitting an ultrasonic transmission wave to biomedical tissue;

a receiving section which amplifies a reflected ultrasonic wave acquired as a result of reflection of the ultrasonic transmission wave from the biomedical tissue and received by the ultrasonic probe, to thus generate a received signal;

a phase detection section for subjecting the received signal to phase detection;

a computing section which determines an amount of change in thickness arising at a plurality of positions within the biomedical tissue from a phase detection signal acquired from the phase detection section and which computes a relative elastic characteristic from a value determined by dividing a maximum amount of change in thickness acquired from an arbitrary reference area in the biomedical tissue by a maximum amount of change in thickness acquired from another area; and

a display section for displaying a distribution of the relative elastic characteristics computed by the computing sections

wherein the maximum amount of change in thickness acquired from the arbitrary reference area in the biomedical tissue is a maximum amount of change in thickness acquired from an area of an adventitia in the blood vessel or a maximum amount of change in thickness acquired in the past from an arbitrary reference area.

2. An ultrasonic diagnostic apparatus for diagnosing a blood vessel by an ultrasonic wave, comprising:

a transmission section for driving an ultrasonic probe for transmitting an ultrasonic transmission wave to biomedical tissue;

a receiving section which amplifies a reflected ultrasonic wave acquired as a result of reflection of the ultrasonic transmission wave from the biomedical tissue and received by the ultrasonic probe, to thus generate a received signal;

a phase detection section for subjecting the received signal to phase detection;

a computing section which determines distortions appearing at a plurality of positions within the biomedical tissue from a phase detection signal acquired from the phase detection section and which computes a relative elastic characteristic from a value determined by dividing distortion arising in an arbitrary reference area in the biomedical tissue by a distortion appearing in another area; and

a display section for displaying a distribution of the relative elastic characteristics computed by the computing section,

wherein the distortion arising in the arbitrary reference area is a distortion arising in an area of an adventitia in the blood vessel or a distortion acquired in the Past from an arbitrary reference area.

3. An ultrasonic diagnostic apparatus for diagnosing a blood vessel by an ultrasonic wave, comprising:

a transmission section for driving an ultrasonic probe for transmitting an ultrasonic transmission wave to biomedical tissue;

a receiving section which amplifies a reflected ultrasonic wave acquired as a result of reflection of the ultrasonic transmission wave from the biomedical tissue and received by the ultrasonic probe, to thus generate a received signal;

a phase detection section for subjecting the received signal to phase detection;

a computing section which determines elastic characteristics of a plurality of positions within the biomedical tissue from a phase detection signal acquired from the phase detection section and which computes a relative elastic characteristic from a value determined by dividing an elastic characteristic of another area by an elastic characteristic of an arbitrary reference area in the biomedical tissue; and

a display section for displaying a distribution of the relative elastic characteristics computed by the computing section,

wherein the elastic characteristic of the arbitrary reference area in the biomedical tissue is an elastic characteristic of an area of an adventitia in the blood vessel or an elastic characteristic acquired in the past from an arbitrary reference area.

4. The ultrasonic diagnostic apparatus according to claim 1, wherein the computing section has a reference area setting section for setting the reference area.

5. The ultrasonic diagnostic apparatus according to claim 4, wherein the display section displays the reference area set by the computing section so as to be superimposed on at least one of an ultrasonic tomogram image or an elastic characteristic image.

6. The ultrasonic diagnostic apparatus according to claim 4, wherein the display section displays positional coordinates of the reference area set by the computing section in the form of numerals.

7. The ultrasonic diagnostic apparatus according to claim 2, wherein the computing section has a reference area setting section for setting the reference area.

8. The ultrasonic diagnostic apparatus according to claim 7, wherein the display section displays the reference area set by the computing section so as to be superimposed on at least one of an ultrasonic tomogram image or an elastic characteristic image.

9. The ultrasonic diagnostic apparatus according to claim 7, wherein the display section displays positional coordinates of the reference area set by the computing section in the form of numerals.

10. The ultrasonic diagnostic apparatus according to claim 3, wherein the computing section has a reference area setting section for setting the reference area.

11. The ultrasonic diagnostic apparatus according to claim 10, wherein the display section displays the reference area set

by the computing section so as to be superimposed on at least one of an ultrasonic tomogram image or an elastic characteristic image.

12. The ultrasonic diagnostic apparatus according to claim 10, wherein the display section displays positional coordinates of the reference area set by the computing section in the form of numerals.

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专利名称(译)	超声诊断设备		
公开(公告)号	US20090118615A1	公开(公告)日	2009-05-07
申请号	US11/995993	申请日	2006-07-20
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IPC分类号	A61B8/00		
CPC分类号	A61B5/02007 A61B8/485 A61B8/0891 A61B8/08		
优先权	2005210233 2005-07-20 JP		
其他公开文献	US7946987		
外部链接	Espacenet USPTO		

摘要(译)

本发明的目的在于提供一种超声波诊断装置，该超声波诊断装置能够在不依赖于血压测量的精度或稳定性且不涉及血压测量的情况下，针对每个听力节拍显示弹性特性的稳定空间分布。在本发明的超声波诊断装置中，从超声波探头13发射并由生物医学组织反射的超声波反射波通过接收部分15，延迟时间控制部分16，相位检测输入到计算部分19。根据从相位检测部分17获取的相位检测信号，计算部分19计算相对弹性特性，该相对弹性特性是由在任意参考区域的弹性特性归一化的弹性特性。生物医学组织。由计算部分计算的相对弹性特性的分布显示在显示部分21上。

