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Chaggares

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(54) **HIGH FREQUENCY ULTRASOUND
TRANSDUCER HAVING AN ULTRASONIC
LENS WITH INTEGRAL CENTRAL
MATCHING LAYER**

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A61B 8/00 (2006.01)
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B06B 1/06 (2006.01)
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CPC **A61B 8/4272** (2013.01); **B06B 1/067**
(2013.01); **G10K 11/30** (2013.01); **Y10T**
156/10 (2015.01)

(58) **Field of Classification Search**
None
See application file for complete search history.

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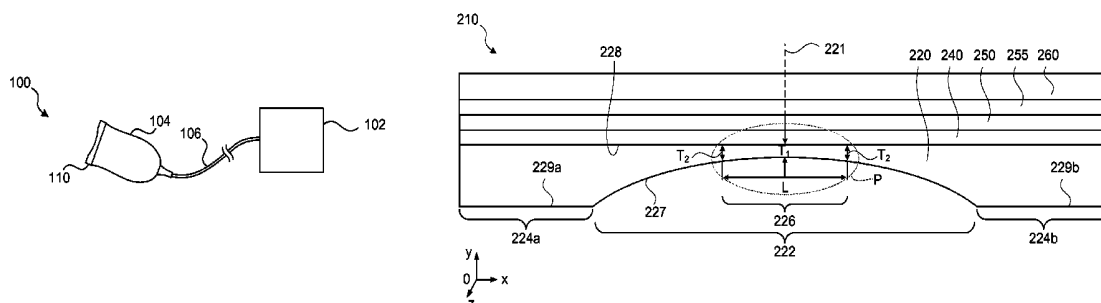
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(57) **ABSTRACT**

High frequency ultrasound transducers configured for use
with high frequency ultrasound diagnostic imaging systems
are disclosed herein. In one embodiment, an ultrasound
transducer includes a concave lens having an average thick-
ness in a center portion that is substantially equal to an
odd multiple a $\frac{1}{4}$ -wavelength of the center frequency of the
ultrasound transducer.

13 Claims, 3 Drawing Sheets



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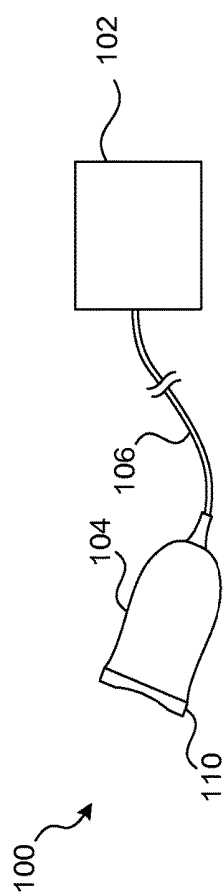


FIG. 1

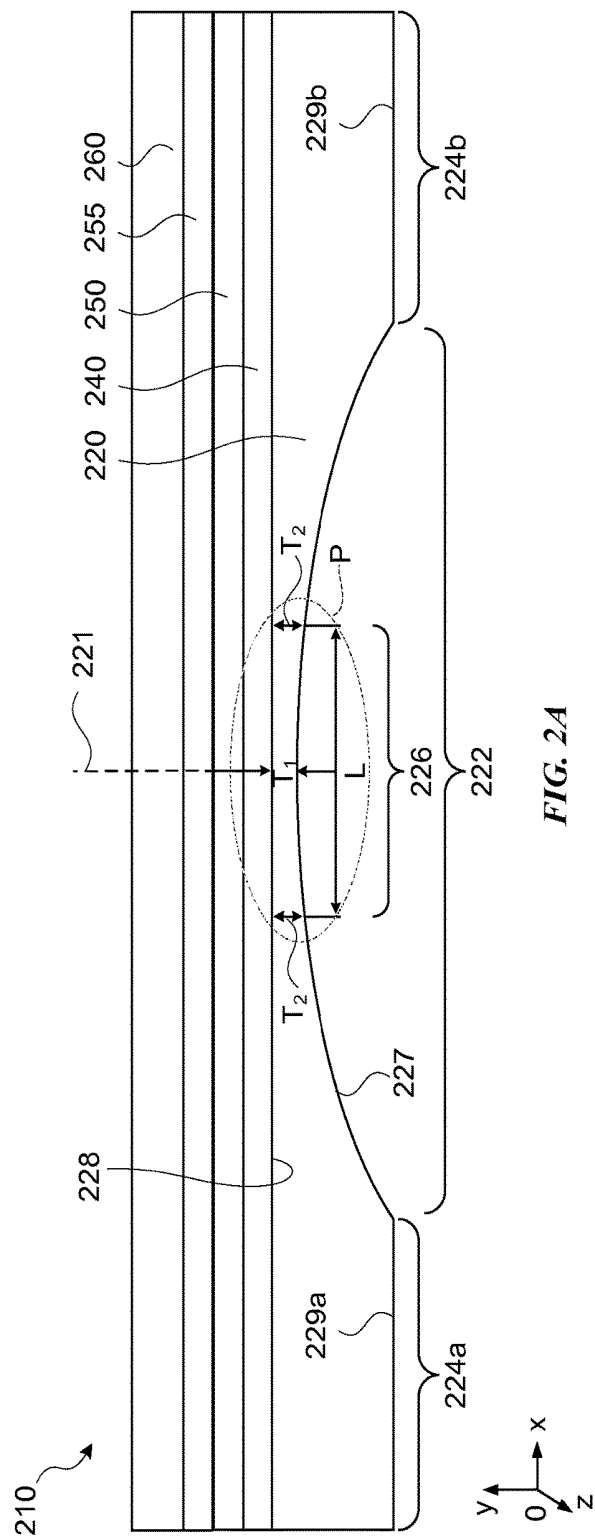
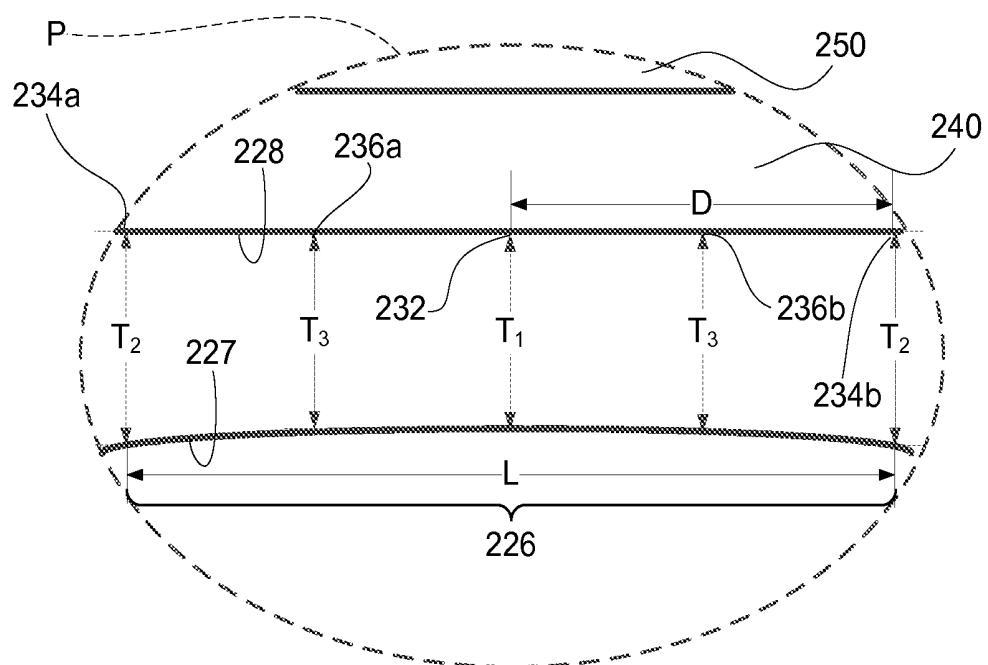


FIG. 2A

**FIG. 2B**

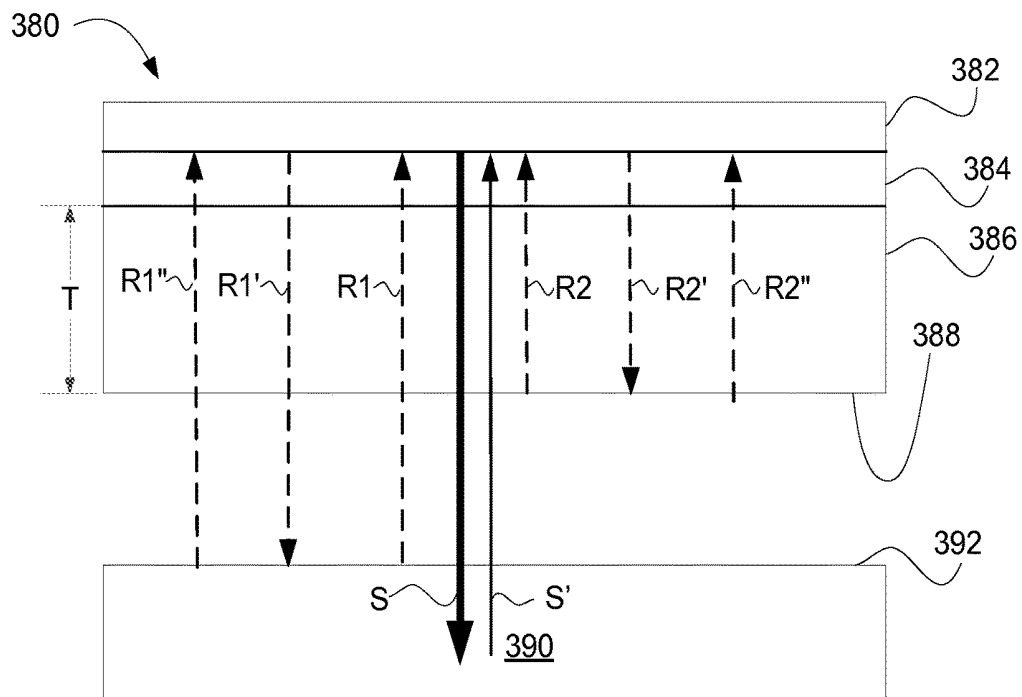


FIG. 3
(PRIOR ART)

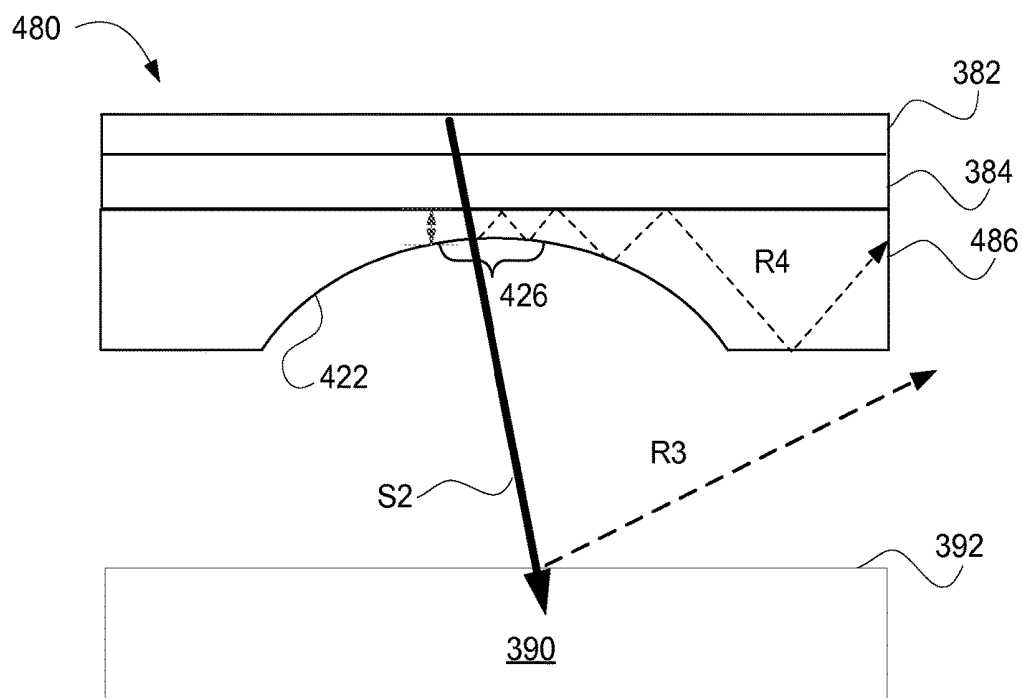


FIG. 4

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HIGH FREQUENCY ULTRASOUND TRANSDUCER HAVING AN ULTRASONIC LENS WITH INTEGRAL CENTRAL MATCHING LAYER

TECHNICAL FIELD

The disclosed technology generally relates to the fields of ultrasonic transducers and medical diagnostic imaging. More specifically, the disclosed technology relates to high frequency ultrasonic transducers and acoustic lenses configured for use therewith.

PATENTS AND PATENT APPLICATIONS INCORPORATED BY REFERENCE

The following patents are also incorporated by reference herein in their entireties: U.S. Pat. No. 7,052,460, titled "SYSTEM FOR PRODUCING AN ULTRASOUND IMAGE USING LINE-BASED IMAGE RECONSTRUCTION," and filed Dec. 15, 2003; U.S. Pat. No. 7,255,648, titled "HIGH FREQUENCY, HIGH FRAME-RATE ULTRASOUND IMAGING SYSTEM," and filed Oct. 10, 2003; U.S. Pat. No. 7,230,368, titled "ARRAYED ULTRASOUND TRANSDUCER," and filed Apr. 20, 2005; U.S. Pat. No. 7,808,156, titled "ULTRASONIC MATCHING LAYER AND TRANSDUCER," and filed Mar. 2, 2006; U.S. Pat. No. 7,901,358, titled "HIGH FREQUENCY ARRAY ULTRASOUND SYSTEM," and filed Nov. 2, 2006; and U.S. Pat. No. 8,316,518, titled "METHODS FOR MANUFACTURING ULTRASOUND TRANSDUCERS AND OTHER COMPONENTS," and filed Sep. 18, 2009.

BRIEF DESCRIPTION OF THE DRAWINGS

The invention may be more completely understood in consideration of the accompanying drawings, which are incorporated in and constitute a part of this specification, and together with the description, serve to illustrate the disclosed technology.

FIG. 1 is a schematic view of an ultrasound imaging system configured in accordance with one or more embodiments of the disclosed technology.

FIG. 2A is a cross-sectional schematic view of an ultrasound transducer stack configured in accordance with one or more embodiments of the disclosed technology.

FIG. 2B is an enlarged view of a portion P of FIG. 2A.

FIG. 3 is a schematic side view of a prior art transducer.

FIG. 4 is a schematic side view of a transducer configured in accordance with one or more embodiments of the disclosed technology.

DETAILED DESCRIPTION

Ultrasonic transducers provide a means for converting electrical energy into acoustic energy and vice versa. When the electrical energy is in the form of a radio frequency (RF) signal, a transducer can produce ultrasonic signals with the same frequency characteristics as the driving electrical RF signal. Conventional clinical ultrasound transducers are typically operated at center frequencies ranging from less than 1 Megahertz (MHz) to about 10 MHz. Ultrasound in the frequency spectrum of 1-10 MHz generally provides a means of imaging biological tissue with a resolution ranging from several millimeters to generally greater than 150 microns and at depths from a few millimeters to greater than 10 centimeters.

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In contrast, high frequency ultrasonic (HFUS) transducers are generally ultrasonic transducers with center frequencies above 15 MHz and ranging to over 60 MHz (e.g., 15 MHz, 20 MHz, 25 MHz, 30 MHz, 40 MHz, 50 MHz, 60 MHz).

HFUS transducers provide higher resolution than transducers that operate at lower frequencies (e.g., less than 15 MHz.) while limiting a maximum depth of penetration. As a result, HFUS transducers can image biological tissue at depths ranging from, for example, a fraction of a millimeter (e.g., 0.25 mm, 0.5 mm, 0.75 mm) to 3 cm or greater (e.g., 4 cm) with resolutions ranging, for example, from about 20 microns to about 200 microns.

For transducers operating at frequencies less than 10 MHz, for example, a wide variety of lens materials are available to produce convex lenses that are substantially acoustically impedance-matched to a medium (e.g., tissue in a subject) to be imaged. Acoustic energy received at these transducers is typically almost completely transmitted through the lens material to be received by the transducer, with almost no energy reflected back into the medium, and thus no multipath artifacts are created. In addition, one skilled in the art will understand that a well-designed transducer, having a well matched lens material will not exhibit multiple reflections within the lens itself. In the case of HFUS transducers, however, very few materials are suitable for constructing acoustic lenses due to significantly higher acoustic attenuation. As those of ordinary skill in the art will appreciate, acoustic attenuation in polymers tends to increase exponentially with frequency. Accordingly, an acoustic attenuation of ultrasound energy at 20 MHz in a polymer can be an order of magnitude (e.g., 10 times greater, 20 times greater, 100 times greater) than an acoustic attenuation of ultrasound energy of 10 MHz and below in the same polymer.

There can be many challenges associated with fabricating HFUS transducers that do not arise when working with traditional clinical ultrasonic transducers that operate at frequencies below about 10 MHz. Those of ordinary skill in the art will appreciate that structures (e.g., transducer layers, matching layers, lenses) associated with an ultrasound transducer generally scale in a manner that is inversely proportional to an operating frequency of the transducer. For example, a 50 MHz transducer will have structures about 10 times smaller than a 5 MHz transducer. In many cases, materials or techniques used with lower frequency transducers (e.g., less than about 10 MHz.) cannot be scaled down to sizes and/or shapes suitable for use in HFUS transducers. Accordingly, new technologies may need to be developed or adapted in the fabrication of HFUS transducers. In other cases, entirely new requirements exist when dealing with the higher radio frequency electronic and acoustic signals associated with HFUS transducers.

Conventional HFUS transducers typically include hard plastic acoustic lenses shaped and/or formed into concave lenses in order to focus an elevation dimension of the transducer. Suitable HFUS lens materials may include, for example, polymethylpentene (e.g., TPX®), cross-linked polystyrene (e.g., Rexolite®), and polybenzimidazole (e.g., Celazole®), all of which have relatively low attenuation at frequencies greater than about 15 MHz. Acoustic lenses made from materials suited for HFUS use, however, may also have acoustic impedances significantly or substantially different (e.g., 10% different, 25% different, 50% different) from an acoustic impedance of a subject to be imaged. The resulting acoustic impedance mismatch (e.g., a difference of 0.1 MRayl, 0.3 MRayl, 0.5 MRayl, 1 MRayl, 2 MRayls) between the lens and the subject can cause multipath imag-

ing artifacts when ultrasound energy is transmitted from the transducer and received at the transducer to form an ultrasound image. An acoustic impedance mismatch at the front of the lens with respect to the coupling medium or the subject can also result in intra-lens reflections and/or lens reverberation artifacts that can degrade the axial resolution of the ultrasound transducer.

The multipath or multi-bounce artifacts can cause a ghost image of bright specular reflectors appearing at an equal depth below the true image of the specular reflector. A skin line of a subject, for example, may be imaged at a depth of 4 mm in the image and cause a multipath artifact at a depth of 8 mm. Those of ordinary skill in the art will appreciate that such an artifact may be produced when ultrasonic energy emitted from the transducer strikes a strong specular reflector (e.g., a skin line of a subject) roughly normal to the path of the ultrasound. A portion (e.g., 5%, 10%) of the emitted ultrasonic energy may be reflected back from the specular reflector toward the transducer lens, whereupon a second reflection may occur if the lens is not substantially acoustically matched to the transmission medium (e.g., gel, water). The second reflection may then propagate back to the specular reflector a second time, where again, a specular reflection occurs and acoustic energy is once again received by the transducer. A cascade of such reflections can cause a series of multipath artifacts to appear in an ultrasound image. Such partial reflections can occur repeatedly until no significant energy remains in the reflections. One approach to mitigating imaging artifacts may include positioning an acoustic matching layer on an outer surface of an acoustic lens. Lenses having matching layers on their outer surfaces, however, can be very difficult to fabricate and, in many cases, are impractical for use with ultrasound transducers that operate at higher frequencies (e.g., greater than about 15 MHz.).

Lens reverberation artifacts caused by, for example, intra-lens multiple reflections can be similar to the multipath artifacts described above. Intra-lens reflections, however, occur entirely within the lens material and may be caused by an acoustic mismatch between the outer surface of the lens and the acoustic coupling medium or the subject being imaged. A partial echo is produced at the front face of the lens as the acoustic pulse exits the transducer and enters the subject. This echo can then reverberate between any internal acoustic mismatch in the transducer acoustic stack, such as the back surface of the lens for example. As those of ordinary skill in the art will appreciate, every effort will be made to acoustically match the back surface of the lens to the acoustic stack of the transducer, typically through the use of some form of acoustic matching layer. However, due to the low attenuation of HFUS lens materials, even a small reflection from the back surface/stack interface can give rise to a lens reverb artifact. The effect of the lens reverb artifact is to effectively lengthen the pulse of the transducer as each reverb echo become part of the main transducer pulse and thus any echoes received by the transducer.

FIG. 3 is a schematic view of a prior art transducer **380** that illustrates one example of the intra-lens reflections and reverberation artifacts described above. The transducer **380** includes a transducer layer **382**, a matching layer **384** and an acoustic lens **386** having a lower surface **388** and a thickness **T**. The transducer **380** transmits and receives ultrasound energy (e.g., high frequency ultrasound of 15 MHz or greater) through a skin line **392** of a subject **390** (e.g., a human patient, an animal). The transducer layer **382** is configured to transmit a primary ultrasound signal **S** into the

subject **390** and receives ultrasound echoes **S'**, which are used to form an ultrasound image.

First, second and third reflections **R1**, **R1'** and **R1''** illustrate one example of the multipath artifacts described above. The skin line **392** reflects a portion (e.g., 5%, 10%, 20%) of the signal **S** thereby forming the first reflection **R1**. The first reflection **R1** propagates back toward the transducer layer **382**, which reflects a portion (e.g., 5%, 10%, 20%) of the first reflection **R1** back toward the subject thereby forming the second reflection **R1'**. The skin line **392** reflects a portion of the second reflection **R1'** back toward the transducer layer **382** thereby forming the third reflection **R1''**. The transducer layer **382** receives the echoes **S'** along with portions of the first reflection **R1** and third reflection **R1''**, all of which are combined by an image processor (not shown) to form an ultrasound image. As those of ordinary skill in the art will appreciate, the reflections **R1** and **R1''** can cause undesirable artifacts in the ultrasound image.

First, second and third reflections **R2**, **R2'** and **R2''** illustrate one example of the intra-lens reverberation artifacts described above. The lower surface **388** of the lens **386** reflects a portion (e.g., 5%, 10%, 20%) of the signal **S** thereby forming the first reflection **R2**. The first reflection **R2** propagates back toward the transducer layer **382**, which reflects a portion (e.g., 5%, 10%, 20%) of the first reflection **R2** back toward the subject thereby forming the second reflection **R2'**. The lower surface **388** of the lens **386** reflects a portion of the second reflection **R2'** back toward the transducer layer **382** thereby forming the third reflection **R2''**. The transducer layer **382** receives a combination of the echoes **S'** along with portions of the first reflection **R2** and the third reflection **R2''** to form an ultrasound image. The reflections **R2** and **R2''** can cause undesirable artifacts in the ultrasound image. In many instances, reflections similar to **R1**, **R1''**, **R2** and **R2''** can cause artifacts in the same ultrasound image, which can significantly reduce image quality.

FIG. 4 is a schematic side view of a transducer **480** configured in accordance with one or more embodiments of the disclosed technology. The transducer **480** includes an lens **486** having a curved surface **422** and a center portion **426**. The center portion **426** has an average thickness approximately equal to an odd multiple of a quarter wavelength (e.g., $\frac{1}{4}$ -wavelength, $\frac{3}{4}$ -wavelength, $\frac{5}{4}$ -wavelength, $\frac{7}{4}$ -wavelength) of the center frequency of the transducer **480**. A signal **S2** is transmitted into the subject **390**. The skin line **392** reflects a portion of the signal **S2** to form a first reflection **R3**, and the curved portion **422** reflects a portion of the signal **S2** to form second reflections **R4**. In contrast to reflections **R1** and **R2** discussed above, the first reflection **R3** and the second reflections **R4** are not specular reflections and thus do not travel back to the transducer **382**. Accordingly the lens **486** can significantly reduce artifacts in a HFUS image, such as the intra-lens and multipath reflections discussed above with reference to FIG. 3.

The disclosed technology can provide a reduction of multipath artifacts (e.g., intra-lens reverberation artifacts, external multi-bounce artifacts) in HFUS transducers described above. In one aspect of the present disclosure, an ultrasound transducer includes an acoustical lens in which a center portion of the lens (e.g., the thinnest part of the concave shape of the lens between two end portions of the lens) has a thickness of about a fractional portion of a wavelength of the transducer center frequency. In some embodiments, for example, the lens center portion can have an average thickness approximately equal to an odd multiple of a quarter wavelength (e.g., $\frac{1}{4}$ -wavelength, $\frac{3}{4}$ -wave-

length, $5/4$ -wavelength, $7/4$ -wavelength) of the transducer center frequency (e.g., 15 MHz, 20 MHz, 25 MHz, 30 MHz). Incorporating the lens described above onto an ultrasound transducer results in the central portion of the lens effectively adding an additional matching layer (e.g., a quarter wavelength matching layer) to the front of the transducer. The disclosed technology therefore provides a lens having reduced acoustic reflectivity to normal incident plane waves, thus mitigating multipath acoustic artifacts in the image, and reducing intra lens reverberations as well. In some embodiments, for example, the disclosed technology can increase the transmission coefficient of an HFUS transducer lens from 85% to about 95%. Stated differently, the disclosed technology can reduce the reflection coefficient of an HFUS transducer lens from 15% to less than between 5% and 10% or less, thereby significantly increasing sensitivity of the HFUS transducer (e.g., an increase between 1 dB and 2.5 dB).

In another aspect of the disclosed technology, an ultrasound transducer stack includes a transducer layer and a lens layer. The transducer layer is configured to transmit ultrasound energy at a center frequency (e.g., 15 MHz or higher). The lens layer has an upper surface underlying the transducer layer. At least a portion of the lens layer has a concave curvature in a direction normal to an axial direction of the transducer. A center portion of the lens layer has an average thickness that is substantially equal to an odd multiple (e.g., 1, 3, 5) of a $1/4$ wavelength of the center frequency of the transducer layer. In some embodiments, a matching layer is disposed between the lens layer and the transducer layer. In one embodiment, for example, the matching layer is attached to the lens layer by another matching layer that comprises cyanoacrylate. In some embodiments, the lens layer has an acoustic impedance substantially different (e.g., 10% different, 25% different, 50% different) than an acoustic impedance of water.

In yet another aspect of the disclosed technology, an ultrasound system includes an ultrasound imaging system coupled to an ultrasound transducer probe. The ultrasound transducer probe is configured to transmit ultrasound toward a subject and receive ultrasound energy from the subject. The transducer probe includes a lens layer and one or more transducer elements configured to operate at a center frequency (e.g., between about 15 MHz and about 60 MHz). A portion of the lens layer has a concave curvature in a direction normal to an axial direction of the transducer. A center portion of the concave curvature has an average thickness substantially equal to (e.g., within about 1%, within about 2%, within about 5%) an odd multiple (e.g., 1, 3, 5, 7, 9) of a $1/4$ wavelength of the center frequency of the one or more transducer elements. In some embodiments, a reflection coefficient of the lens layer is less than about 5%. In some embodiments, the reflection coefficient is between, for example, about 1% and 15%.

In still another aspect of the disclosed technology, a method of constructing an ultrasound transducer includes fabricating an acoustic lens layer and attaching or bonding the lens layer to a first matching layer operationally coupled to a transducer layer. The lens layer is fabricated to have a center curved section and two flat side sections. Fabricating the curved section includes fabricating a center portion having a midpoint and two endpoints such that the center portion has a first thickness at the midpoint and a second thickness at each of the two endpoints. An average of the first thickness and the second thickness is substantially equal to (e.g., within about 1%, within about 2%, within about 5%) an odd multiple of a $1/4$ wavelength (e.g., $1/4$ -wavelength, $3/4$ -

wavelength, $5/4$ -wavelength) of the center frequency (e.g., between about 15 MHz and about 60 MHz) of the ultrasound transducer. In some embodiments, the method further includes bonding or attaching a second matching layer to the lens layer with the first matching layer such that the second matching layer is positioned between the first matching layer and the transducer layer. In some embodiments, the lens layer has a speed of sound significantly different (e.g., 100% different, 200% different) than a speed of sound in water.

In another aspect of the disclosed technology, an ultrasound transducer stack includes a transducer layer comprising one or more ultrasound transducer elements configured to operate at a center frequency of 15 MHz or greater (e.g., between about 15 MHz and about 60 MHz). The transducer stack further includes an acoustic lens having a rear surface attached to a matching layer operationally coupled to the transducer layer. A front surface of the acoustic lens includes two flat side sections and a center curved section extending therebetween in an elevation direction relative to the transducer stack. A first thickness of the center curved section in an axial direction relative to the transducer stack is less than an odd multiple of $1/4$ -wavelength of the center frequency. The thickness of the center curved section increases outwardly a first distance in the elevation direction to an endpoint having a second thickness in the axial direction that is greater than an odd multiple of $1/4$ -wavelength of the center frequency such that the average thickness in the axial direction of the center curved section between the midpoint and the endpoint is substantially an odd multiple of $1/4$ -wavelength of the center frequency. In some embodiments, a length of the center curved section is twice the first distance. In some embodiments, the length of the center curved section is about 10% or less of a total length of the transducer stack in the elevation direction. In some embodiments, the first thickness is between about 95% and 99.5% of the odd multiple of the $1/4$ -wavelength of the center frequency, and the second thickness is between about 100.5% and 105% of the odd multiple of the $1/4$ -wavelength of the center frequency.

Suitable Systems

FIG. 1 is a schematic view of an ultrasound system 100 configured in accordance with an embodiment of the disclosed technology. The ultrasound system 100 includes an ultrasound probe 104 coupled to an image processing system 102 via a link 106 (e.g., a wire, a wireless connection). The probe 104 includes a transducer 110 (e.g., an HFUS stack). The transducer 110 can transmit ultrasound energy (e.g., HFUS energy) into a subject and receive at least a portion of the reflected ultrasound energy from the subject. The received ultrasound energy can be converted into a corresponding electrical signal and transmitted electrically to the image processing system 102, which can form one or more ultrasound images based on the received ultrasound energy.

FIG. 2A is a cross section schematic view of an ultrasound transducer stack 210 (e.g., the transducer 110 of FIG. 1) configured in accordance with one or more embodiments of the disclosed technology. The transducer stack 210 includes an acoustic lens 220, a first matching layer 240, a second matching layer 250, a third matching layer 255 and a transducer layer 260 (e.g., a piezoelectric transducer layer, a PMUT layer, a CMUT layer). In some embodiments, the first matching layer 240 can include a bonding material (e.g., cyanoacrylate, a polymer, an epoxy) having a $1/4$ -wavelength thickness and can be configured to bond or otherwise attach a front surface of the second matching layer 250 to a rear surface 228 of the lens 220. A rear surface of the matching layer 250 is bonded or otherwise attached to a front surface

of the third matching layer **255**. A rear surface of the third matching layer **255** is attached to a front surface of the transducer layer **260**. A centerline **221** extends along an axial direction (i.e., along the y-axis shown in FIG. 2A) of the transducer stack **210**. In the illustrated embodiment, the transducer stack **210** includes a three matching layers—the first matching layer **240**, the second matching layer **250** and the third matching layer **255**. In some embodiments, however, the transducer stack **210** may include one or more additional matching layers as disclosed, for example, in U.S. Pat. No. 7,808,156, incorporated by reference above. Other embodiments of the transducer stack **210** may not include one or more of the first matching layer **240**, the second matching layer **250** and the third matching layer **255**.

The lens **220** includes a curved section **222** that has a concave curvature (e.g., cylindrical, parabolic or hyperbolic curvature) in an elevation direction (i.e., along the x-axis shown in FIG. 2) of the transducer stack **210**. The curved section **222** is bounded by side section **224** (identified individually as a first side section **224a** and a second side section **224b**). The curved section **222** has a curved outer surface **227** and the flat side portions **224** have outer surfaces **229** (identified individually as a first outer surface **229a** and a second outer surface **229b**). The curved section **222** includes a center portion **226** centered at the centerline **221**. As discussed in more detail with reference to FIG. 2A, the center portion **226** has a first thickness T_1 at a midpoint and a second thickness T_2 at two endpoints. The center portion **222** has a length L (e.g., less than 0.5 mm, 0.5 mm, 0.7 mm, 1 mm, greater than 1 mm) in the elevation direction of the transducer. In some embodiments, the length L can extend between about 1% and 10% of the length of the transducer in the elevation direction. In some embodiments, the length L and a radius of curvature of the center portion **226** can be determined by the focal number (e.g., F2, F5, F8, F10) of the lens and the focal depth of the transducer. As those of ordinary skill in the art will appreciate, the focal number of the lens is proportional to a ratio of the focal depth of the transducer and a length of the curved section **222** of the lens.

The lens **220** can comprise, for example, polymethylpentene, cross-linked polystyrene and/or polybenzimidazole. In other embodiments, however, the lens **220** can comprise any suitable material (e.g., metals, such as aluminum or stainless steel, or ceramic materials, such as PZT or alumina) having a speed of sound higher than a speed of sound of a medium being imaged (e.g., water, tissue in a subject). Moreover, in some embodiments, the first thickness T_1 of the center portion **226** may be slightly less than an odd multiple of $\frac{1}{4}$ of the wavelength (e.g., between approximately 95% and 99.5% of an odd multiple of the $\frac{1}{4}$ wavelength thickness) of a center frequency (e.g., 15 MHz or greater) of the transducer layer **260**. Correspondingly, the second thickness T_2 may be slightly more than an odd multiple of $\frac{1}{4}$ of the wavelength (e.g., between approximately 100.5% and 105% of an odd multiple of the $\frac{1}{4}$ wavelength thickness) of the center frequency. The center portion **226** of the curved section **222** therefore has a substantially average thickness of approximately an odd multiple of $\frac{1}{4}$ of the wavelength (within a $\pm 5\%$ of an odd multiple of $\frac{1}{4}$ wavelength). Fabricating the center portion **226** to have an average thickness substantially equal to a fractional wavelength of the center frequency of the transducer layer **260** can provide an improved acoustic match to a subject being imaged and therefore can significantly reduce multipath reflections compared to an acoustic lens having an arbitrary thickness.

FIG. 2B is an enlarged view of a portion P of FIG. 2A showing the center portion **226** in more detail. The center

portion **222** has a midpoint **232** and extends between a first endpoint **234a** and second endpoint **234b** in the elevation direction. The midpoint **232** is spaced apart from each of the first and second midpoints **234a** and **234b** a distance D in the elevation direction (i.e., one-half the length L). The thickness of the center portion **222** in the axial direction increases outwardly from T_1 at the midpoint **232** to the thickness T_2 at each of the first and second midpoints **234a** and **234b**. The average thickness of the center portion **222** substantially equal to an odd multiple (e.g., 1, 3, 5, 7) of a $\frac{1}{4}$ -wavelength of the center frequency of the transducer layer **260** (FIG. 2A). Further, at intermediate points **236a** and **236b**, the center portion **222** has a thickness T_3 generally corresponds to the average thickness of the center portion **222** between midpoint **232** and each of the first and second midpoints **234a** and **234b**.

In some embodiments, however, the center portion **226** can be configured to have an average $\frac{3}{4}$ -wavelength thickness to provide adequate dielectric strength to meet desired medical electrical safety standards. In other embodiments, the center portion **226** may have an average thickness less than $\frac{3}{4}$ wavelength. In some embodiments, for example, the center portion **226** can be fabricated to have an average thickness of the $\frac{1}{4}$ of the wavelength of an operational center frequency (e.g., 20 MHz, 25 MHz, 30 MHz) of the transducer layer **260**. In some embodiments, the average thickness of the center portion **226** can be any odd multiple (e.g., 1, 3, 5, 7, 9) of $\frac{1}{4}$ of the wavelength of the operational center frequency of the transducer layer **260** (FIG. 2A). In other embodiments, however, the average thickness can be any suitable fraction of the wavelength of the operational center frequency of the transducer layer **260** (FIG. 2A). Those of ordinary skill in the art will appreciate, for example, that for broadband ultrasound transducers, a $\frac{1}{4}$ wavelength lens thickness will generally perform better than a $\frac{3}{4}$ wavelength lens thickness, and increasing odd multiples of $\frac{1}{4}$ -wavelength generally perform progressively worse. In contrast, narrowband transducers (e.g., CW Doppler transducers) can have acoustic lenses with increasing odd multiples of the $\frac{1}{4}$ -wavelength without a significant reduction in performance.

Fabricating the center portion **226** to have of an average thickness corresponding generally to a fractional portion (e.g., $\frac{1}{4}$, $\frac{3}{4}$) of the wavelength can, in addition to minimizing multi-path artifacts, acoustically enhance a central part of the elevation dimension (i.e., along the x-axis of FIG. 2A) of the transducer layer **260** (FIG. 2A), thereby providing a desirable boost to a normal component of the elevation beam. This can be viewed as achieving the equivalent of mild apodization of the elevation beam by enhancing the central part of the beam relative to the edges, as opposed to attenuating the edges relative to the center of the beam. The apodization of the elevation beam can lead to a reduction in sidelobes in the elevation beam.

From the foregoing, it will be appreciated that specific embodiments of the invention have been described herein for purposes of illustration, but that various modifications may be made without deviating from the scope of the invention. Accordingly, the invention is not limited except as by the appended claims.

I claim:

1. An ultrasound transducer stack comprising:
 - a transducer layer configured to transmit ultrasound energy at a center frequency;
 - a lens layer secured to the transducer layer, wherein at least a portion of the lens layer has a concave recess with a length L measured in an elevation direction of

- the transducer stack and wherein a center portion of the concave recess has a length that is less than L and is defined between a center point of the concave recess and points outwardly therefrom in the elevation direction such that the center portion has an average thickness measured in an axial direction of the transducer stack that is substantially equal to one of 1, 3, 5 or 7 multiples of a $\frac{1}{4}$ wavelength of the center frequency of the transducer layer at a speed of sound in the lens material;
- a first matching layer disposed between the transducer layer and the lens layer; and
- a second matching layer disposed between the lens layer and the first matching layer, wherein the second matching layer comprises cyanoacrylate, and wherein the first matching layer and the second matching layer each have a thickness approximately $\frac{1}{4}$ -wavelength of the center frequency of the ultrasound energy from the transducer layer at the speed of sound in the lens material.
2. The ultrasound transducer stack of claim 1, wherein the center frequency at which the transducer layer is configured to transmit ultrasound energy is greater than 15 MHz, and wherein the lens layer is acoustically penetrable at frequencies greater than 15 MHz.
3. The ultrasound transducer stack of claim 1, wherein the average thickness of the center portion of the lens layer is $\frac{1}{4}$ of the wavelength of the center frequency of the ultrasound energy from the transducer layer at the speed of sound in the lens material.
4. The ultrasound transducer stack of claim 1, wherein the average thickness of the center portion of the lens layer is $\frac{3}{4}$ of the wavelength of the center frequency of the ultrasound energy from the transducer layer at the speed of sound in the lens material.
5. The ultrasound transducer stack of claim 1, wherein the lens layer has an acoustic impedance substantially different than an acoustic impedance of water.
6. An ultrasound system, comprising:
an ultrasound imaging system; and
an ultrasound transducer probe coupled to the imaging system and configured to transmit ultrasound energy at a center operating frequency toward a subject and receive ultrasound energy from the subject, wherein the ultrasound transducer probe includes:
one or more transducer elements configured to generate ultrasound energy at the center operating frequency; and
a lens layer, wherein at least a portion of the lens layer has a concave recess with a length L measured in an elevation direction of the transducer probe and a center region that is smaller than L measured in the elevation direction, wherein the average thickness of the lens in the center region as measured in an axial direction of the transducer probe is substantially equal to one of 1, 3, 5 or 7 multiples of $\frac{1}{4}$ wavelength of the center frequency of the ultrasound energy produced at a speed of sound in the lens layer.
7. The ultrasound system of claim 6, wherein the center operating frequency of the ultrasound energy transmitted is greater than 15 MHz, and wherein the lens layer is acoustically penetrable at frequencies greater than 15 MHz.
8. The ultrasound system of claim 7, wherein a reflection coefficient of the lens layer is less than 10%.

9. The ultrasound system of claim 6, wherein the average thickness of the center region of the lens layer is $\frac{1}{4}$ of the wavelength of the center frequency of the ultrasound energy transmitted.

10. The ultrasound system of claim 6, wherein the average thickness of the center region of the lens layer is $\frac{3}{4}$ of the wavelength of the center frequency of the ultrasound energy transmitted.

11. An ultrasound transducer stack, comprising:

a transducer layer comprising one or more ultrasound transducer elements configured to generate ultrasound energy at a center frequency of 15 MHz or greater;

a matching layer spaced apart from the transducer layer in an axial direction relative to the transducer stack; and
an acoustic lens having a front surface and a rear surface, wherein the rear surface of the lens is attached to the matching layer, wherein the front surface includes two flat side sections and a concave curved section extending therebetween in an elevation direction relative to the transducer stack, wherein the concave curved section includes a central area that is smaller than a length of the concave curved section as measured in the elevation direction with a first thickness at a center of the lens in the axial direction of the stack that is less than one of 1, 3, 5 or 7 multiples of $\frac{1}{4}$ -wavelength of the center frequency of the ultrasound energy generated at a speed of sound in the acoustic lens, wherein the thickness of the central area increases outwardly in the elevation direction to a pair of points where the thickness of the lens has a second thickness in the axial direction that is greater than said one of 1, 3, 5 or 7 multiples of $\frac{1}{4}$ -wavelength of the center frequency of the ultrasound energy generated at the speed of sound in the lens such that the average thickness of the central area of the lens in the axial direction is substantially equal said 1, 3, 5 or 7 multiples of $\frac{1}{4}$ -wavelength of the center frequency of the ultrasound energy generated by the transducer layer at the speed of sound in the lens.

12. The ultrasound transducer stack of claim 11, wherein the first thickness is between about 95% and 99.5% of said one of 1, 3, 5 or 7 multiples of the $\frac{1}{4}$ -wavelength of the center frequency, and wherein the second thickness is between about 100.5% and 105% of said one of 1, 3, 5 or 7 multiples of the $\frac{1}{4}$ -wavelength of the center frequency of the ultrasound energy generated.

13. An ultrasound transducer comprising:

a transducer layer configured to generate ultrasound energy at a center frequency; and a lens layer coupled to the transducer layer, wherein the lens layer has a concave curvature in a direction normal to an axial direction of the transducer having a length L measured in an elevation direction of the transducer, and a center portion of the lens layer that is smaller than L with a central point where a thickness of the lens layer as measured in an axial direction of the transducer is between 95%-99.5% of one of 1, 3, 5 or 7 multiples of a $\frac{1}{4}$ wavelength of the center frequency of the ultrasound energy generated at a speed of sound in the lens layer and extending outwardly to points where the thickness of the lens layer is between 100.5 and 105% of said one of 1, 3, 5 or 7 multiples of a $\frac{1}{4}$ wavelength of the center frequency of the ultrasound energy generated at the speed of sound in the lens layer such that an average thickness of the lens layer in the center portion of the lens is substantially equal to said one of

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1, 3, 5 or 7 multiples of the $\frac{1}{4}$ wavelength of the center frequency of the ultrasound energy generated by the transducer.

* * * * *

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专利名称(译)	具有带有整体中心匹配层的超声透镜的高频超声换能器		
公开(公告)号	US10265047	公开(公告)日	2019-04-23
申请号	US14/656602	申请日	2015-03-12
[标]申请(专利权)人(译)	富士胶片索诺声公司		
申请(专利权)人(译)	FUJIFILM SONOSITE , INC.		
当前申请(专利权)人(译)	FUJIFILM SONOSITE , INC.		
[标]发明人	CHAGGARES NICHOLAS CHRISTOPHER		
发明人	CHAGGARES, NICHOLAS CHRISTOPHER		
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优先权	61/952086 2014-03-12 US		
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摘要(译)

本文公开了配置用于高频超声诊断成像系统的高频超声换能器。在一个实施例中，超声换能器包括凹透镜，该凹透镜在中心部分具有平均厚度，该凹透镜基本上等于超声换能器的中心频率的奇数倍且1/4波长。

