



US009412357B2

(12) **United States Patent**
Medan et al.

(10) **Patent No.:** **US 9,412,357 B2**
(45) **Date of Patent:** ***Aug. 9, 2016**

(54) **MAPPING ULTRASOUND TRANSDUCERS**

(58) **Field of Classification Search**

(71) Applicants: **Yoav Medan**, Haifa (IL); **Yoni Hertzberg**, Moshav (IL); **Dov Maor**, Haifa (IL)

CPC A61B 8/587; G10K 11/346; A61N 2007/0078; A61N 2007/0095; G01H 17/00; G01N 29/30; G01S 15/8934-15/8947
USPC 73/1.82, 1.86, 584; 600/437, 448, 459; 324/307; 367/13

(72) Inventors: **Yoav Medan**, Haifa (IL); **Yoni Hertzberg**, Moshav (IL); **Dov Maor**, Haifa (IL)

See application file for complete search history.

(73) Assignee: **INSIGHTEC LTD.**, Tirat Carmel (IL)

(56) **References Cited**

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 233 days.

U.S. PATENT DOCUMENTS

2,795,709 A 6/1957 Camp
3,142,035 A 7/1964 Harris

(Continued)

This patent is subject to a terminal disclaimer.

FOREIGN PATENT DOCUMENTS

CN 1744861 A 3/2006
CN 1981708 A 6/2007

(Continued)

(21) Appl. No.: **14/138,864**

(22) Filed: **Dec. 23, 2013**

OTHER PUBLICATIONS

(65) **Prior Publication Data**
US 2014/0112095 A1 Apr. 24, 2014

Examination Report Received for European Patent Application No. 05773991.4, mailed on Nov. 2, 2012, 5 pages.

(Continued)

Related U.S. Application Data

(62) Division of application No. 12/904,655, filed on Oct. 14, 2010, now Pat. No. 8,661,873.

Primary Examiner — Peter Macchiarolo

Assistant Examiner — David L Singer

(60) Provisional application No. 61/251,450, filed on Oct. 14, 2009.

(74) *Attorney, Agent, or Firm* — Morgan, Lewis & Bockius LLP

(51) **Int. Cl.**
G10K 11/34 (2006.01)
A61B 8/00 (2006.01)
A61N 7/00 (2006.01)

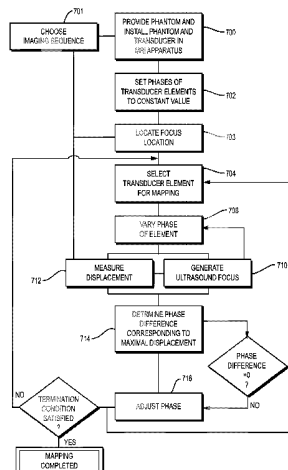
(Continued)

(57) **ABSTRACT**

Ultrasound transducers may be mapped by varying a focus-affecting parameter and adjusting the parameter so as to improve focus quality. In some embodiments, mapping involves successively varying the phase of one transducer element, or group of elements, with respect to a constant phase of the other transducer elements, and determining the phase at which a tissue displacement in the ultrasound focus is maximized.

(52) **U.S. Cl.**
CPC **G10K 11/346** (2013.01); **A61B 8/587** (2013.01); **A61N 2007/0078** (2013.01); **A61N 2007/0095** (2013.01); **G01H 17/00** (2013.01); **G01N 29/30** (2013.01)

20 Claims, 5 Drawing Sheets



(56)

References Cited

U.S. PATENT DOCUMENTS						
6,128,522	A	10/2000	Acker et al.	6,824,516	B2 11/2004	Batten et al.
6,128,958	A	10/2000	Cain	6,936,046	B2 8/2005	Hissong et al.
6,135,960	A	10/2000	Holmberg	6,951,540	B2 10/2005	Ebbini et al.
6,135,971	A	10/2000	Hutchinson et al.	6,961,606	B2 11/2005	DeSilets et al.
6,142,939	A	11/2000	Eppstein et al.	7,001,379	B2 2/2006	Behl et al.
6,156,549	A	12/2000	Drewes et al.	7,077,820	B1 7/2006	Kadziauskas et al.
6,193,659	B1	2/2001	Ramamurthy et al.	7,094,205	B2 8/2006	Marmarelis
6,217,530	B1	4/2001	Martin et al.	7,128,711	B2 10/2006	Medan et al.
6,242,915	B1	6/2001	Hurd	7,155,271	B2 12/2006	Halperin et al.
6,246,895	B1*	6/2001	Plewes A61B 8/00 324/309	7,175,596	B2 2/2007	Vitek et al.
6,246,896	B1	6/2001	Dumoulin et al.	7,175,599	B2 2/2007	Hynynen et al.
6,263,230	B1	7/2001	Haynor et al.	7,264,592	B2 9/2007	Shehada
6,267,734	B1	7/2001	Ishibashi et al.	7,264,597	B2 9/2007	Cathignol
6,289,233	B1	9/2001	Dumoulin et al.	7,267,650	B2 9/2007	Chow et al.
6,309,355	B1	10/2001	Cain et al.	7,344,509	B2 3/2008	Hynynen et al.
6,317,619	B1	11/2001	Boernert et al.	7,377,900	B2 5/2008	Vitek et al.
6,322,527	B1	11/2001	Talish	7,429,248	B1 9/2008	Winder et al.
6,334,846	B1	1/2002	Ishibashi et al.	7,452,357	B2 11/2008	Vlegele et al.
6,350,245	B1	2/2002	Cimino	7,505,805	B2 3/2009	Kuroda
6,374,132	B1	4/2002	Acker et al.	7,505,808	B2 3/2009	Anderson et al.
6,392,330	B1	5/2002	Zloter et al.	7,507,213	B2 3/2009	Schultheiss et al.
6,397,094	B1	5/2002	Ludeke et al.	7,510,536	B2 3/2009	Foley et al.
6,413,216	B1	7/2002	Cain et al.	7,511,501	B2 3/2009	Wexler
6,419,648	B1	7/2002	Vitek et al.	7,535,794	B2 5/2009	Prus et al.
6,424,597	B1	7/2002	Bolomey et al.	7,553,284	B2 6/2009	Vaitekunas
6,425,867	B1	7/2002	Vaezy et al.	7,603,162	B2 10/2009	Danz et al.
6,428,477	B1	8/2002	Mason	7,611,462	B2 11/2009	Vortman et al.
6,428,532	B1	8/2002	Doukas et al.	7,652,410	B2 1/2010	Prus
6,433,464	B2	8/2002	Jones	7,699,780	B2 4/2010	Vitek et al.
6,461,314	B1	10/2002	Pant et al.	7,819,805	B2 10/2010	Davies et al.
6,475,150	B2	11/2002	Haddad	1,006,603	A1 3/2011	Vitek et al.
6,478,739	B1	11/2002	Hong	8,057,408	B2 11/2011	Cain et al.
6,503,204	B1	1/2003	Sumanaweera et al.	8,075,488	B2 12/2011	Burton
6,506,154	B1	1/2003	Ezion et al.	8,661,873	B2 3/2014	Medan et al.
6,506,171	B1*	1/2003	Vitek A61H 23/0245 600/439	8,932,237	B2 1/2015	Vitek et al.
6,508,774	B1	1/2003	Acker et al.	2001/0031922	A1 10/2001	Weng et al.
6,511,064	B1	1/2003	Phinney et al.	2002/0016557	A1 2/2002	Duarte et al.
6,511,428	B1	1/2003	Azuma et al.	2002/0035779	A1 3/2002	Krieg et al.
6,522,142	B1	2/2003	Freundlich	2002/0082528	A1 6/2002	Friedman et al.
6,523,272	B1	2/2003	Morales	2002/0082589	A1 6/2002	Friedman et al.
6,524,251	B2	2/2003	Rabiner et al.	2002/0095087	A1 7/2002	Mourad et al.
6,543,272	B1	4/2003	Vitek	2002/0111552	A1 8/2002	Maor et al.
6,554,826	B1	4/2003	Deardorff	2002/0151790	A1 10/2002	Abend
6,559,644	B2	5/2003	Freundlich et al.	2002/0161300	A1 10/2002	Hoff et al.
6,566,878	B1	5/2003	Komura et al.	2002/0188229	A1 12/2002	Ryaby
6,582,381	B1	6/2003	Yehezkel et al.	2003/0004439	A1 1/2003	Pant et al.
6,589,174	B1	7/2003	Chopra et al.	2003/0055308	A1 3/2003	Friemel et al.
6,599,256	B1	7/2003	Acker et al.	2003/0060820	A1 3/2003	Maguire et al.
6,612,988	B2	9/2003	Maor et al.	2003/0187371	A1 10/2003	Vortman et al.
6,613,004	B1	9/2003	Vitek et al.	2004/0030251	A1 2/2004	Ebbini et al.
6,613,005	B1*	9/2003	Friedman A61N 7/02 600/371	2004/0059265	A1 3/2004	Candy et al.
6,618,608	B1	9/2003	Watkins et al.	2004/0068186	A1 4/2004	Ishida et al.
6,618,620	B1	9/2003	Freundlich et al.	2004/0082868	A1 4/2004	Campbell et al.
6,626,854	B2	9/2003	Friedman et al.	2004/0116809	A1 6/2004	Chow et al.
6,626,855	B1	9/2003	Weng et al.	2004/0122316	A1 6/2004	Satoh
6,629,929	B1	10/2003	Jago et al.	2004/0122323	A1 6/2004	Vortman et al.
6,645,162	B2	11/2003	Friedman et al.	2004/0143187	A1 7/2004	Biagi et al.
6,652,461	B1	11/2003	Levkovitz et al.	2004/0147919	A1 7/2004	Behl et al.
6,666,833	B1	12/2003	Friedman et al.	2004/0210134	A1 10/2004	Hynynen et al.
6,676,601	B1	1/2004	Lacoste et al.	2004/0210135	A1 10/2004	Hynynen et al.
6,676,602	B1	1/2004	Barnes et al.	2004/0236253	A1 11/2004	Vortman et al.
6,679,855	B2	1/2004	Horn et al.	2004/0236523	A1 11/2004	Taylor
6,705,994	B2	3/2004	Vortman et al.	2004/0267126	A1 12/2004	Takeuchi
6,719,694	B2	4/2004	Weng et al.	2005/0033201	A1 2/2005	Takahashi et al.
6,733,450	B1	5/2004	Alexandrov et al.	2005/0096542	A1 5/2005	Weng et al.
6,735,461	B2	5/2004	Vitek et al.	2005/0131301	A1 6/2005	Peszynski et al.
6,761,691	B2	7/2004	Tsuzuki	2005/0154304	A1 7/2005	Robinson
6,770,031	B2	8/2004	Hynynen et al.	2005/0199058	A1 9/2005	Danz et al.
6,770,039	B2	8/2004	Zhong et al.	2005/0203444	A1 9/2005	Schonenberger et al.
6,788,619	B2	9/2004	Calvert	2005/0240126	A1 10/2005	Foley et al.
6,790,180	B2	9/2004	Vitek	2005/0251046	A1 11/2005	Yamamoto et al.
6,805,129	B1	10/2004	Pless et al.	2006/0052661	A1 3/2006	Gannot et al.
				2006/0052701	A1 3/2006	Carter et al.
				2006/0052706	A1 3/2006	Hynynen et al.
				2006/0058671	A1* 3/2006	Vitek A61N 7/02 600/447
				2006/0058678	A1 3/2006	Vitek et al.
				2006/0106300	A1 5/2006	Seppenwoolde et al.
				2006/0173307	A1 8/2006	Amara et al.

(56)

References Cited

U.S. PATENT DOCUMENTS

2006/0173321	A1	8/2006	Kubota et al.	
2006/0173385	A1	8/2006	Lidgren et al.	
2006/0184034	A1	8/2006	Haim et al.	
2006/0184069	A1	8/2006	Vaitekunas	
2006/0206105	A1	9/2006	Chopra et al.	
2006/0229594	A1	10/2006	Francischelli et al.	
2006/0235302	A1	10/2006	Grossman et al.	
2006/0253026	A1	11/2006	Gueck et al.	
2007/0016039	A1	1/2007	Vortman et al.	
2007/0055140	A1	3/2007	Kuroda	
2007/0066897	A1	3/2007	Sekins et al.	
2007/0073135	A1	3/2007	Lee et al.	
2007/0098232	A1	5/2007	Matula et al.	
2007/0167781	A1	7/2007	Vortman et al.	
2007/0167798	A1	7/2007	Cai et al.	
2007/0197918	A1	8/2007	Vitek et al.	
2007/0219470	A1	9/2007	Talish et al.	
2007/0239062	A1	10/2007	Chopra et al.	
2007/0265560	A1	11/2007	Soltani et al.	
2007/0276237	A1	11/2007	Li	
2008/0027342	A1	1/2008	Rouw et al.	
2008/0030104	A1	2/2008	Prus	
2008/0031090	A1	2/2008	Prus et al.	
2008/0033278	A1	2/2008	Assif	
2008/0082026	A1	4/2008	Schmidt et al.	
2008/0103558	A1	5/2008	Wenzel et al.	
2008/0108900	A1	5/2008	Lee et al.	
2008/0125660	A1	5/2008	Yao et al.	
2008/0183077	A1	7/2008	Moreau-Gobard et al.	
2008/0228081	A1	9/2008	Becker et al.	
2008/0312562	A1	12/2008	Routh et al.	
2009/0088623	A1	4/2009	Vortman et al.	
2009/0093721	A1	4/2009	Katsuyama	
2009/0096450	A1	4/2009	Roland	
2009/0118619	A1	5/2009	Oshiki	
2009/0230823	A1*	9/2009	Kushculey	A61N 7/02 310/366
2010/0030076	A1	2/2010	Vortman et al.	
2010/0056962	A1	3/2010	Vortman et al.	
2010/0125193	A1	5/2010	Zadicario	
2010/0179425	A1	7/2010	Zadicario	
2010/0268088	A1	10/2010	Prus et al.	
2010/0274130	A1	10/2010	Anand et al.	
2010/0318002	A1	12/2010	Prus et al.	
2011/0034800	A1*	2/2011	Vitek	A61B 5/055 600/411
2011/0094288	A1	4/2011	Medan et al.	
2011/0130663	A1	6/2011	Raju et al.	
2011/0137147	A1	6/2011	Skliar et al.	
2011/0251527	A1	10/2011	Kushculey et al.	
2011/0270136	A1	11/2011	Vitek et al.	
2012/0083695	A1	4/2012	Napolitano et al.	
2013/0077441	A1	3/2013	Ramamurthy et al.	

FOREIGN PATENT DOCUMENTS

CN	101137329	A	3/2008
CN	102348481	A	2/2012
CN	102946945	A	2/2013
CN	103140261	A	6/2013
DE	10102317	A1	8/2002
EP	0031614	A1	7/1981
EP	174920	A1	3/1986
EP	272347	A1	6/1988
EP	0320303		6/1989
EP	450334	A2	10/1991
EP	462311	A1	12/1991
EP	467690	A2	1/1992
EP	0558029		9/1993
EP	627206	A2	12/1994
EP	734742	A2	10/1996
EP	875203	A2	11/1998
EP	1582886	A1	10/2005
EP	1591073	A1	11/2005

EP	1774920		4/2007
EP	1936404		6/2008
EP	2429656	B1	6/2013
EP	2563475	B1	8/2014
FR	2692999	A1	12/1993
FR	280661	1	9/2001
GB	2019565	A	10/1979
JP	07/184907		7/1995
JP	00/166940		6/2000
JP	01/516075		9/2001
JP	02/530145		9/2002
JP	2006-203653	T	2/2006
JP	5066569	B2	11/2012
JP	5087007	B2	11/2012
WO	91/15999	A1	10/1991
WO	91/19332	A1	12/1991
WO	WO-93/15415	A1	8/1993
WO	WO-95/14505		6/1995
WO	WO-97/17018	A1	5/1997
WO	00/78232	A1	12/2000
WO	01/43640	A2	6/2001
WO	01/80708	A2	11/2001
WO	WO-01/80709		11/2001
WO	01/80708	A3	3/2002
WO	WO-02/44753		6/2002
WO	WO-03/013654		2/2003
WO	03/070105	A1	8/2003
WO	WO-2004/021044	A1	3/2004
WO	2004/066856	A1	8/2004
WO	WO-2005/038745		4/2005
WO	2005/058029	A2	6/2005
WO	2006/018686	A1	2/2006
WO	2006/021851	A1	3/2006
WO	WO-2006/025001	A1	3/2006
WO	WO-2007/051066		5/2007
WO	WO-2007/073551		6/2007
WO	2007/093998	A1	8/2007
WO	2008/015523	A2	2/2008
WO	WO-2008/039449		4/2008
WO	WO-2008/119054		10/2008
WO	WO-2009/081339		7/2009
WO	WO-2009085466	A1	7/2009
WO	WO-2010/058292		5/2010
WO	WO-2010/082135		7/2010
WO	WO-2010/119340		10/2010
WO	WO-2010/143072		12/2010
WO	WO-2011/013001		2/2011
WO	WO-2011/024074		3/2011
WO	2011/045669	A2	4/2011

OTHER PUBLICATIONS

Examination Report Received for European Patent Application No. 06820942.8, mailed on Dec. 11, 2014, 5 pages.

Examination Report Received for European Patent Application No. 07804649.7, mailed on Feb. 17, 2015, 5 pages.

Examination Report Received for European Patent Application No. 10720818.3, mailed on Sep. 11, 2012, 3 pages.

Examination Report Received for European Patent Application No. 10785194.1, mailed on Jan. 22, 2015, 5 pages.

Examination Report Received for European Patent Application No. 11743607.1, mailed on Sep. 18, 2013, 3 pages.

Examination Report Received for European Patent Application No. 11743611.3, mailed on Dec. 19, 2014, 5 pages.

Examination Report Received for Chinese Patent Application No. 200980153997.1, mailed on Oct. 20, 2014, 8 pages. (English Translation only).

Examination Report Received for European Patent Application No. 10709054.0, mailed on Dec. 22, 2014, 4 pages.

PCT International Patent Application No. PCT/IB2010/002143, International Preliminary Report on Patentability issued on Jan. 31, 2012, 8 pages.

PCT International Patent Application No. PCT/IB2010/002265, International Preliminary Report on Patentability issued on Feb. 28, 2012, 11 pages.

200680029730.8, "First Office Action", 200680029730.8 PRC, First Office Action, mailed on Apr. 24, 2010, 7 pages.

(56)

References Cited

OTHER PUBLICATIONS

- Examination Report in Chinese Patent Application No. 200980153997.1, mailed on Apr. 15, 2014, 7 pages.
- Examination Report in Chinese Patent Application No. 201080011633.2, mailed on Oct. 8, 2013, 9 pages.
- PCT/IB2003/005551 "International Search Report", PCT/IB2003/005551, filed on Dec. 1, 2003, by Vortman et al., International Search Report mailed Mar. 9, 2004, 3 pages.
- International Application Serial No. PCT/IB2003/005551, International Written Opinion mailed on Sep. 10, 2004.
- International Application Serial No. PCT/IB2004/001498, International Search Report and Written Opinion mailed on Aug. 31, 2004, 8 pages.
- International Application Serial No. PCT/IB2004/001512, International Preliminary Report on Patentability mailed on Nov. 25, 2005, 5 pages.
- International Application Serial No. PCT/IB2004/001512, International Search Report and Written Opinion mailed on Sep. 7, 2004, 7 pages.
- International Application Serial No. PCT/IB2005/002273, International Search Report and Written Opinion mailed on Dec. 20, 2005, 6 pages.
- International Application Serial No. PCT/IB2005/002413, International Search Report and Written Opinion mailed on Nov. 22, 2005, 8 pages.
- International Application Serial No. PCT/IB2006/001641, International Search Report and Written Opinion mailed on Sep. 25, 2006, 8 pages.
- International Application Serial No. PCT/IB2006/003300, International Search Report and Written Opinion mailed on Feb. 14, 2008, 7 pages.
- International Application Serial No. PCT/IB2007/001079, International Search Report and Written Opinion mailed on Dec. 10, 2007, 11 pages.
- International Application Serial No. PCT/IB2007/001079, Partial International Search Report and Written Opinion mailed on Sep. 25, 2007.
- International Application Serial No. PCT/IB2007/002134, International Search Report and Written Opinion mailed on Dec. 13, 2007, 8 pages.
- International Application Serial No. PCT/IB2007/002140, International Search Report and Written Opinion mailed on Dec. 29, 2008, 7 pages.
- International Application Serial No. PCT/IB2008/003069, International Search Report and Written Opinion mailed on Apr. 27, 2009, 10 pages.
- International Application Serial No. PCT/IB2010/000189, International Search Report and Written Opinion mailed on Jun. 1, 2010, 11 pages.
- International Application Serial No. PCT/IB2010/00097, International Search Report and Written Opinion mailed on Jul. 29, 2010, 9 pages.
- International Application Serial No. PCT/IB2010/002265, Partial International Search Report mailed on Mar. 11, 2011, 4 pages.
- International Application Serial No. PCT/IB2011/001293, International Preliminary Report on Patentability mailed on Nov. 8, 2012, 9 pages.
- International Application Serial No. PCT/IB2011/001293, International Search Report and Written Opinion mailed on Dec. 19, 2011, 12 pages.
- International Application Serial No. PCT/IB2011/001375, International Search Report and Written Opinion mailed on Nov. 10, 2011, 12 pages.
- International Application Serial No. PCT/IL2002/000477, International Written Opinion mailed on Feb. 25, 2003, 9 pages.
- Botros et al., "A hybrid computational model for ultrasound phased-array heating in presence of strongly scattering obstacles," *IEEE Trans. on Biomed. Eng.*, vol. 44, No. 11, pp. 1039-1050 (Nov. 1997).
- Cain et al., "Concentric-ring and Sector-vortex Phased-array Applicators for Ultrasound Hyperthermia," *IEEE Trans. on Microwave Theory & Techniques*, vol. MTT-34, No. 5, pp. 542-551 (May 1986).
- Chen et al., "MR Acoustic Radiation Force Imaging: Comparison of Encoding Gradients," 1 page, (Mar. 2007).
- Cline et al., "Focused US system for MR imaging-guide tumor ablation," *Radiology*, v. 194, No. 3, pp. 731-737 (Mar. 1995).
- Cline et al., "MR Temperature mapping of focused ultrasound surgery," *Magnetic Resonance in Medicine*, vol. 32, No. 6, pp. 628-636 (1994).
- Cline et al., "Simultaneous magnetic resonance phase and magnitude temperature maps in muscle," *Magnetic Resonance in Medicine*, vol. 35, No. 3, pp. 309-315 (Mar. 1996).
- Daum et al., "Design and evaluation of a feedback based phased array system for ultrasound surgery," *IEEE Trans. Ultrason. Ferroelec. Freq. Control*, vol. 45, No. 2, pp. 431-434 (Mar. 1998).
- de Senneville et al., "Real-time adaptive methods for treatment of mobile organs by MRI-controlled high-intensity focussed Ultrasound," *Magnetic Resonance in Medicine* 57:319-330 (2007).
- Fjield et al., "The Combined Concentric-ring and Sector-vortex Phased Array for MRI Guided Ultrasound Surgery," *IEEE Trans. on Ultrasonics, Ferroelectrics and Freq. Cont.*, vol. 44, No. 5, pp. 1157-1167 (Sep. 1997).
- Herbert et al., "Energy-based adaptive focusing of waves: application to ultrasonic transcranial therapy," 8th Intl. Symp. on Therapeutic Ultrasound., 3 pages (Sep. 2009).
- Huber et al., "A New Noninvasive Approach in Breast Cancer Therapy Using Magnetic Resonance Imaging-Guided Focussed Ultrasound Surgery," *Cancer Research* 61, 8441-8447 (Dec. 2001).
- Jolesz et al., "Integration of interventional MRI with computer-assisted surgery," *J. Magnetic Resonance Imaging*. 12:69-77 (2001).
- Kohler et al., "Volumetric HIFU Ablation guided by multiplane MRI thermometry," 8th Intl. Symp. on Therapeutic Ultrasound, edited by E.S. Ebbini, U. of Minn. pp. 228-230 (Sep. 2009).
- Kowalski et al., "Optimization of electromagnetic phased-arrays for hyperthermia via magnetic resonance temperature estimation," *IEEE Trans. on Biomed. Eng.*, vol. 49, No. 11, pp. 1229-1241 (Nov. 2002).
- Maxwell et al., "Noninvasive thrombolysis using pulsed ultrasound cavitation therapy—Histotripsy," Abstract, U.S. Natl. Lib. of Med., NIH, *Ultrasound Med. Biol.* (Oct. 23, 2009).
- McDannold et al., "MRI evaluation of the thermal ablation of tumors and focused ultrasounds," *JMRI* vol. 8, No. 1, pp. 91-100 (1998).
- McDannold et al., "Magnetic resonance acoustic radiation force imaging," *Med. Phys.* vol. 35, No. 8, pp. 3748-3758 (Aug. 2008).
- Medel et al., "Sonothrombolysis: An emerging modality for the management of stroke," *Neurosurgery*, vol. 65, No. 5, pp. 979-993 (Nov. 2009).
- Mougenot et al., "MR monitoring of the near-field HIFU heating," 8th Intl. Symp. on Therapeutic Ultrasound, edited by E.S. Ebbini, U. of Minn. pp. 159-161 (Sep. 2009).
- Vimeux et al., "Real-time control of focused ultrasound heating based on rapid MR thermometry," *Investig. Radiology*, vol. 43, No. 3, pp. 190-193 (1999).
- Vykhodtseva et al., "MRI detection of the thermal effects of focused ultrasound on the brain," *Ultrasound in Med. & Biol.*, vol. 26, No. 5, pp. 871-880 (2000).
- "How is Ablatherm treatment performed?" http://www.edap-hifu.com/eng/physicians/hifu/3c_treatment_treat-description.htm, accessed Jan. 3, 2003 (3 pages).
- "What is HIFU? HIFU: High Intensity Focused Ultrasound," http://www.edap-hifu.com/eng/physicians/hifu2a_hifu_overview.htm, accessed Jan. 3, 2003 (1 page).
- "About HIFU, What are the physical principles?" http://www.edap-hifu.com/eng/physicians/hifu/2c_hifu_physical.htm, accessed Jan. 3, 2003 (2 pages).
- "How does HIFU create a lesion?" http://www.edap-hifu.com/eng/physicians/hifu/2d_hifu_lesion.htm, accessed Jan. 3, 2003 (1 page).
- "Prostate Cancer Phase I Clinical Trials Using High Intensity Focused Ultrasound (HIFU)," *Focus Surgery*, <http://www.focus-surgery.com/PCT%20Treatment%20with%20HIFU.htm>, accessed Jan. 3, 2003 (2 pages).
- "Abstract" *Focus Surgery*, <http://www.focus-surgery.com/Sanghvi.htm>, accessed Jan. 3, 2003.

(56)

References Cited

OTHER PUBLICATIONS

Exablate 2000 Specification, InSightec, Ltd. (2 pages) Pub 280002 (Mar. 2007).

FDA Approves Exablate 2000 as Non-invasive surgery for Fibroids, Oct. 22, 2004 (4 pages).

McGough et al., "Direct Computation of Ultrasound Phased-Array Driving Signals from a Specified Temperature Distribution for Hyperthermia," IEEE Transactions on Biomedical Engineering, vol. 39, No. 8, pp. 825-835 (Aug. 1992).

McDonnald et al. "Usefulness of MR Imaging-Derived Thermometry and Dosimetry in Determining the Threshold for Tissue Damage Induced by Thermal Surgery in Rabbits," Radiology, vol. 216, No. 2000 pp. 517-523 (2000).

Suprijanto et al. "Displacement Correction Scheme for MR-Guided Interstitial Laser Therapy," Ellis RE, Peters TM (Eds.): MiCCAI , LNCS 2879, pp. 399-407 (2003).

Shmatukha et al. "Correction of Proton Resonance Frequency Shift Temperature Maps for Magnetic Field Disturbances Caused by Breathing," Physics in Medicine and Biology, vol. 51, No. 18 pp. 4689-4705 (2006).

De Senneville et al., "An Optimised Multi-Baseline Approach for On-Line MR-Temperature Monitoring on Commodity Graphics Hardware," Biomedical Imaging, pp. 1513-1516 (2008).

Vigen et al., "Triggered, Navigated, Multi-Baseline Method for Proton Resonance Frequency Temperature Mapping with Respiratory Motion," Magnetic Resonance in Medicine, vol. 50, pp. 1003-1010 (2003).

International Search Report and Written Opinion mailed Sep. 7, 2011 for International Application No. PCT/IB2010/002757 (16 pages).

International Preliminary Report on Patentability for PCT/IB2010/002757 dated Apr. 17, 2012.

* cited by examiner

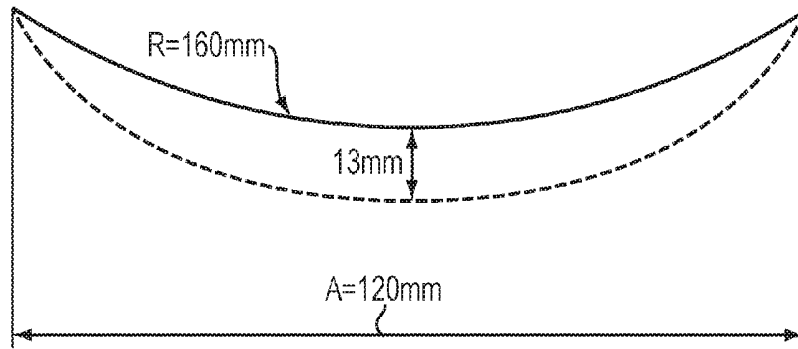


FIG. 1

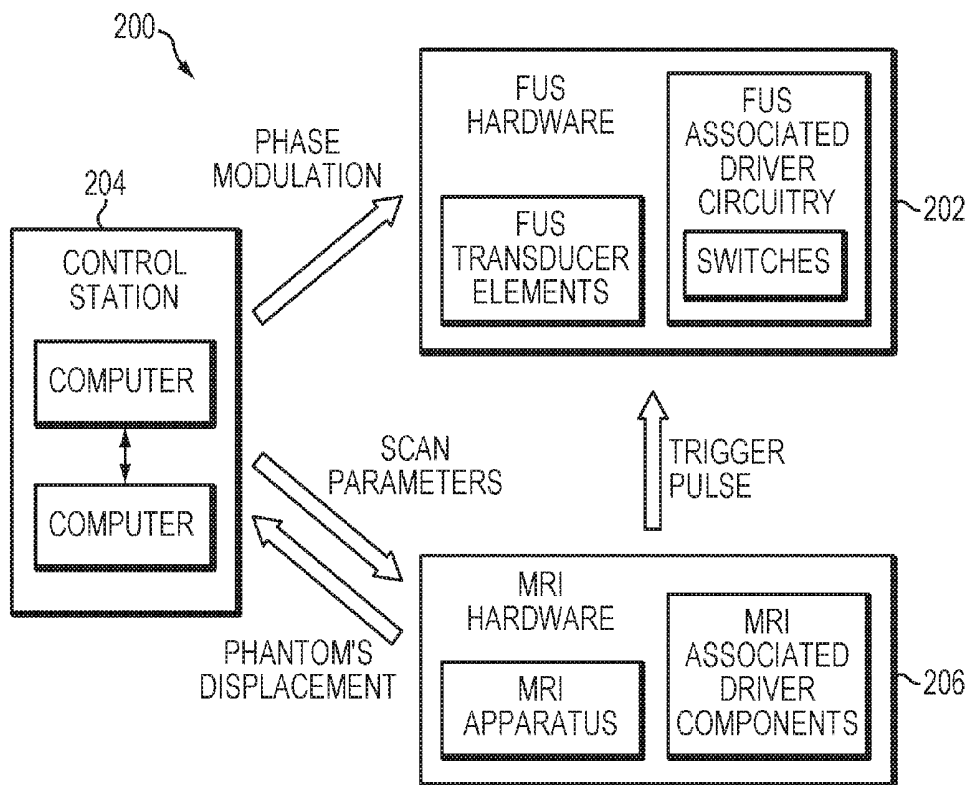


FIG. 2

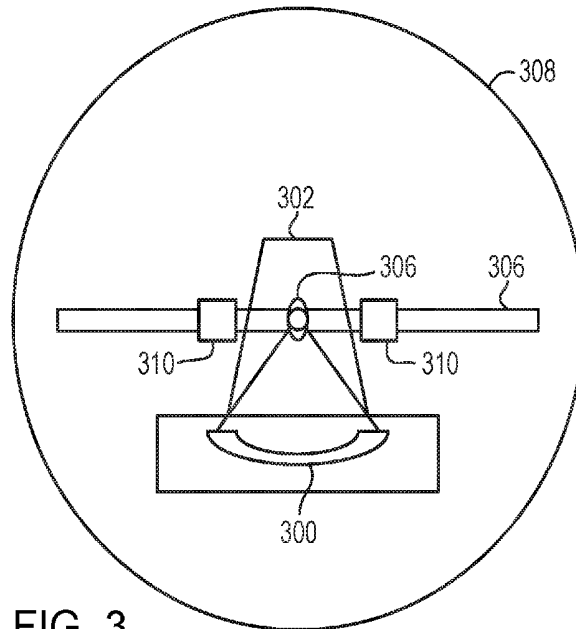


FIG. 3
PRIOR ART

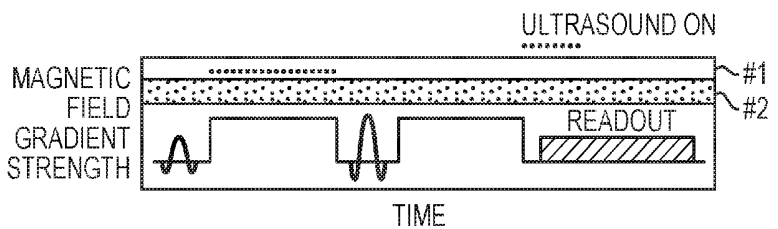


FIG. 4A
PRIOR ART

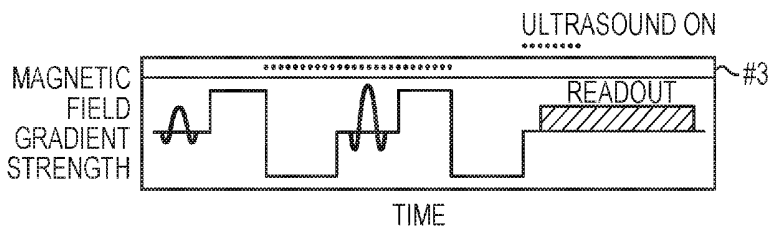


FIG. 4B
PRIOR ART

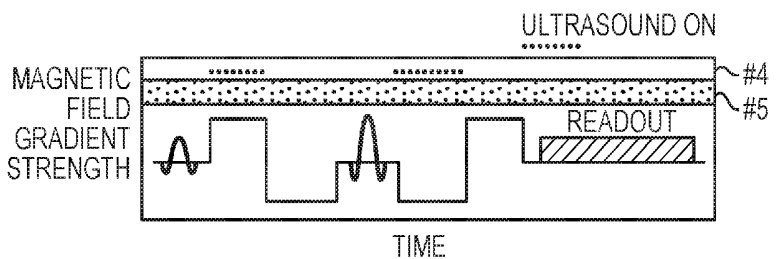


FIG. 4C
PRIOR ART

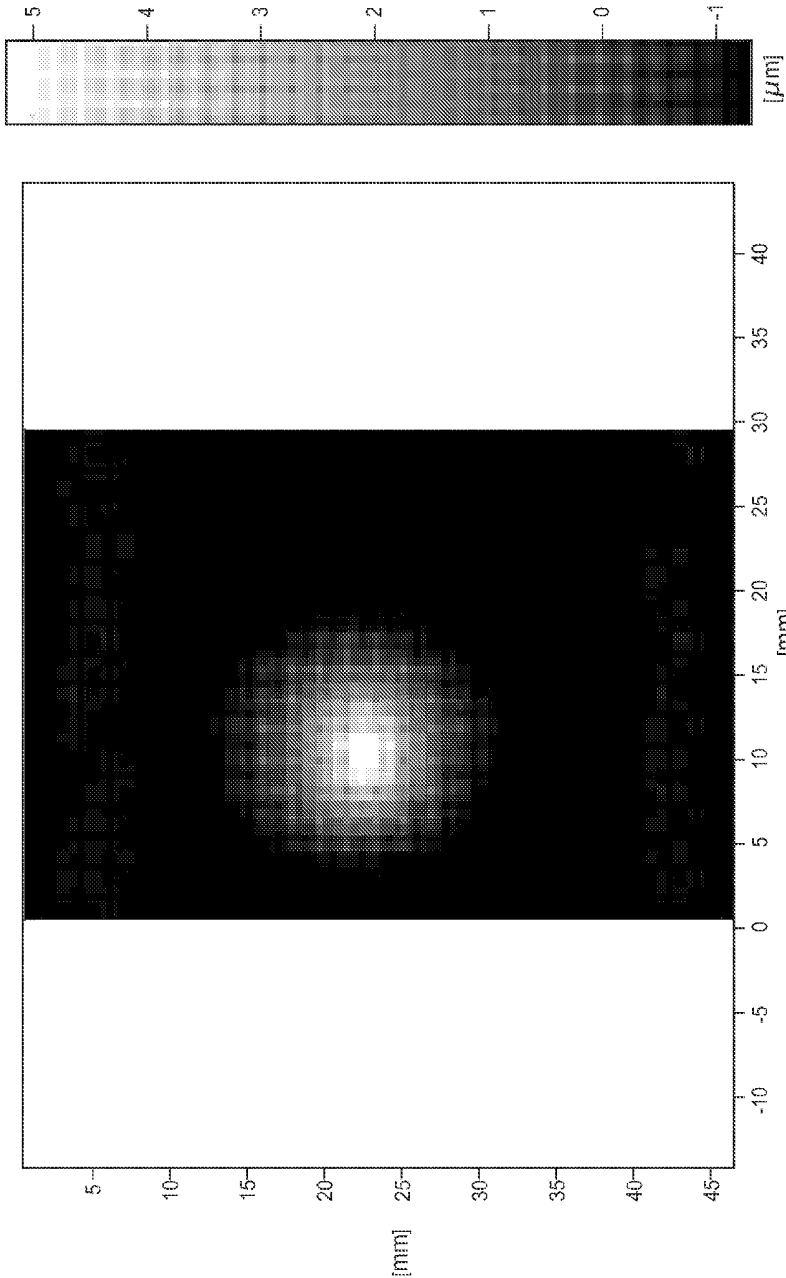


FIG. 5

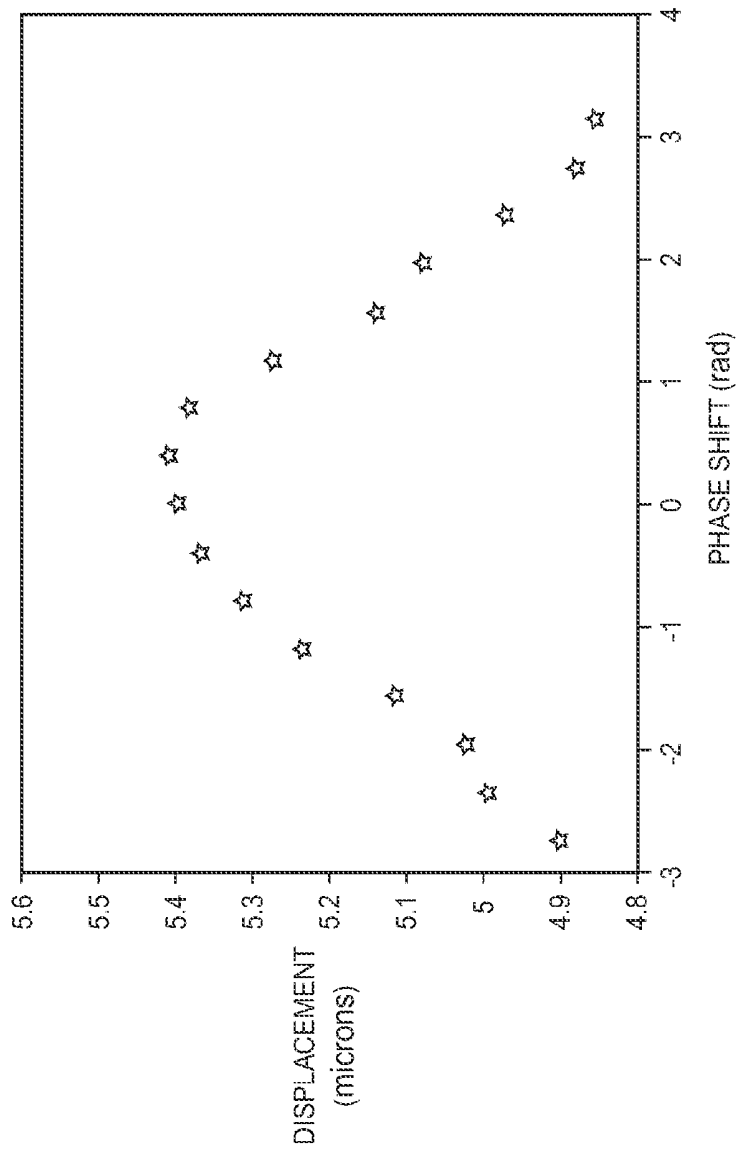


FIG. 6

MAPPING ULTRASOUND TRANSDUCERS**CROSS-REFERENCE TO RELATED APPLICATION**

This application is a Divisional Application of Ser. No. 12/904,655, filed Oct. 14, 2010, which claims priority to and the benefit of U.S. Provisional Patent Application No. 61/251,450, filed on Oct. 14, 2009, both of which are incorporated herein by reference.

FIELD OF THE INVENTION

The present invention relates, generally, to systems and methods for mapping ultrasound transducers. In particular, various embodiments are directed to improving the quality of the ultrasound focus using experimental feedback.

BACKGROUND

Focused ultrasound (i.e., acoustic waves having a frequency greater than about 20 kilohertz) can be used to image or therapeutically treat internal body tissues within a patient. For example, ultrasonic waves may be used to ablate tumors, eliminating the need for the patient to undergo invasive surgery. For this purpose, a piezo-ceramic transducer is placed externally to the patient, but in close proximity to the tissue to be ablated (“the target”). The transducer converts an electronic drive signal into mechanical vibrations, resulting in the emission of acoustic waves. The transducer may be shaped so that the waves converge in a focal zone. Alternatively or additionally, the transducer may be formed of a plurality of individually driven transducer elements whose phases can each be controlled independently from one another. Such a “phased-array” transducer facilitates steering the focal zone to different locations by adjusting the relative phases between the transducers. Magnetic resonance imaging (MRI) may be used to visualize the patient and target, and thereby to guide the ultrasound beam.

The effectiveness of ultrasound therapy depends on the accuracy of the focus location, the sharpness and shape of the focal zone, and the avoidance of “hot spots” (i.e., regions of high ultrasound intensity) outside the target. Transducer elements that are not properly configured or controlled can lead to improper focus location and reduced focus quality, resulting in less effective therapy, and possibly damage to healthy tissue surrounding the target. It is therefore desirable to correct any mechanical misconfigurations. Improper transducer configuration may result from manufacturing errors, inadvertent shifting of transducer elements from their expected locations during use or repair, deformation of the transducer due to thermal expansion, or a combination of these and other effects. Even slight locational deviations can have significant effects on the quality of the transducer output. For example, as illustrated in FIG. 1, if the height of a curved transducer surface having a width of 120 mm and a nominal radius of curvature of 160 mm changes by only 1 mm, the ultrasound focus shifts by about 13 mm. In a phased array, deviations of the transducer locations from the intended locations can be compensated for by adjusting the phases with which the elements are driven. This procedure is hereinafter referred to as “mapping” the transducer.

One approach to mapping a phased-array transducer surface involves driving each transducer element individually to produce an acoustic wave pulse in water; measuring the arrival of the acoustic wave pulse in three locations using a hydrophone; determining for each location the time of flight,

and thus the distance, from the transducer element; and calculating the coordinates of the element location by triangulation from the three measurements. Based on the intended and the measured actual locations of the transducer elements, the necessary phase adjustments can be calculated. This method is described in U.S. Pat. No. 7,535,794 to Prus et al., which is hereby incorporated herein by reference in its entirety. In addition to a hydrophone, implementation of the method requires other auxiliary equipment, such as an amplifier and data-acquisition module. Further, to avoid damaging the hydrophone, the mapping is typically performed at transducer power levels significantly below those used during normal operation, which can undermine the validity of the adjustments under therapeutic conditions. Alternative transducer mapping methods that do not have these drawbacks are therefore desirable.

SUMMARY

The present invention generally provides methods for mapping a phased-array transducer by generating an ultrasound focus and improving the focus quality based on experimental feedback. In various embodiments, one or more focus-affecting parameters (such as the phase and/or amplitude of one or more transducer elements) are varied, and the resulting variation of the focus quality is measured (e.g., in terms of an integral or peak intensity, focus size, or intensity profile). The focus-affecting parameter(s) are then set to values for which the focus quality is optimized. For example, the relative phases of the transducer elements may be fine-tuned one at a time to maximize the intensity at the focus. In this manner, unwanted phase shifts resulting from electronic delays or other sources may be corrected, and any deviations from the intended locations of the transducer elements may be compensated for without the need to explicitly determine the actual transducer locations.

During the mapping procedure, the ultrasound focus may be generated in a phantom. To determine the focus quality, the focus may be visualized, for example, by magnetic-resonance acoustic radiation force imaging (MR-ARFI)—an MRI technique measuring minute material displacements that are caused by and indicative of the acoustic field. The displacement increases with the acoustic field intensity. Thus, by adjusting the transducer element phases (and/or amplitudes or other focus-affecting parameters) so as to increase the material displacement in the phantom, the intensity at the focus and, consequently, the focus quality may be improved. Advantageously, MR-ARFI facilitates mapping the transducer at normal operational power levels, which increases the relevance and applicability of any mapping-based adjustments to the subsequent therapeutic operation. Further, the ultrasound focus may be imaged during the mapping procedure with the same MRI or other imaging apparatus (e.g., X-ray-based computer-aided tomography or other tomographic modality) that is used to guide the focus during therapeutic operation, and, consequently, additional (auxiliary) mapping equipment is not needed.

In one aspect, the invention provides a method for improving and/or optimizing the focus of an ultrasound transducer having a plurality of transducer elements. The method includes driving the plurality of transducer elements so as to generate an ultrasound focus, varying a focus-affecting parameter associated with one or more of the transducer elements, measuring a resulting variation on the quality of the focus, and selecting parameter value(s) that result in the best focus quality. The focus-varying parameter(s) may be or include the phase and/or amplitude of one of the transducer

elements (or a group of jointly driven elements), or a phase/amplitude gradient or other parameter determining relative phase/amplitude settings of multiple transducer elements that form the whole transducer or a region thereof, or a combination of such parameters. In embodiments in which the location and/or orientation of the transducer or transducer elements are susceptible to direct user control, the focus-varying parameter(s) may, alternatively or additionally, include such location(s) and/or orientation(s). Other focus-varying parameters include, e.g., the drive frequency of the transducer. The quality measurement may involve, for instance, scanning a profile of the focus (e.g., measuring the intensity in the focus region along a line through the focus), measuring the peak (i.e., maximum) intensity of the focus, and/or measuring the integral intensity or size of the focus (i.e., integrating the intensity or area over the cross-section of the focus, where the cross-section is defined, e.g., by the regions in which the intensity is more than a set fraction, e.g., half or 1/e, of the peak intensity).

In certain embodiments, varying the focus-varying parameter(s) and measuring the resultant focus quality includes driving a selected one of the transducer elements at a variable phase while driving the other transducer elements at a constant phase (thereby varying the focus quality); determining the phase difference, if any, between the constant and variable phases where the focus quality is optimized; and, if the phase difference is non-zero, adjusting the relative phase of the selected transducer element based thereon. These steps may be repeated for the remaining transducer elements.

In some embodiments, the quality measurement comprises measuring the displacement associated with the focus using, e.g., ARFI. The ARFI measurement may involve applying a sequence of MR field gradients (such as, e.g., repeated bipolar gradients). The ultrasound focus may be generated by an ultrasound pulse synchronized with the sequence of MR field gradients. The method may further involve providing a phantom (which may include a material having low tensile strength and/or a small elastic modulus), and generating the ultrasound focus and measuring the focus quality in the phantom.

In another aspect, the invention is directed to a method for mapping an ultrasound transducer comprising a plurality of transducer elements. The method includes driving the transducer elements so as to generate an ultrasound focus, and measuring a displacement associated with the focus by ARFI. Further, it involves varying the displacement by driving one of the transducer elements at a variable phase while driving the other transducer elements at a constant phase, and determining the phase difference, if any, between the constant and variable phases at which the displacement is maximized. If the phase difference is non-zero, the relative phase of the selected transducer element is adjusted based on the phase difference. The phase difference may also be used to determine the location of the selected transducer element. The application of a variable phase and determination of the phase difference between the variable and constant phases may be repeated for the remaining transducer elements. The ultrasound focus may be generated, and the displacement be measured, in a phantom, which may have a low tensile strength and/or a small elastic modulus. Acoustic-radiation force imaging to measure the displacement may involve applying a sequence of MR field gradients, e.g., a sequence including repeated bipolar gradients. The transducer elements may be driven so as to generate an ultrasound pulse synchronized with the sequence of MR field gradients.

The above-described mapping method(s) may be varied by grouping transducer elements and mapping a group, rather

than an individual element, at a time. Accordingly, in yet another aspect of the invention, a selected group of transducer elements is driven at a variable phase while other groups of transducer elements are driven at a constant phase, and the phase difference between the constant and variable phases that maximizes the displacement associated with the focus may be determined and form the basis for adjusting the relative phase of the selected group of transducer elements.

In a further aspect, the invention is directed to a method for controlling an ultrasound transducer having a plurality of transducer elements. The method includes mapping the ultrasound transducer as described above by driving the transducers to generate an ultrasound focus; varying a focus-affecting parameter associated with at least one of the elements and measuring a resulting variation on a quality of the focus; and selecting a value of the parameter associated with a best focus quality. In particular, in some embodiments, mapping may include measuring a displacement associated with the focus (e.g., using ARFI), and determining, for each of the transducer elements, the relative phase associated with that element by driving the transducer element at a variable phase while driving the other transducer elements at a constant phase and determining the phase difference between the constant and variable phases that maximizes the displacement. The method further includes controlling the transducer based on the mapping step (e.g., by adjusting the relative phase of each transducer for which the phase difference is non-zero). Controlling the transducer may include driving the elements to produce outputs converging at a focus corresponding to a target treatment region. Mapping may be carried out using a phantom, and may be repeated in between therapeutic applications of ultrasound.

BRIEF DESCRIPTION OF THE DRAWINGS

The foregoing will be more readily understood from the following detailed description of the invention in conjunction with the drawings, wherein:

FIG. 1 is a schematic drawing illustrating the effect of a change in the transducer surface on the focus location;

FIG. 2 is a block-diagram illustrating, on a high level, a system for performing transducer mapping in accordance with some embodiments of the invention;

FIG. 3 is a schematic diagram illustrating, in more detail, the configuration of a transducer mapping system in accordance with some embodiments;

FIGS. 4A-4C illustrate various MR-ARFI sequences in accordance with some embodiments;

FIG. 5 is an image of material displacements in an ultrasound focus region in accordance with some embodiments;

FIG. 6 is a graph illustrating material displacement in the focus center as a function of the phase of an individual transducer element, as it may be used in mapping methods in accordance with various embodiments; and

FIG. 7 is a flow chart illustrating an approach to mapping an ultrasound transducer array in accordance with various embodiments of the invention.

DETAILED DESCRIPTION

FIG. 2 illustrates in block-diagram form an exemplary system for performing transducer mapping in accordance with various embodiments hereof, and the interplay between the different system components. The system includes, first, the focused ultrasound transducer hardware 202, which itself includes the transducer array, a frequency generator for providing an electronic drive signal, and drivers for the trans-

ducer elements. (As used herein, the term “transducer” refers to the entire array, as distinguished from the individual transducer elements.) Each driver contains electronic circuitry for setting the phase of the respective transducer element(s), and optionally also for adjusting the amplitude(s) of vibrations. In some embodiments, each transducer elements is independently controllable by a separate associated driver. In alternative embodiments, driver elements are organized (e.g., via hardwiring or configurable switches) into multiple groups of elements driven collectively by the same driver. The drivers are controlled by a control station 204, which may include a computer system specially designed for use with the transducer hardware, or a general-purpose computer (or cluster of computers) having suitable (and conventional) driver software installed.

The mapping system 200 further includes MRI (or other tomographic or imaging) hardware 206, i.e., an MRI apparatus and related driver components, which is likewise controlled by the control station 204. Again, control functionality for the MRI hardware 206 may be implemented in a special-purpose computer system, or in conventional driver software installed on a general-purpose computer system. The transducer hardware 202 and MRI hardware 206 may be controlled by the same computer within control station 204, or by separate computers that are in communication with one another. Further, computational functionality for processing and analyzing the images acquired with the MRI hardware 206 may be integrated with the MRI apparatus, or implemented (e.g., as a separate software module) in control station 204.

During the mapping procedure, the control station 204 sends control signals to the ultrasound transducer hardware 202 to vary one or more parameters affecting the focus properties. For example, the control station 204 may cause a phase modulation of a particular transducer element or group of elements. Further, the control station 204 provides scan parameters, or other signals triggering and/or controlling image acquisition, to the MRI or other imaging hardware 206. The relative timing of the ultrasound generation and/or modulation with respect to image acquisition may be specified in an imaging sequence, which may be programmed into the control station 204. The control station 204 may then send trigger signals to the ultrasound transducer hardware 202 and the MRI hardware 206, ensuring correct timing between the signals in accordance with the imaging sequence. Alternatively, the control station 204 may communicate a time-delay parameter, which specifies the time delay between the RF pulses and ultrasound pulses, to the MRI hardware 206, which sends a corresponding trigger pulse directly to the ultrasound transducer hardware 204.

The acquired images are processed to determine one or more parameter(s) indicative of the focus quality, which are used in the control station 204 for subsequent mapping steps. For example, in MR-ARFI-based systems, a material displacement indicative of the intensity in the focus is computationally extracted from the images, and the transducer is iteratively adjusted so as to increase the material displacement. Similarly, if thermal MRI is employed, the mapping process involves maximizing the temperature, and thus intensity, in the focus. In general, any imaging technique that provides images suitable for determining focus quality may be used. Depending on the contemplated ultrasound application, the “quality” of the focus may be expressed by different parameters. For therapeutic applications involving targeted tissue destruction, for example, the focus quality may be measured in terms of a peak intensity or total power delivered (corresponding to an integrated intensity over the focus cross

section). If the target area is small, the focus size may be relevant (a smaller focus area generally corresponding to higher focus quality). In some applications (e.g., tissue heating for palliative purposes), homogeneity of the intensity focus area may be important, and focus quality may, accordingly, be measured, at least in part, by the “smoothness” of an intensity profile through the focus.

FIG. 3 schematically illustrates an experimental setup for mapping an ultrasound transducer using tissue displacement as an indicator of focus quality. During the mapping procedure, the transducer 300 is driven so as to focus an ultrasound wave pulse into a phantom 302, which comprises or consists of a material that responds to acoustic pressure in a detectable manner. The ultrasound wave exerts acoustic radiation pressure onto the phantom material along its path. At the focus 304, where waves from the individual transducer elements converge, this pressure is highest, resulting in a temporary local displacement of the material in the longitudinal direction and/or in shear waves that propagate radially away from the focus. By using a soft phantom that responds to acoustic pressure with large enough shear strain (e.g., with a shear strain of at least 10^{-2}), a detectable displacement field that directly reflects the acoustic field may be obtained. Suitable phantom materials have high tensile strength (e.g., higher than 100 kPa) and small elastic moduli (e.g., Young’s modulus less than 1 MPa), and may include or consist of jelly-like materials such as, e.g., Silicone Gel RTV6166, provided by General Electric Co., Waterford, N.Y.

The material displacement may be visualized in an imaging plane 306 using an imaging techniques such as, e.g., magnetic-resonance-based acoustic radiation force imaging (MR-ARFI). In MR-based imaging methods, the object to be imaged (here, the phantom) is placed in a relatively uniform static magnetic field having a field strength of, typically, between about 1.5 and about 3.0 Tesla. Such a field may be generated, for example, by a large cylindrical electromagnet coil 308. The static magnetic field causes hydrogen nuclei spins to align and precess about the general direction of the magnetic field. Radio frequency (RF) pulses and magnetic gradients are then superimposed on the static magnetic field to cause some of the aligned spins to alternate between a temporary high-energy non-aligned state and the aligned state, thereby inducing an RF response signal, called the MR echo or MR response signal, in the RF antenna 310.

In MR-ARFI, transient-motion or displacement-sensitizing magnetic field gradients are applied to the phantom by gradient coils, which are part of standard MRI systems and are typically located near the cylindrical electromagnet coil 308. When the ultrasound pulse is applied in the presence of such gradients, the resulting displacement is directly encoded into the phase of the MR response signal. For example, the gradient coils and transducer may be configured such that the ultrasound pulse pushes phantom material near the focus towards regions of the magnetic field with higher field strengths. In response to the resulting change in the magnetic field, the phase of the MR response signal changes proportionally, thereby encoding in the signal the displacement caused by the ultrasound radiation pressure.

To achieve high image contrast, the ultrasound pulse, encoding gradients, and RF pulse are precisely timed with respect to each other according to a suitable displacement-encoding sequence. FIGS. 4A-4C illustrate five exemplary MR-ARFI sequences that may be used in embodiments of the invention. These sequence diagrams illustrate the order in which the displacement-encoding magnetic field gradients (thin solid lines), ultrasound pulses (dotted lines), and RF pulses (thick solid lines) appear in time. Three different field

gradient sets are shown: two single lobes (a), repeated bipolars (b), and inverted bipolars (c). For gradient set (a), ultrasound may be applied during either the first or the second lobe. Similarly, for gradient set (c), ultrasound may be applied during the first or the second halves of the bipolars. In general, MR-ARFI sequences utilize magnetic field gradients that are synchronized with the ultrasound pulses. In preferred embodiments, a sequence like the repeated bipolar sequence (b) shown in FIGS. 4A-4C may be used.

An example of an MR-ARFI image of an ultrasound focus region is shown in FIG. 5. As shown, the material displacement with respect to an equilibrium position varies between about $-1\ \mu\text{m}$ and $5\ \mu\text{m}$, as indicated in the color-coding of the image. In general, the stronger the acoustic field intensity, the greater will be the maximum displacement at the center of the focus. The acoustic field intensity, in turn, is maximized when the elements of the ultrasound transducer emit acoustic waves that are all in phase at the focus position. If a transducer element is out of phase with respect to the others, the focus intensity in the center decreases. This relationship can be exploited to optimize the focus, and thus to map and adjust the transducer elements. Assuming, for example, that all but one of the transducer elements are properly configured, the correct phase of the last element can be determined by tuning the phase over a full cycle (e.g., between $-\pi$ and $+\pi$), measuring for each phase the displacement in the focus center, and then setting the phase to the value corresponding to the maximum displacement. FIG. 6 depicts the results of such an adjustment procedure. In the illustrated example, the material displacement over the full phase cycle of one element varies between about $4.85\ \mu\text{m}$ and about $5.4\ \mu\text{m}$. The maximum displacement occurs at about $0.12\ \text{rad}$. Consequently, the focus intensity and quality can be improved by introducing a phase shift of $0.12\ \text{rad}$ for the tested transducer element.

In certain embodiments, mapping of the full transducer array is accomplished by varying and adjusting the phase (and/or amplitude) of each element, one at a time, while driving the remaining elements at constant phase. Typically, after each element has been mapped independently, the focus quality has significantly improved. Since the necessary phase adjustments of the transducer elements are all interrelated, however, the focus may not yet be optimal after one iteration. Therefore, in some embodiments, the procedure may be repeated iteratively. With each iteration, the phase adjustments made to maximize the displacement in the focus will, generally, decrease. Thus, a termination condition may be defined by setting a threshold value for phase adjustments, below which further adjustments are deemed immaterial or not clinically necessary. The number of iterations required to reach the termination condition may depend on the order in which the transducer elements are mapped. A mathematical algorithm, for example a "greedy algorithm" as known to persons of skill in the art, may be used to select a mapping order that results in fast convergence of the phase settings. In certain alternative embodiments, the transducer elements may be grouped, and groups of elements may be mapped simultaneously.

FIG. 7 illustrates a representative method for mapping an ultrasound transducer array in accordance with various embodiments of the invention. The method involves, in a first step 700, providing a phantom, and installing the transducer array and phantom in an MRI apparatus. Further, an imaging sequence defining the duration and relative times of ultrasound pulses, RF pulses, and encoding gradients is chosen (step 701). The phases of the transducer elements are then set to a constant value (step 702), and the focus location is determined by identifying the position of the phantom's maximal

displacement in the MR-ARFI image (step 703). An iterative phase-adjustment process is subsequently started by selecting one element (or one group of elements) for mapping (step 704). The selected element is driven at a variable phase (step 708), and for each phase setting, the transducer elements are collectively driven to generate an ultrasound focus in the phantom (710). Substantially simultaneously, or after a time interval overlapping with the generation of the ultrasound focus, the displacement of phantom material in the focus region is measured by MR-ARFI in accordance with the imaging sequence (step 712). Typically, this step is repeated until the variable phase of the selected transducer element has covered a range of phases spanning an interval of 2π . In step 714, the phase difference between the constant phase and the phase of the selected transducer element that maximizes the displacement is determined (step 712). If the phase difference is non-zero, the phase of the transducer element is adjusted by this difference (step 718). Steps 704 through 718 are then repeated until each transducer element has been mapped. If the phase adjustments made in step 718 fall below a predetermined threshold value, or an alternative termination condition is satisfied, the mapping is complete. Otherwise, the mapping procedure for the array may be repeated, starting with the adjusted phase settings of the transducer elements.

The method described above may be varied in several ways. For example, the phase differences may first be determined for all the elements, without adjustments being made, and following this mapping procedure, all the phase adjustments may be made at once. In this case, an iterative phase adjustment is not needed because the reference phase, i.e., the phase of the transducer as a whole, disregarding the element under mapping, is nearly the same for all elements. Further, in some embodiments, the phases of the transducer elements may be adjusted simultaneously, rather than in succession, by varying a drive parameter affecting some or all of the elements. For example, the relative phases between transducer elements may be expressed in terms of a functional dependence of the phase on the position of a transducer element along one or two axes of the transducer array, and such functional dependence, in turn, may be characterized by one or few mathematical parameters (e.g., a linear phase gradient and/or coefficients of higher-order components of the phase modulation in one- or two-dimensional space). Rather than modulating the phase of an individual element, then, the coefficients in the functional dependence may be varied, and the corresponding effect on the focus quality observed.

Alternatively or in addition to phase variations, amplitude variations of individual elements or groups of elements (including variations of the functional dependence of the amplitude on a position along the array) may also be employed to improve the focus quality. Further, in some embodiments, the transducer elements may be movable with respect to the one another within certain ranges (e.g., as a consequence of being mounted on electronically controllable microtranslator stages, pivots, etc.). The experimental adjustment procedure described above may then be used to fine-tune the positions and/or orientations of the transducer elements. The overall shape, position, and orientation of the transducer may likewise be controllable, e.g., via clasps, movable bearings, etc.

Although the present invention has been described with reference to specific details, it is not intended that such details should be regarded as limitations upon the scope of the invention, except as and to the extent that they are included in the accompanying claims.

What is claimed is:

1. A method for mapping an ultrasound transducer comprising a plurality of transducer elements so as to improve a focus thereof, the method comprising:

- (a) driving the plurality of transducer elements so as to generate an ultrasound focus;
- (b) using acoustic radiation force imaging, measuring a displacement associated with the focus;
- (c) grouping the transducer elements;
- (d) driving a selected group of transducer elements at a variable phase while driving the other groups of transducer elements at a same constant phase, thereby varying the displacement;
- (e) determining a phase difference, if any, between the same constant phase and the variable phase where the displacement is maximized; and
- (f) if the phase difference is non-zero, adjusting a relative phase of the selected group of transducer elements based thereon.

2. The method of claim 1 further comprising scanning a profile of the focus.

3. The method of claim 1 further comprising measuring a size of a cross-section of the focus.

4. The method of claim 1 further comprising measuring an integral intensity of the focus.

5. The method of claim 1 further comprising measuring a peak intensity of the focus.

6. The method of claim 1 wherein the acoustic radiation force imaging comprises applying a sequence of MR field gradients.

7. The method of claim 6 wherein the sequence of MR field gradients comprises repeated bipolar gradients.

8. The method of claim 7 wherein step (a) comprises generating an ultrasound pulse synchronized with the sequence of MR field gradients.

9. The method of claim 1 further comprising repeating steps (d) through (f) for the remaining groups of transducer elements.

10. The method of claim 1 further comprising the step of providing a phantom, the driving step generating an ultrasound focus in the phantom and the measuring step measuring a focus quality in the phantom.

11. The method of claim 10 wherein the phantom comprises a material having low tensile strength.

12. The method of claim 11 wherein the phantom comprises a material having a small elastic modulus.

13. A system for mapping an ultrasound transducer so as to improve a focus thereof, the system comprising:

ultrasound transducer hardware for generating an ultrasound focus, the ultrasound transducer hardware comprising an ultrasound transducer having a plurality of transducer elements and associated driver circuitry, the transducer elements being organized in multiple groups of elements;

magnetic-resonance-imaging (MRI) hardware comprising an MRI apparatus and associated driver components for acquiring images of a region comprising the ultrasound focus; a control station in communication with the ultra-

sound transducer hardware and the MRI hardware, the control station being configured to control (i) image acquisition with the MRI hardware and (ii) generation of the ultrasound focus with the ultrasound transducer hardware in accordance with an imaging sequence that specifies the relative timing between image acquisition and ultrasound generation; process acquired images to determine therefrom a displacement associated with the focus; send control signals to the ultrasound transducer hardware to vary a phase of a selected group of transducer elements while driving the other groups of transducer elements at a same constant phase; and adjust the phase of the selected group of transducer elements relative to the same constant phase of the other groups based on a phase difference between the same constant phase and the variable phase where the displacement is maximized.

14. The system of claim 13, wherein the driver circuitry is hardwired to create the groups of transducer elements.

15. The system of claim 13, wherein the driver circuitry comprises switches for configuring the groups of transducer elements.

16. The system of claim 13, wherein the control station comprises separate, intercommunicating computers for controlling the ultrasound transducer hardware and the MRI hardware, respectively.

17. The system of claim 13, wherein the imaging sequence specifies a sequence of MR field gradient synchronized with ultrasound generation.

18. The system of claim 13, wherein controlling image acquisition and ultrasound-focus generation in accordance with an imaging sequence comprises sending trigger signals to the ultrasound transducer hardware and the MRI hardware.

19. The system of claim 13, wherein controlling image acquisition and ultrasound-focus generation in accordance with an imaging sequence comprises communicating a time-delay parameter to the MRI hardware, the MRI hardware being configured to send a trigger signal based on the time-delay parameter to the ultrasound transducer hardware.

20. A method for controlling an ultrasound transducer comprising a plurality of transducer elements organized into groups of elements, the method comprising:

- (a) mapping the ultrasound transducer by (i) driving the plurality of transducer elements so as to generate an ultrasound focus in a phantom, (ii) varying a focus-affecting parameter associated with at least one of the groups of elements while driving the other groups of transducer elements at a same constant value of the focus-affecting parameter and measuring a resulting variation on a quality of the ultrasound focus using magnetic-resonance acoustic radiation force imaging, and (iii) selecting a value of the focus-affecting parameter associated with a best focus quality; and

(b) controlling the ultrasound transducer based on the mapping step so as to focus ultrasound into internal body tissue.

* * * * *

专利名称(译)	映射超声换能器		
公开(公告)号	US9412357	公开(公告)日	2016-08-09
申请号	US14/138864	申请日	2013-12-23
[标]申请(专利权)人(译)	约阿夫棉兰 赫茨伯格约尼 MAOR DOV		
申请(专利权)人(译)	棉兰, 约阿夫 赫茨伯格, 约尼 MAOR, DOV		
当前申请(专利权)人(译)	InSightec的有限公司.		
[标]发明人	MEDAN YOAV HERTZBERG YONI MAOR DOV		
发明人	MEDAN, YOAV HERTZBERG, YONI MAOR, DOV		
IPC分类号	G10K11/34 A61B8/00 G01N29/30 A61N7/00 G01H17/00		
CPC分类号	G10K11/346 A61B8/587 A61N2007/0078 A61N2007/0095 G01H17/00 G01N29/30		
优先权	61/251450 2009-10-14 US		
其他公开文献	US20140112095A1		
外部链接	Espacenet USPTO		

摘要(译)

可以通过改变影响焦点的参数并调整参数来映射超声换能器，以便改善聚焦质量。在一些实施例中，映射涉及相对于其他换能器元件的恒定相位连续地改变一个换能器元件或元件组的相位，并确定超声波焦点中的组织位移最大化的相位。

