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(54) **ACOUSTIC RESPIRATORY MONITORING
SENSOR HAVING MULTIPLE SENSING
ELEMENTS**

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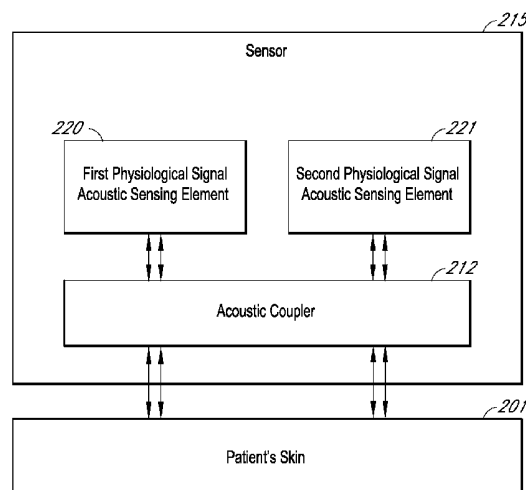
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(57) **ABSTRACT**

According to certain described aspects, multiple acoustic sensing elements are employed in a variety of beneficial ways to provide improved physiological monitoring, among other advantages. In various embodiments, sensing elements can be advantageously employed in a single sensor package, in multiple sensor packages, and at a variety of other strategic locations in the monitoring environment. According to other aspects, to compensate for skin elasticity and attachment variability, an acoustic sensor support is provided that includes one or more pressure equalization pathways. The pathways can provide an air-flow channel from the cavity defined by the sensing elements and frame to the ambient air pressure.

21 Claims, 35 Drawing Sheets



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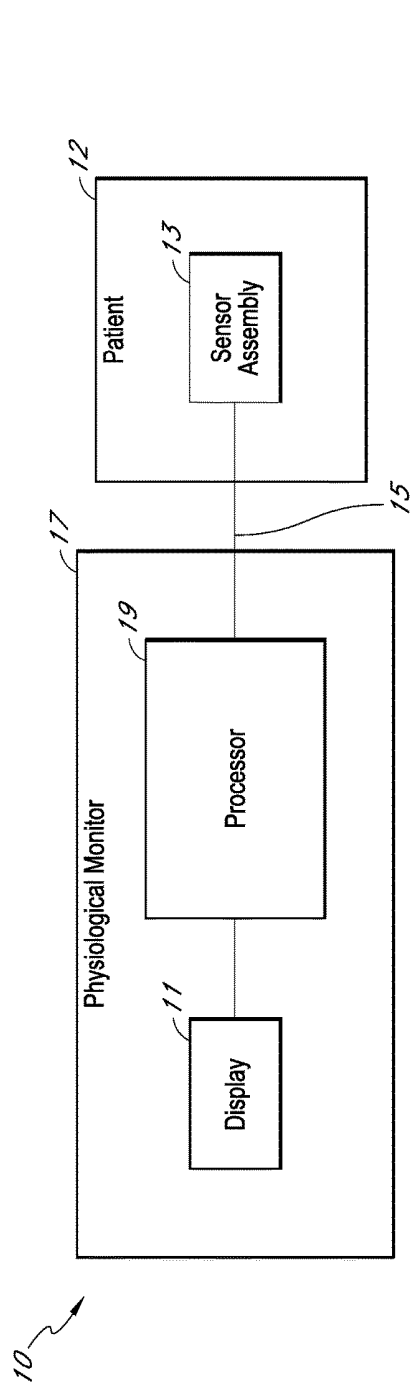


FIG. 1A

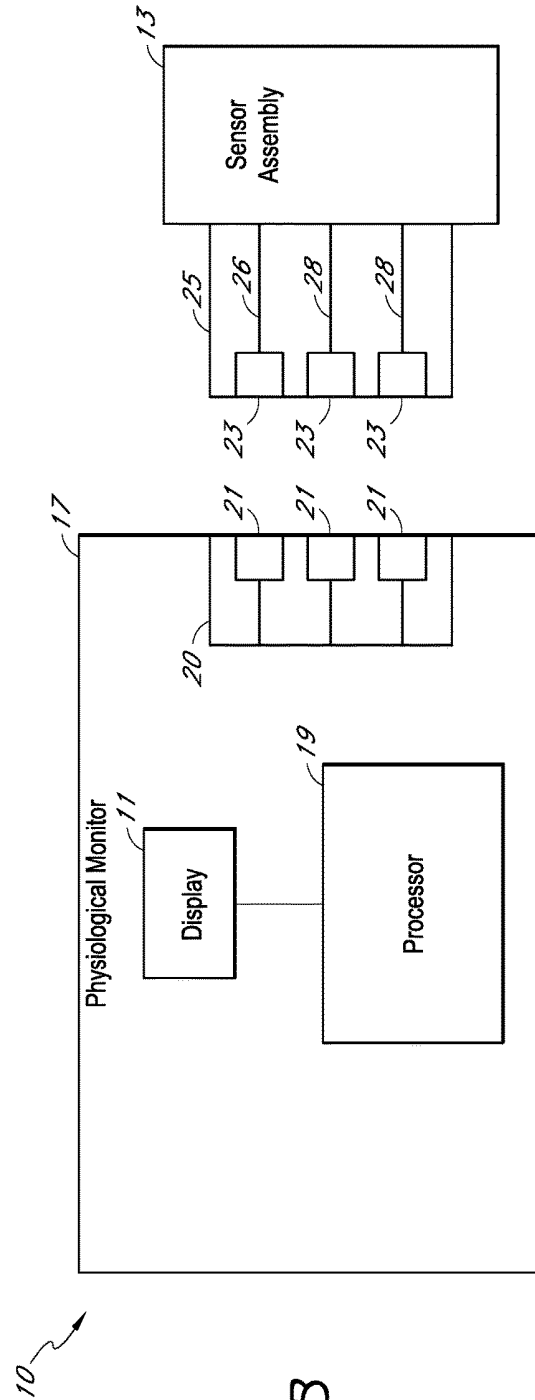


FIG. 1B

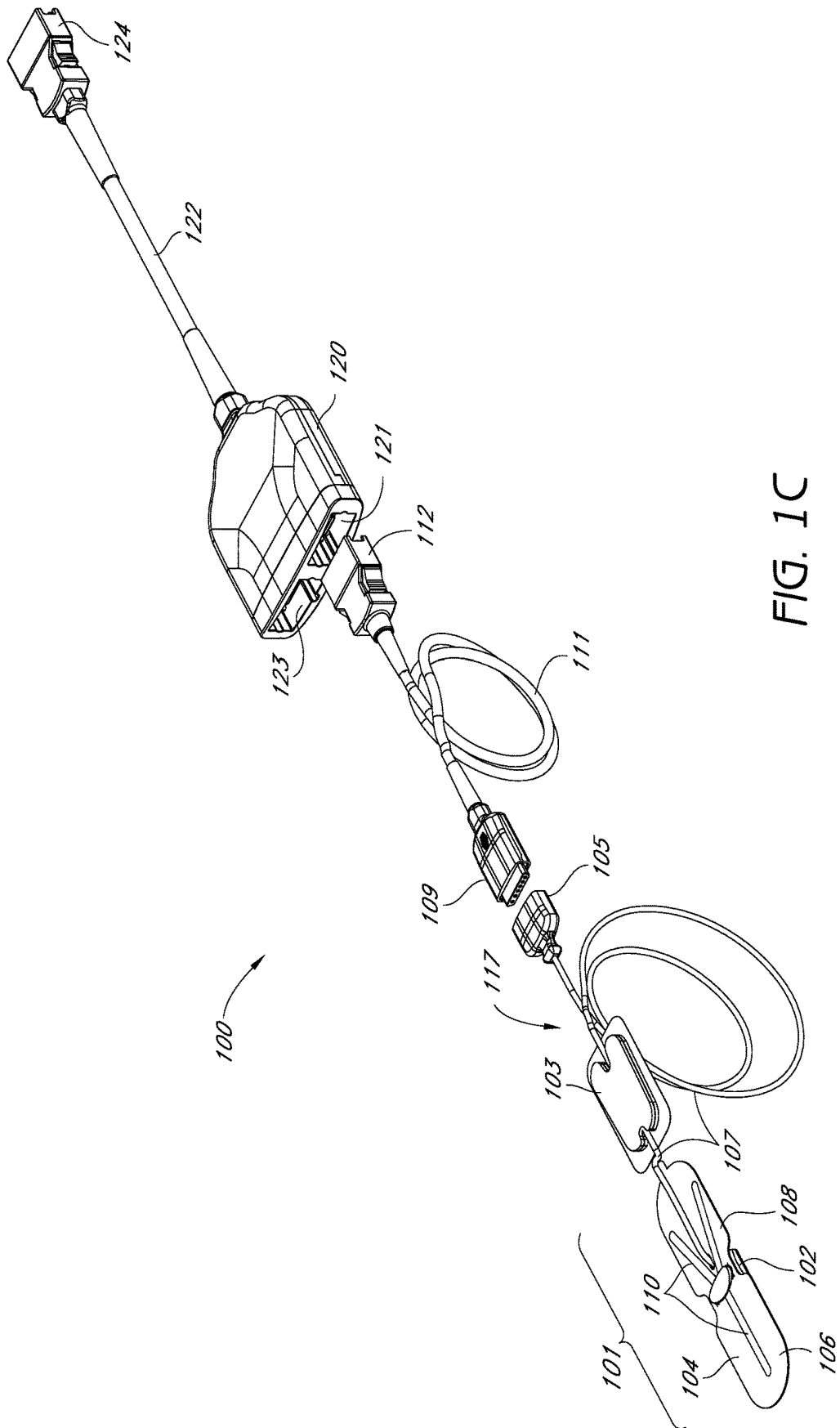


FIG. 1C

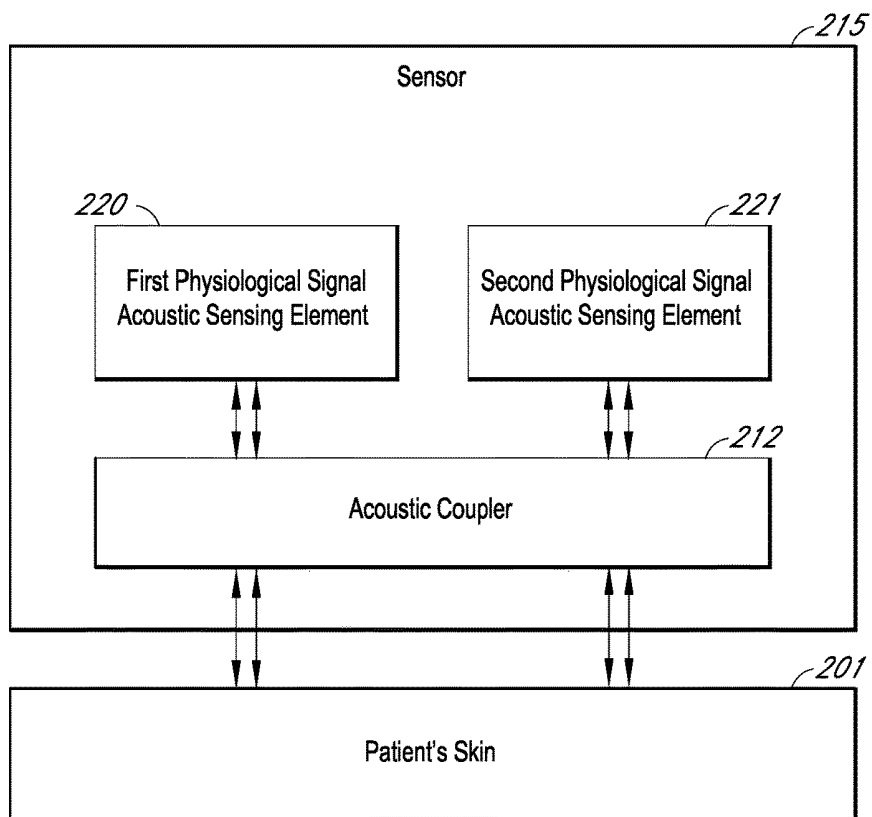


FIG. 2A

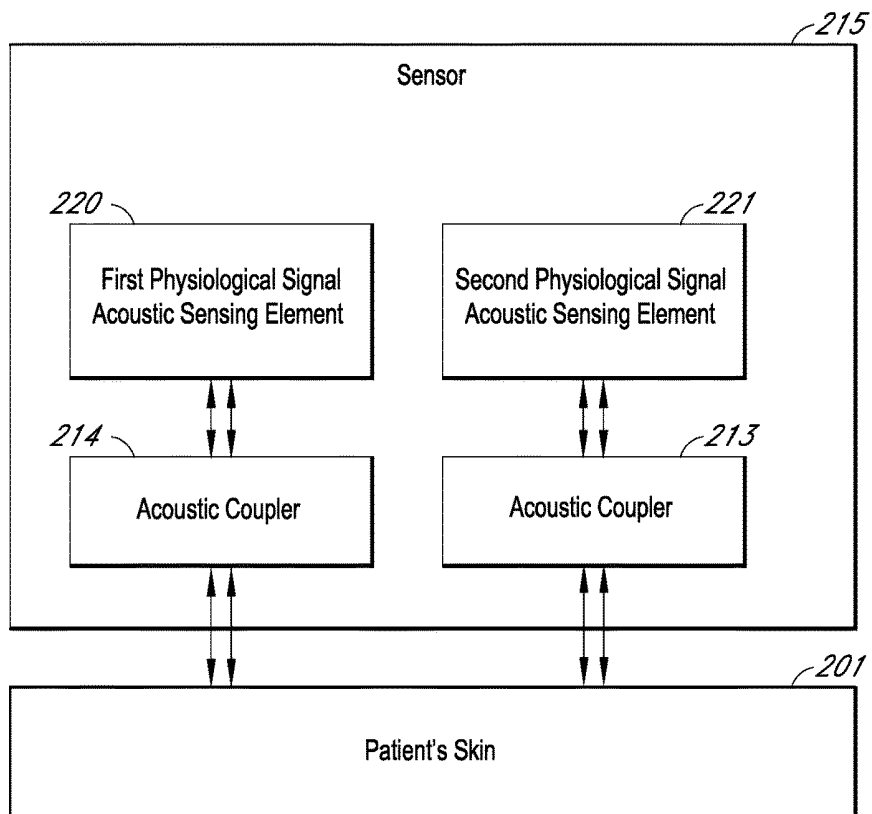


FIG. 2B

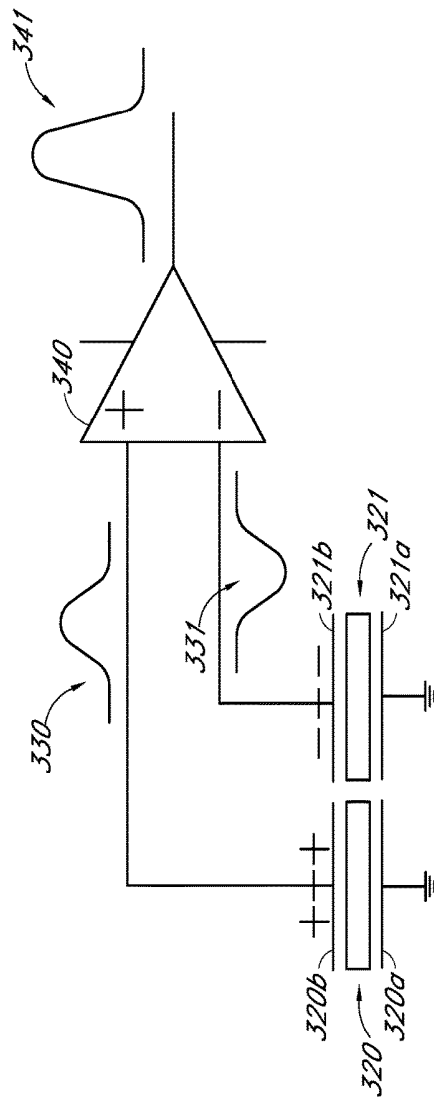


FIG. 3A

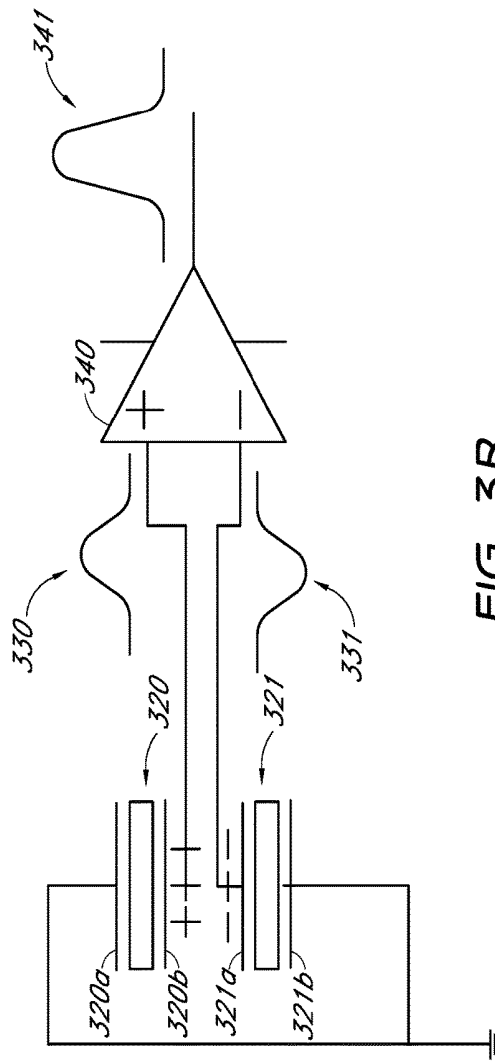
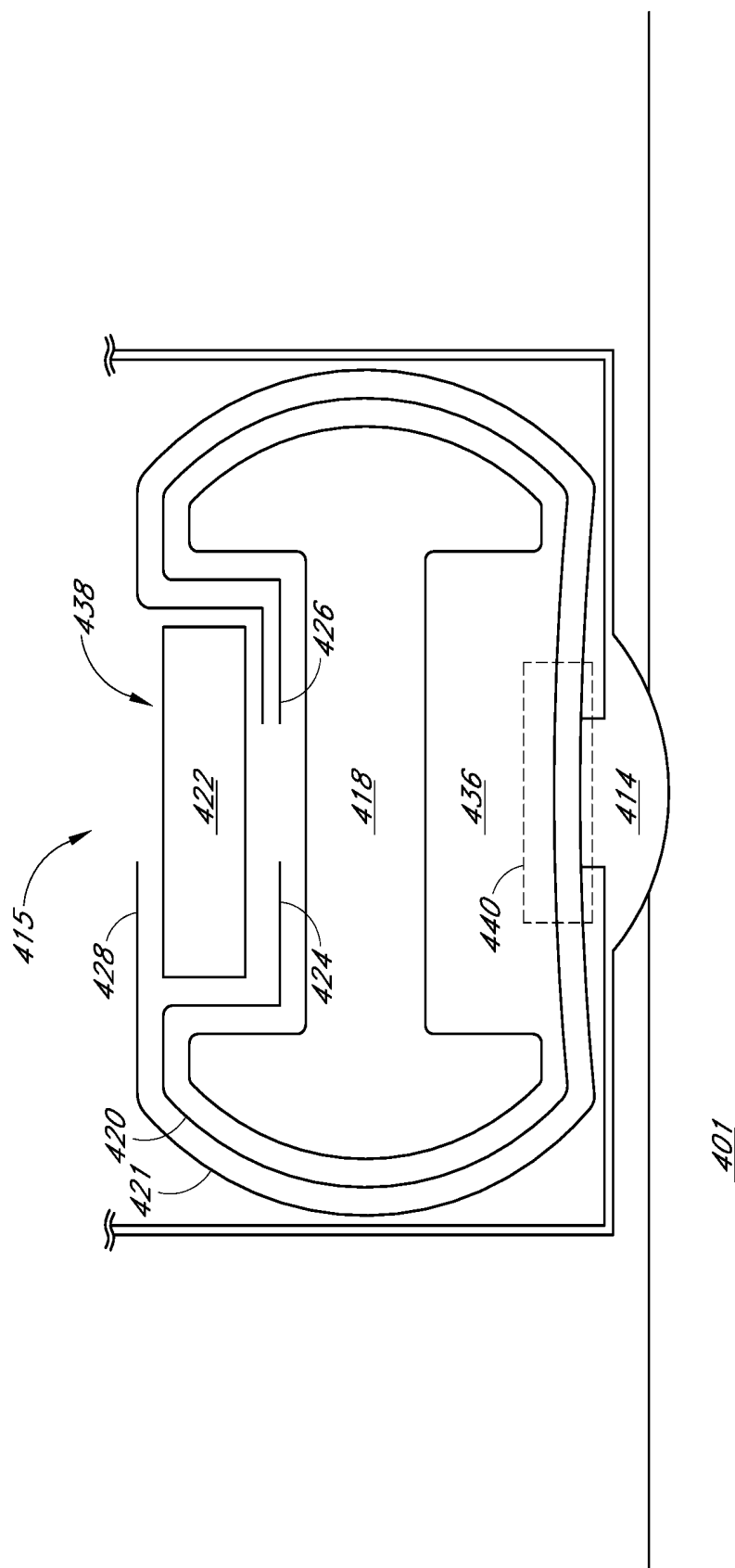


FIG. 3B



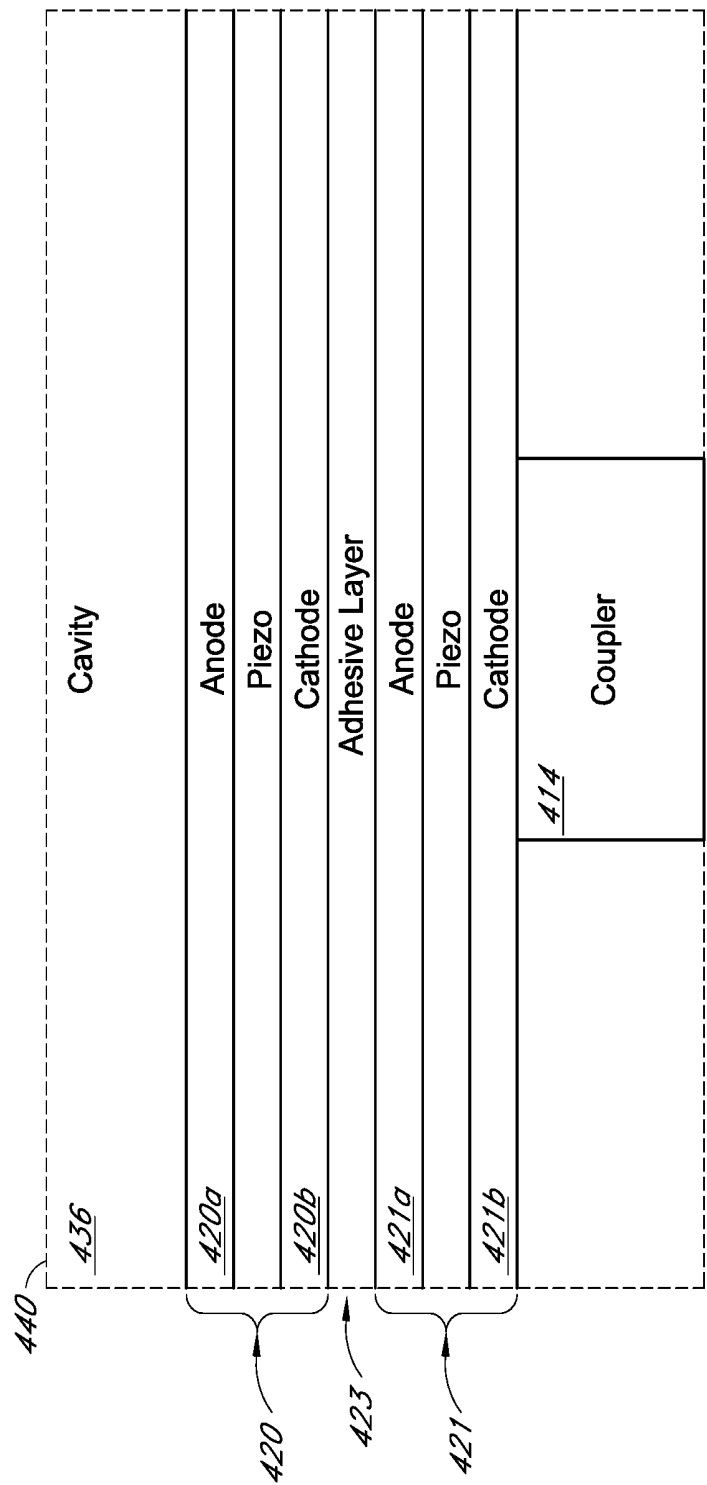


FIG. 4B

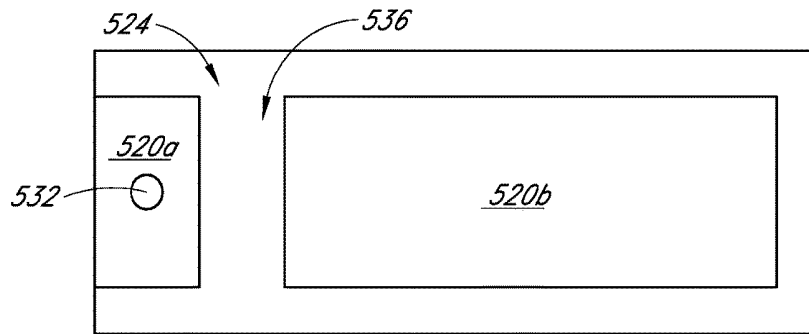


FIG. 5A

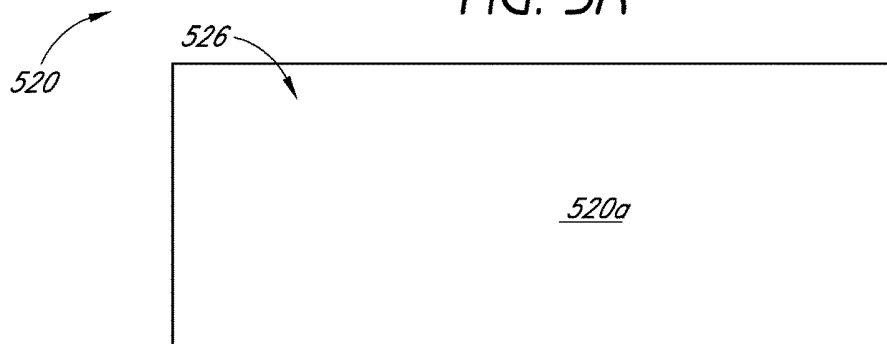


FIG. 5B

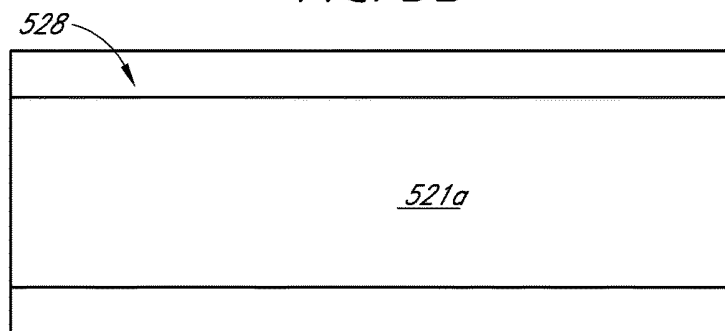


FIG. 5C

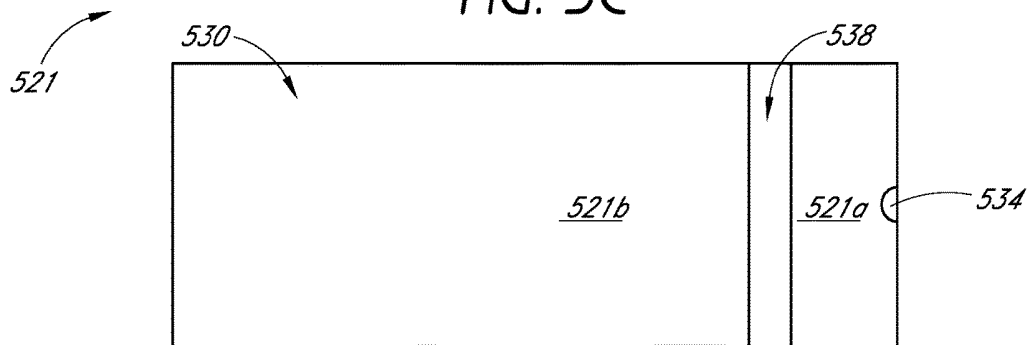
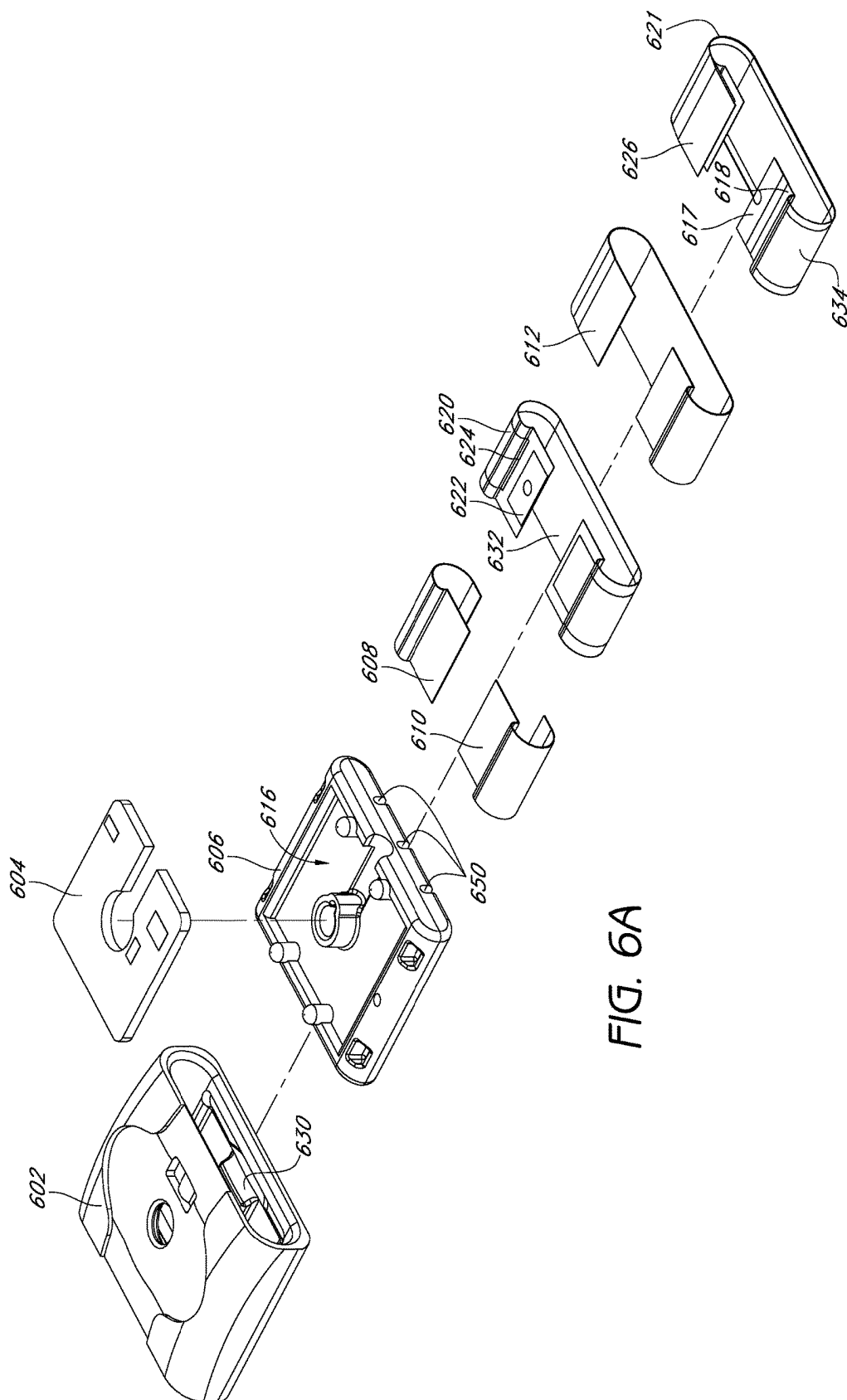
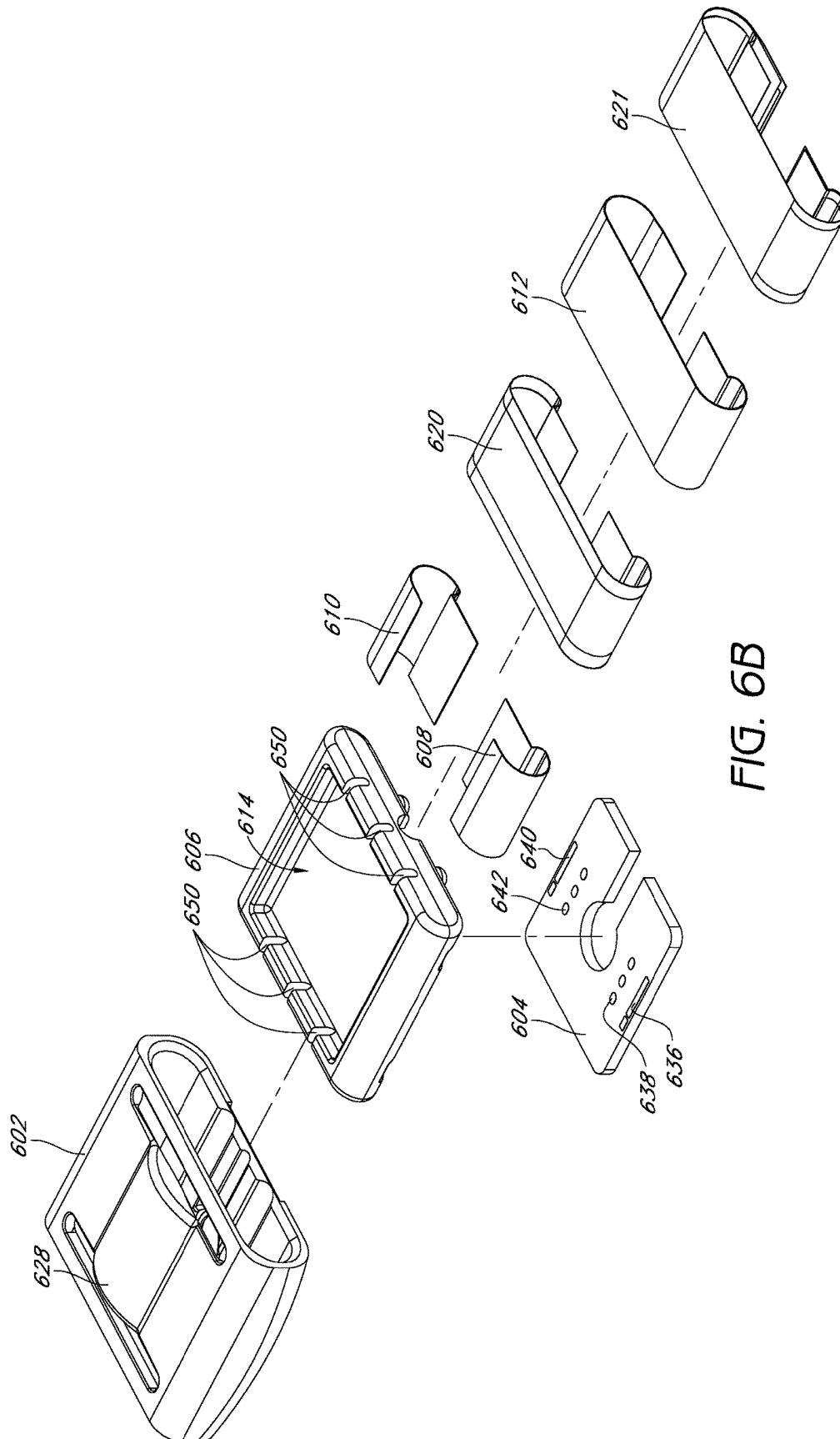


FIG. 5D





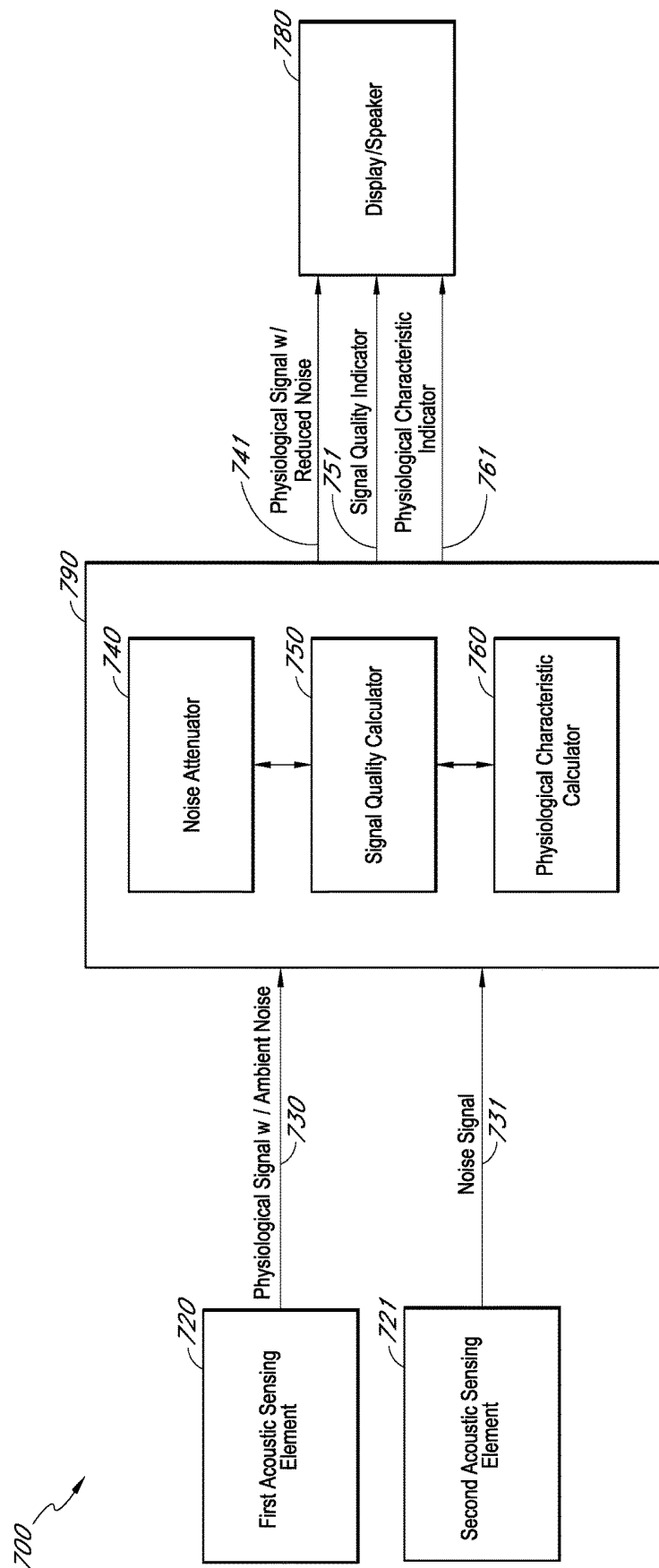


FIG. 7

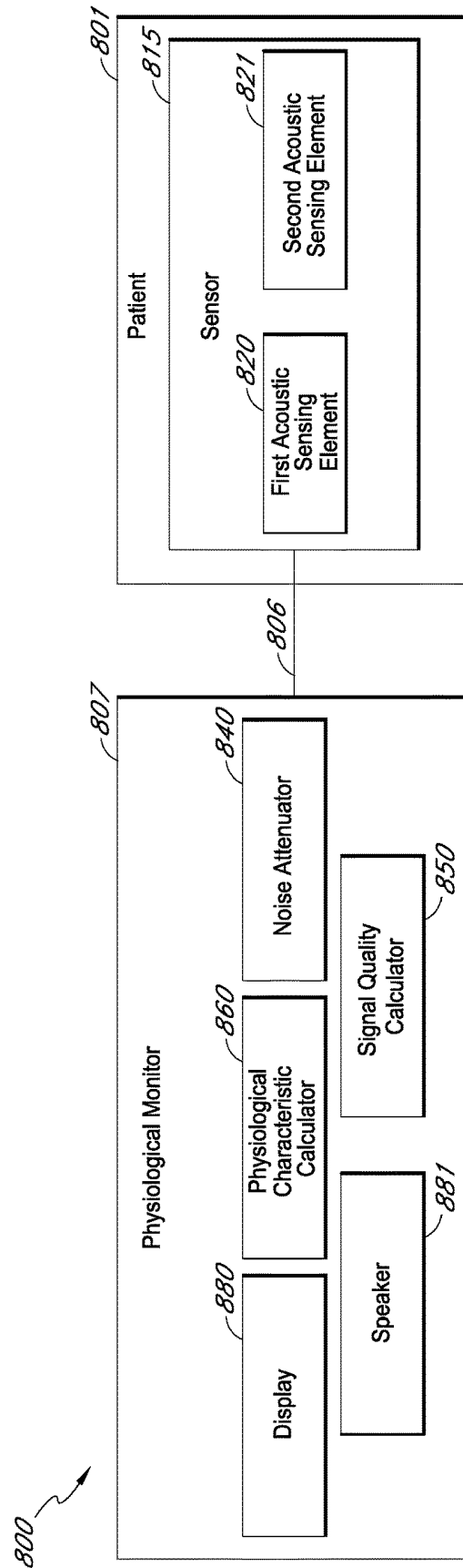
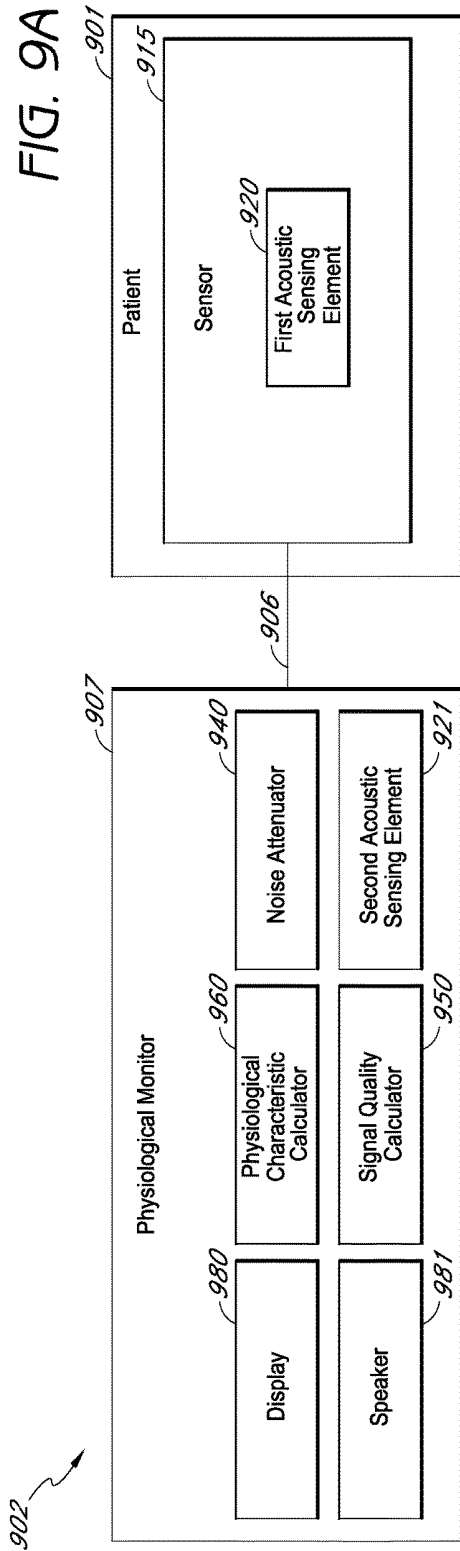
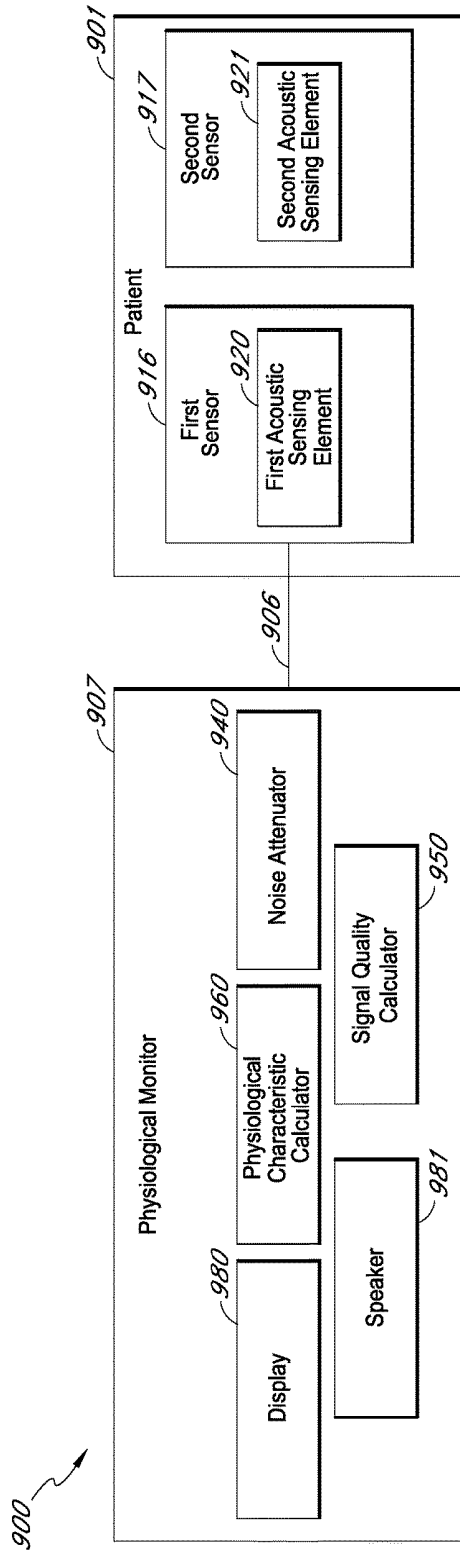


FIG. 8



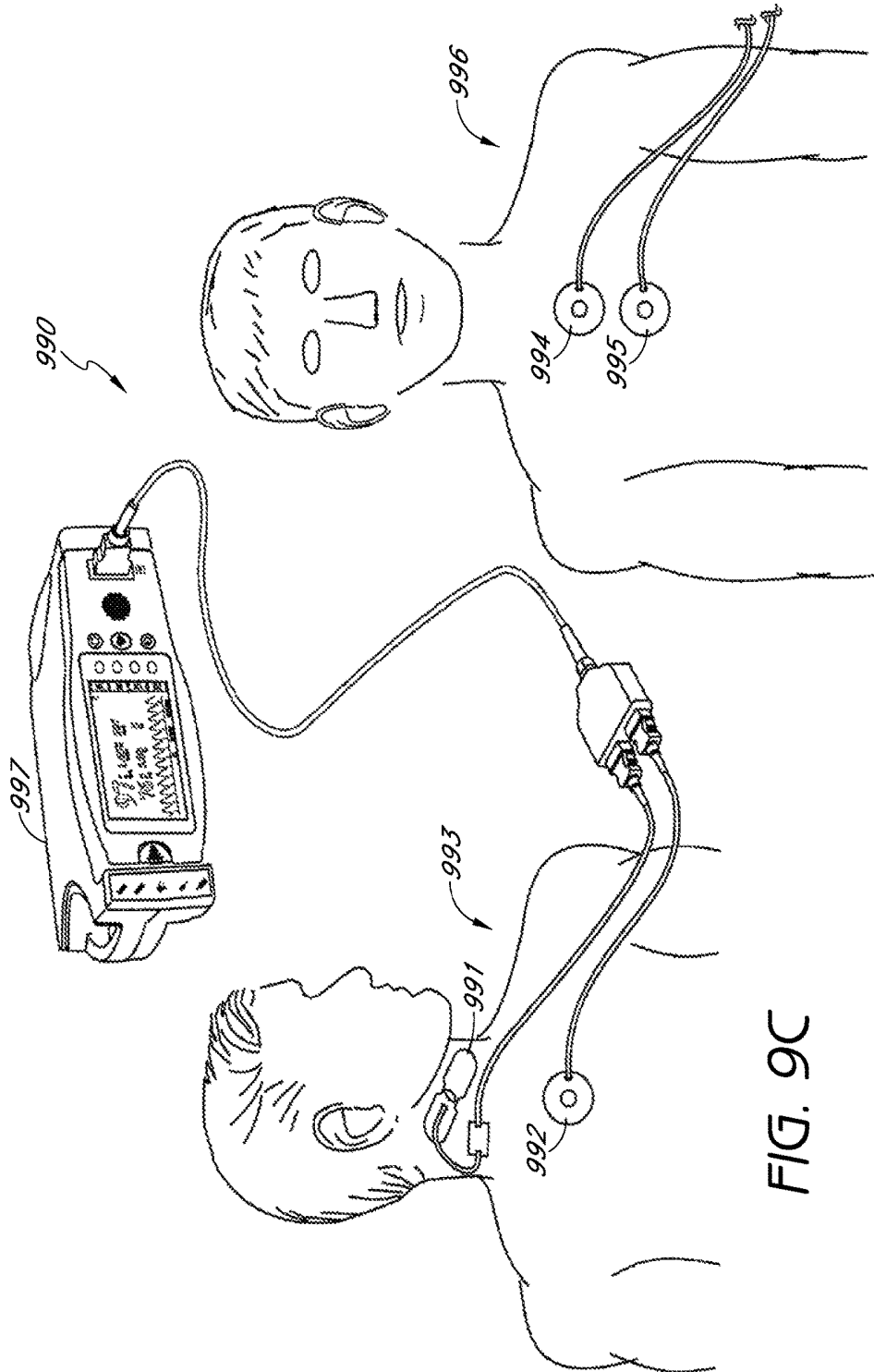


FIG. 9C

FIG. 9D

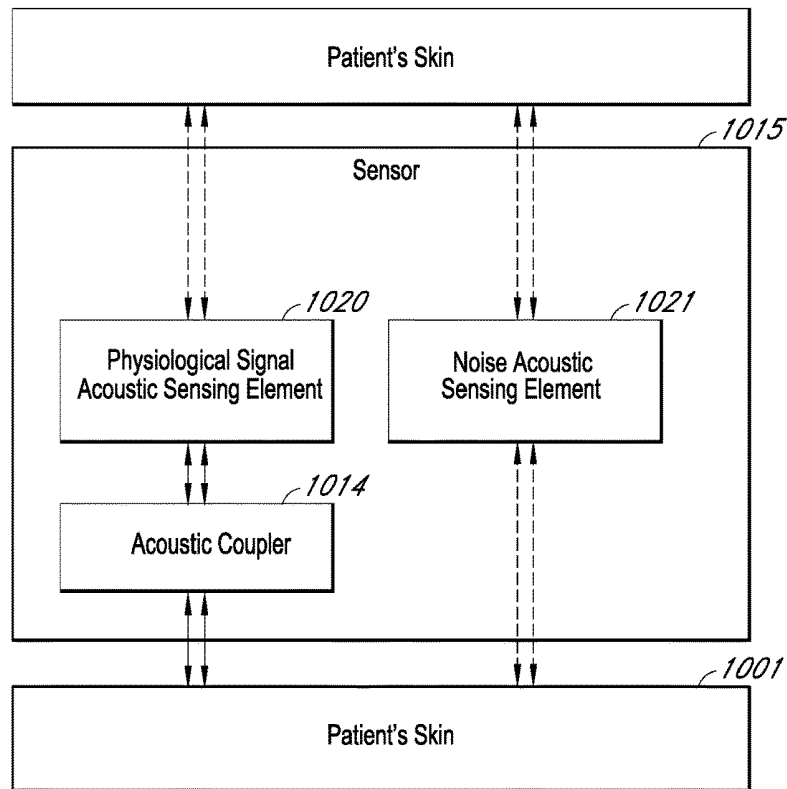


FIG. 10

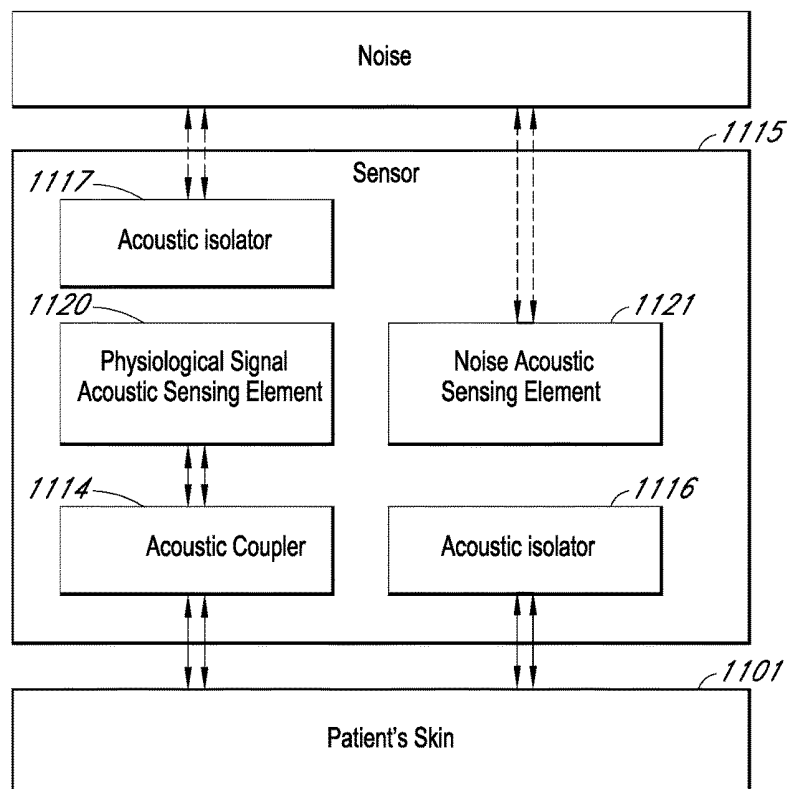


FIG. 11

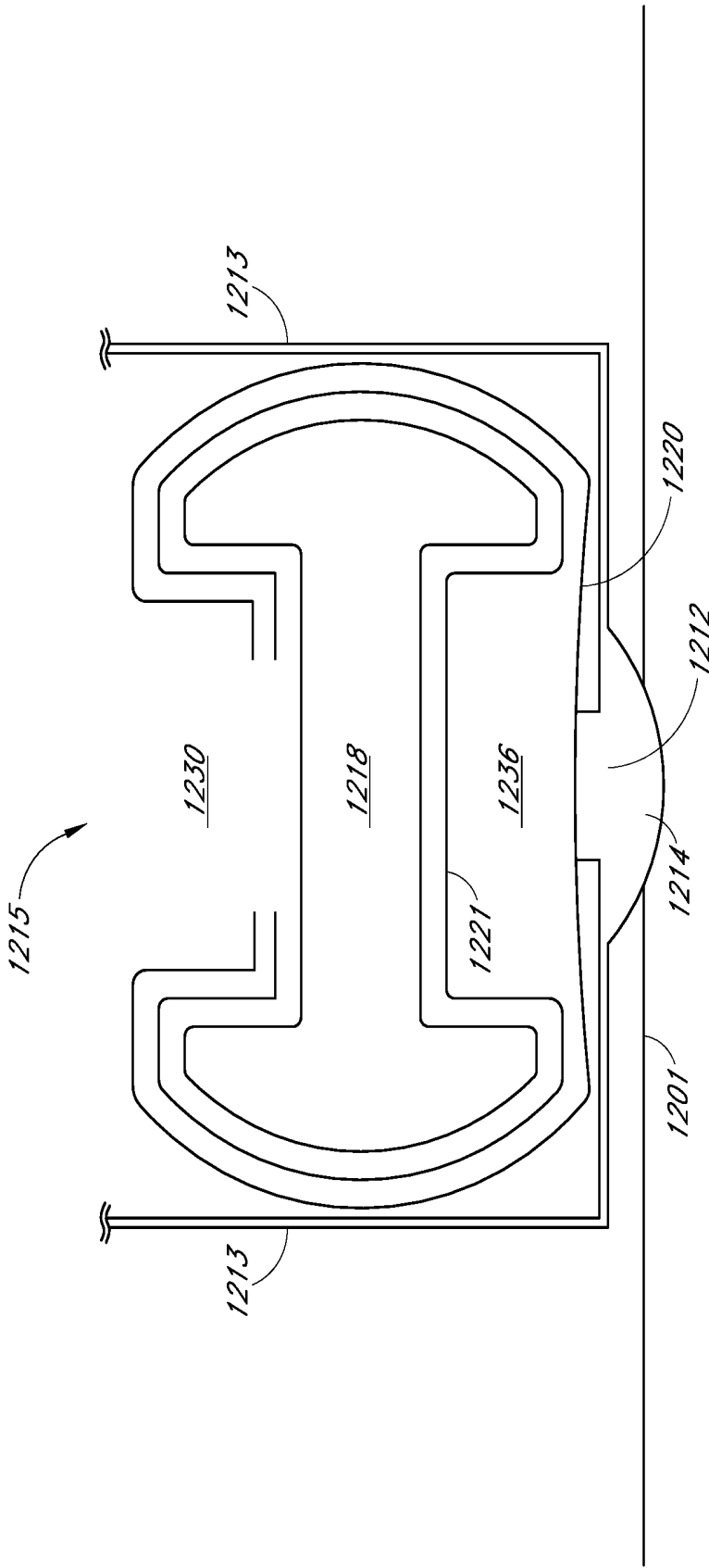


FIG. 12

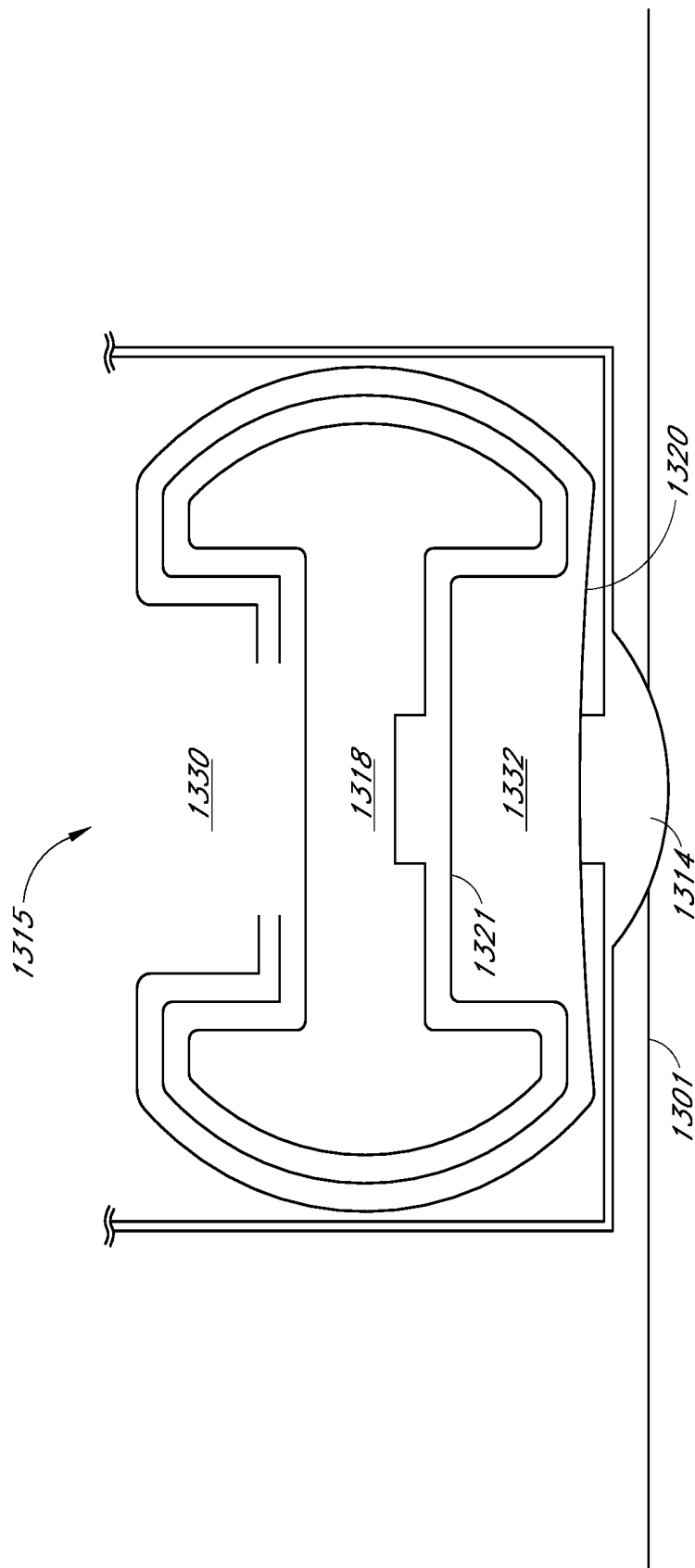


FIG. 13

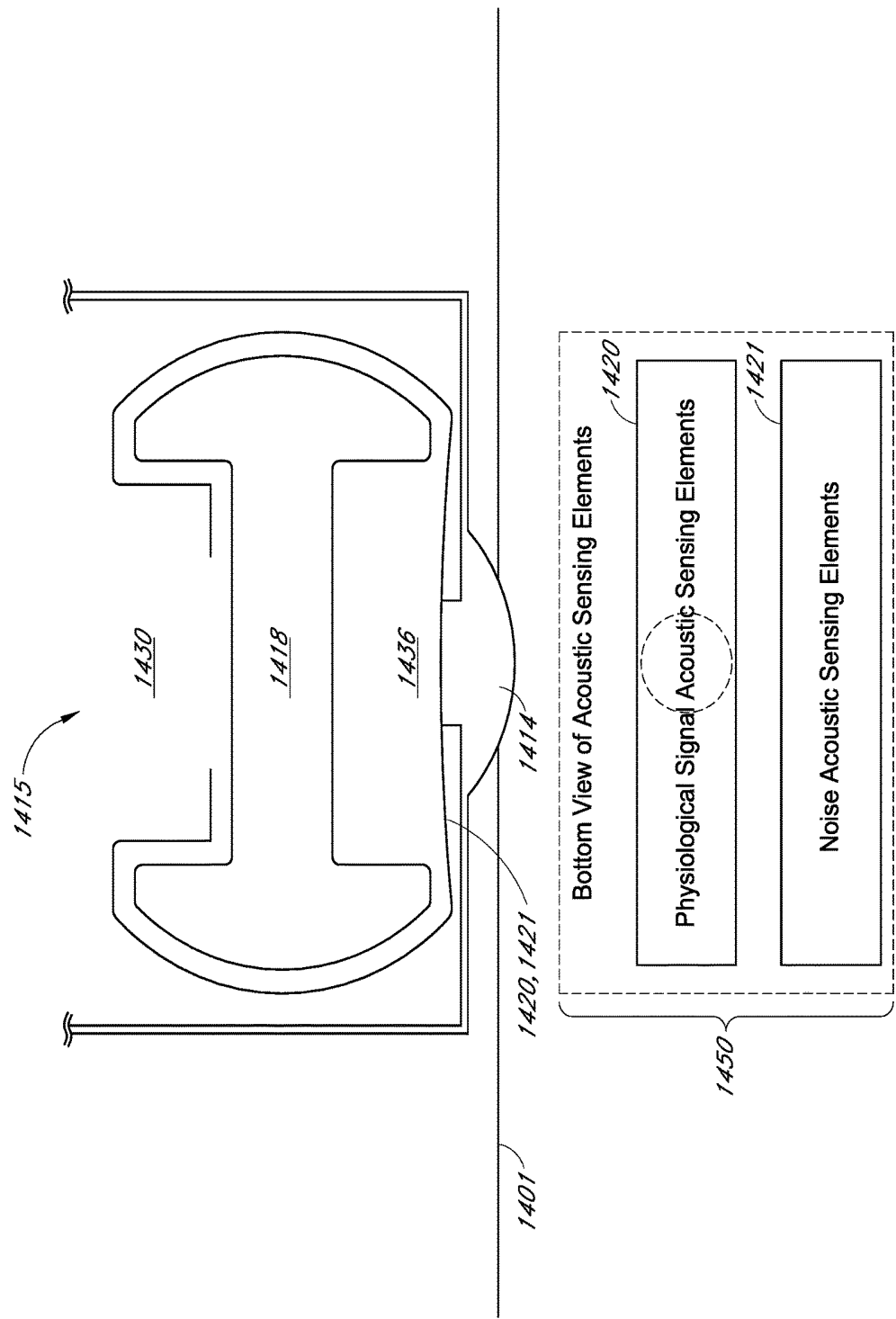


FIG. 14

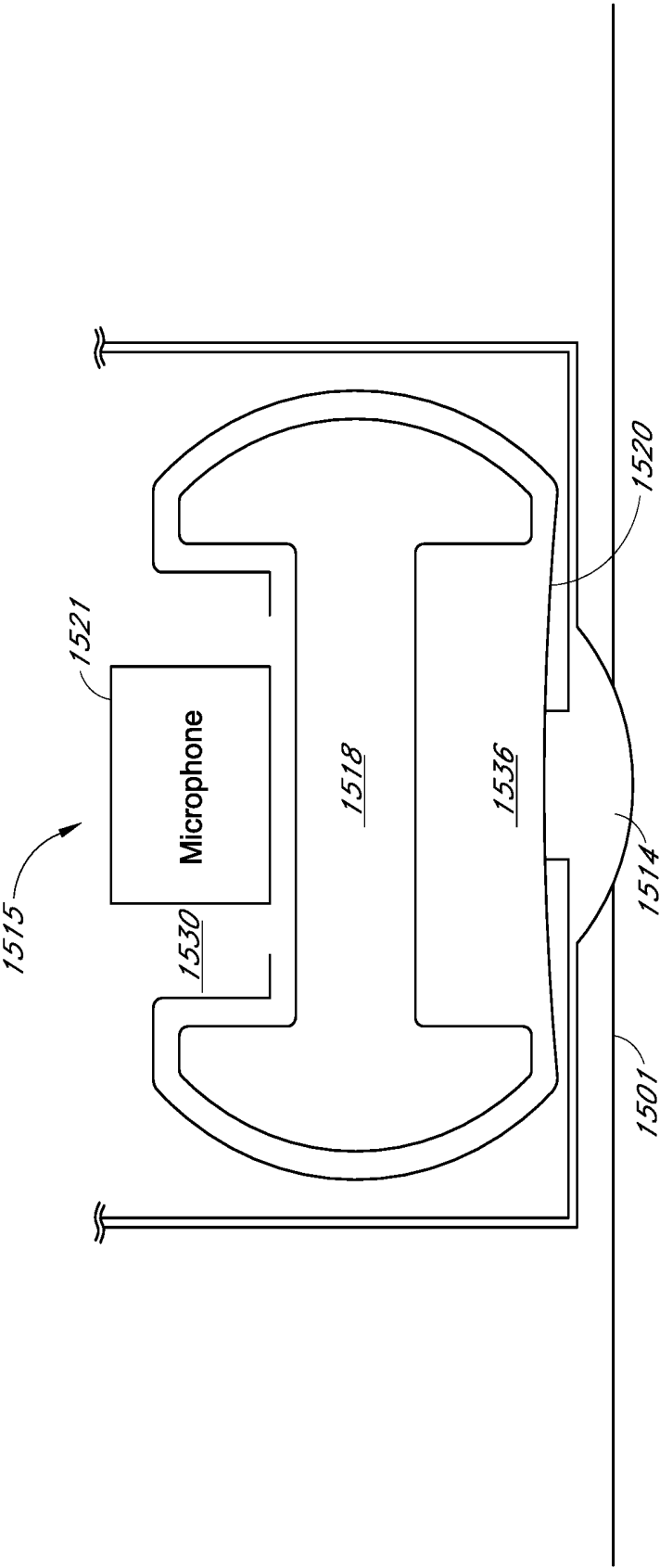


FIG. 15

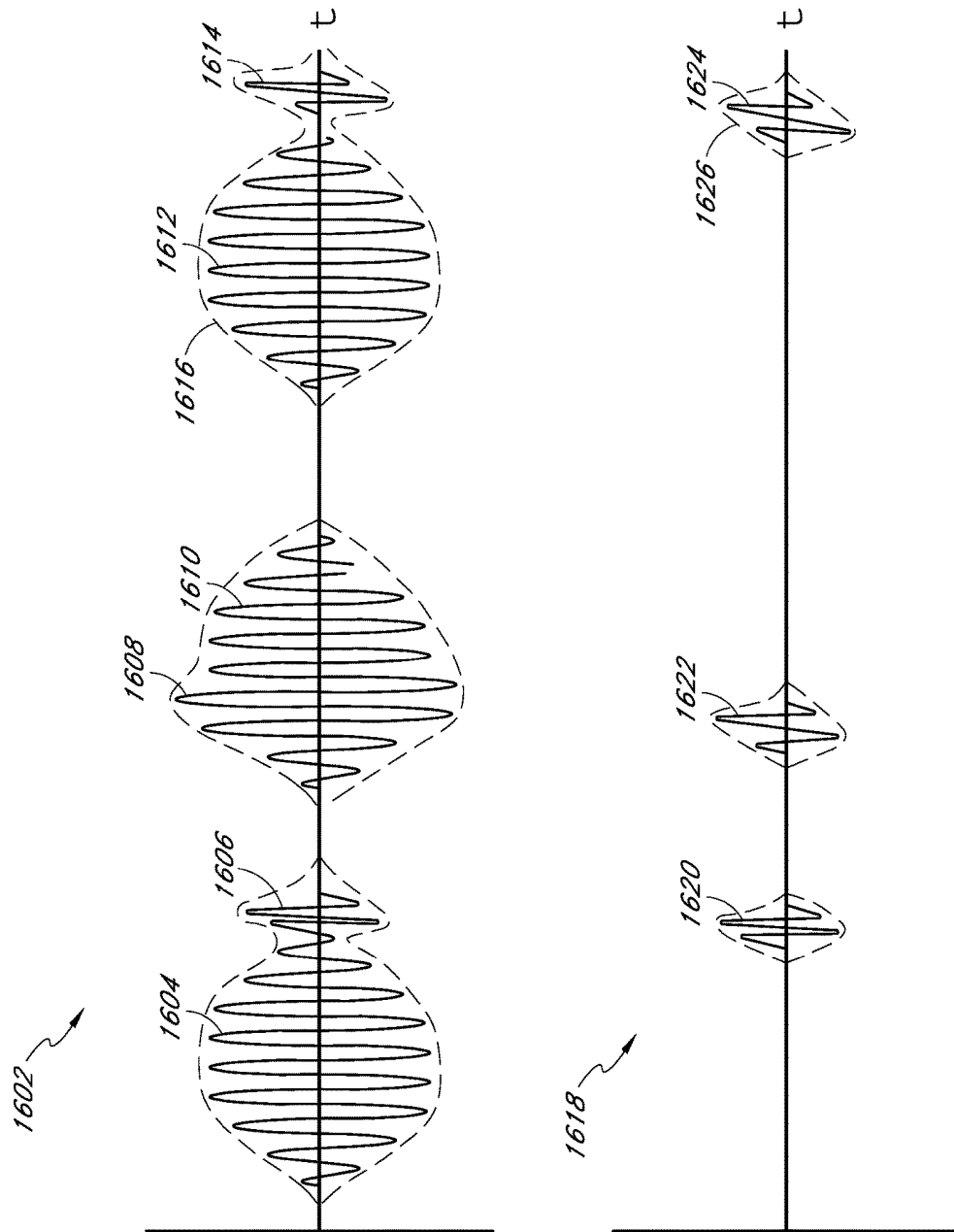


FIG. 16

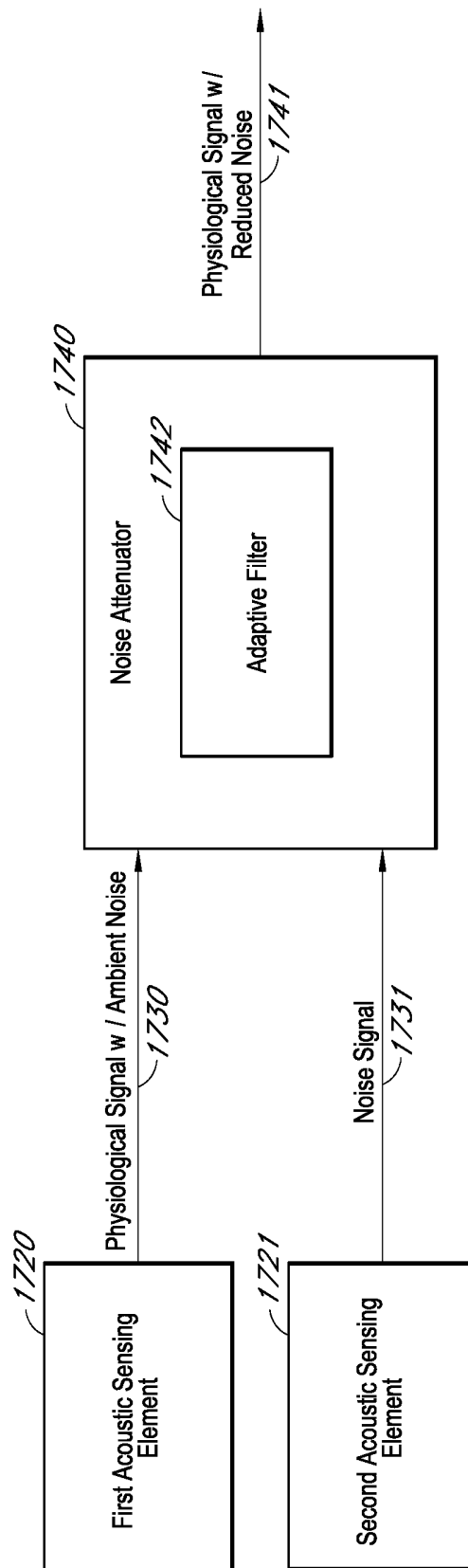


FIG. 17

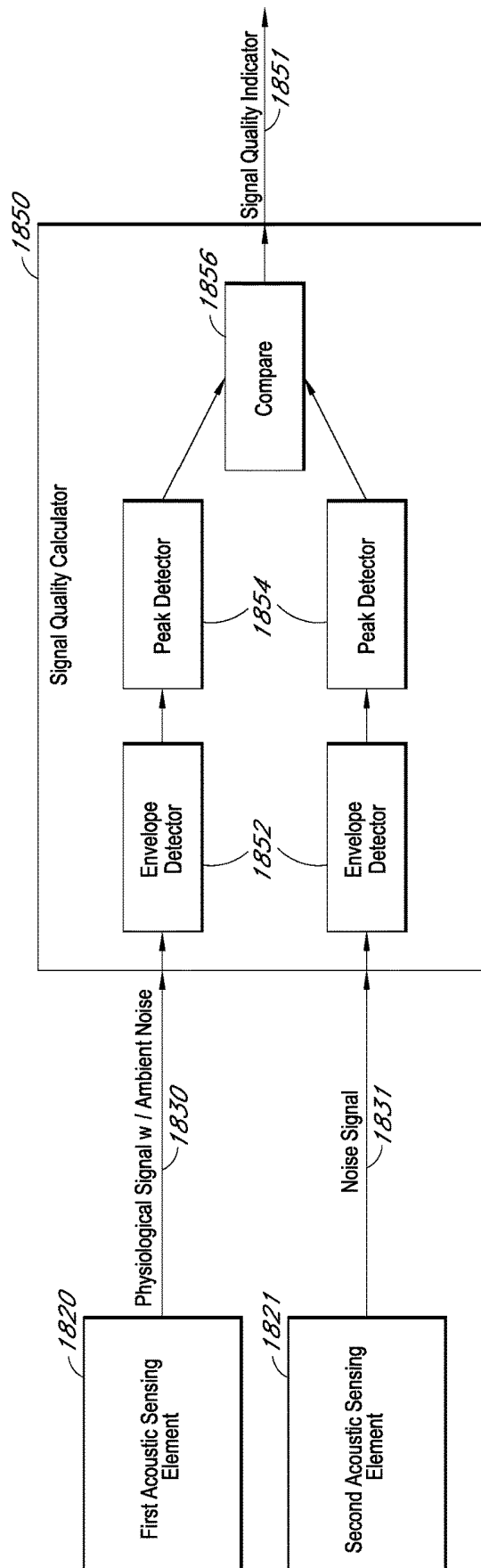
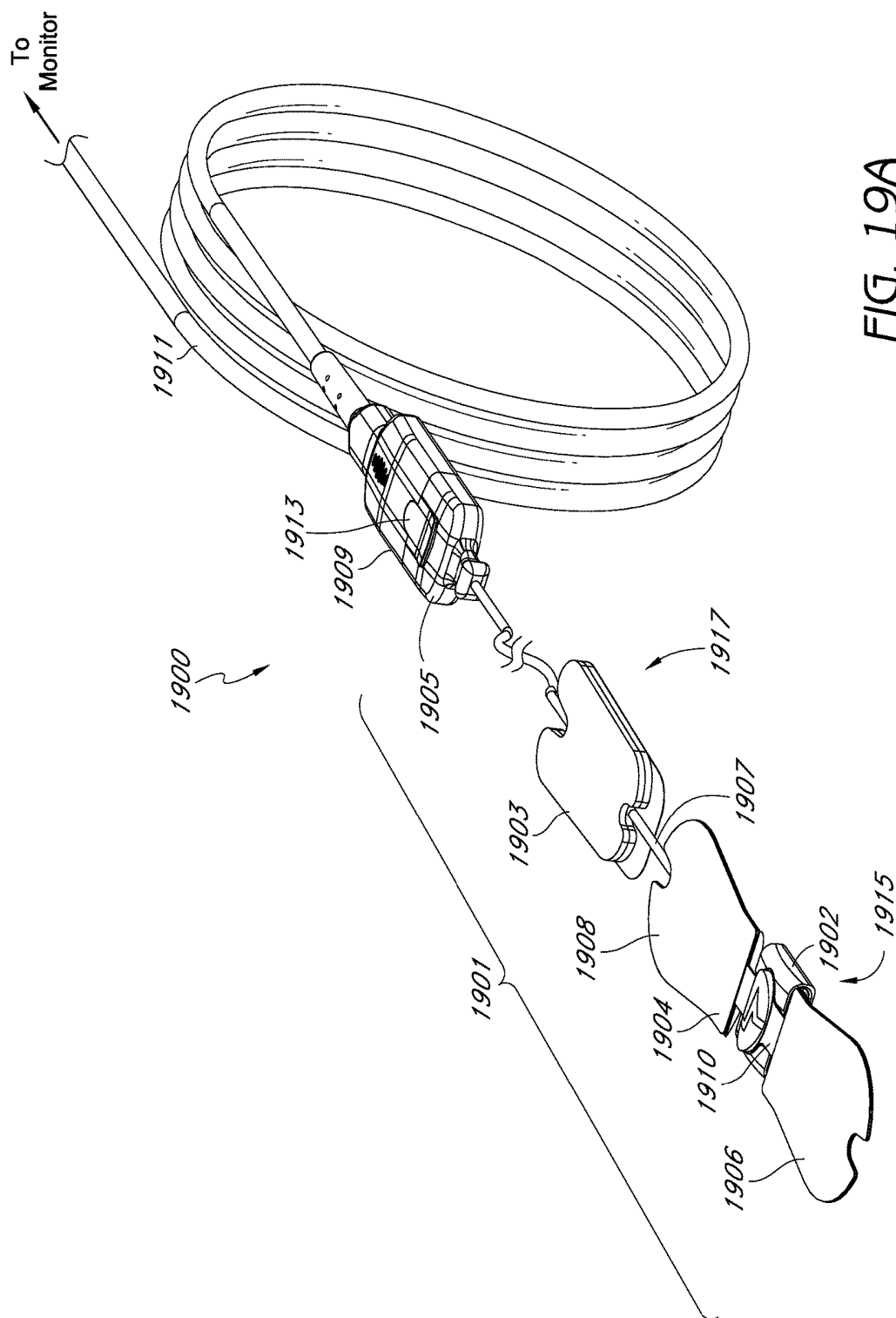


FIG. 18



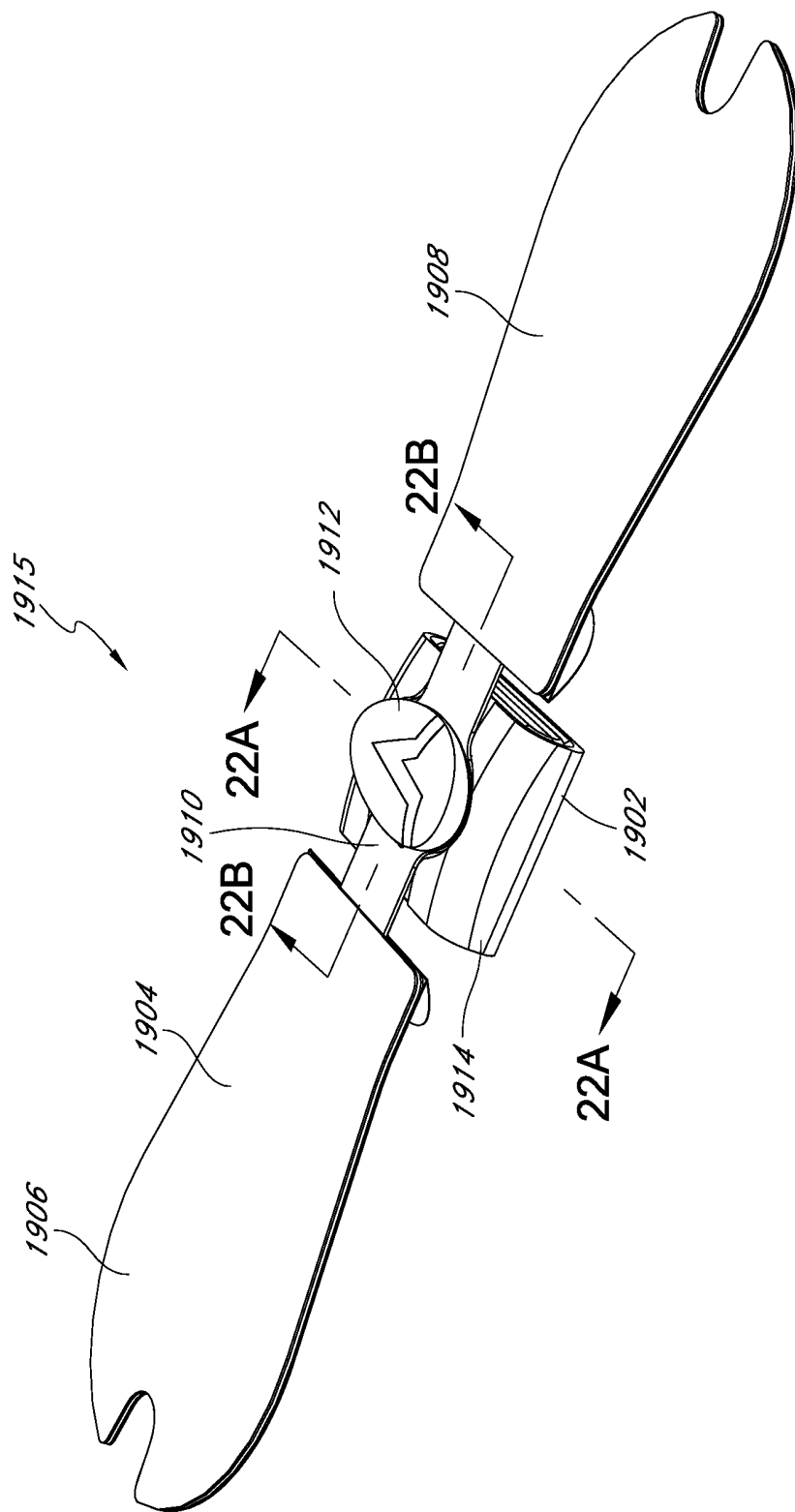


FIG. 19B

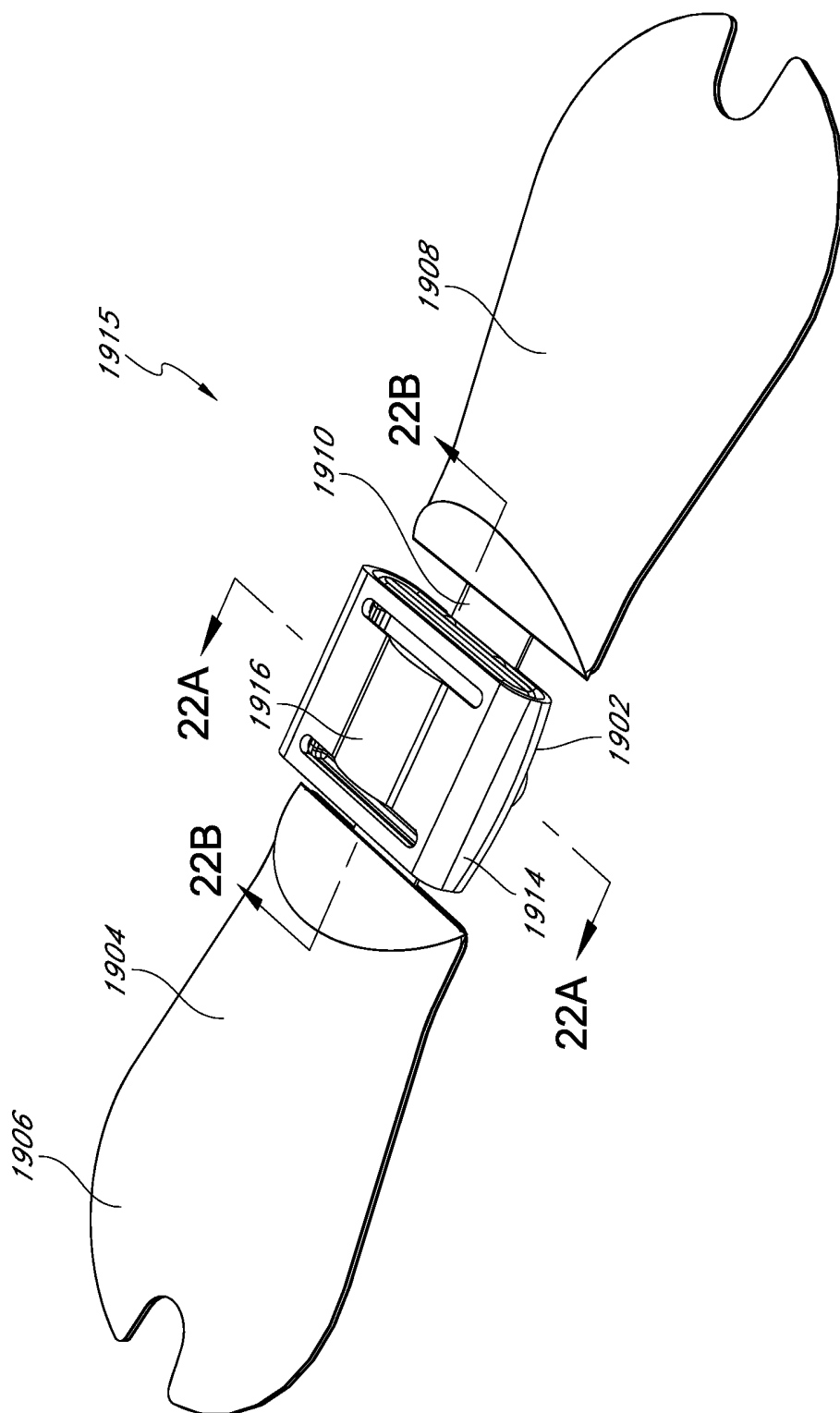
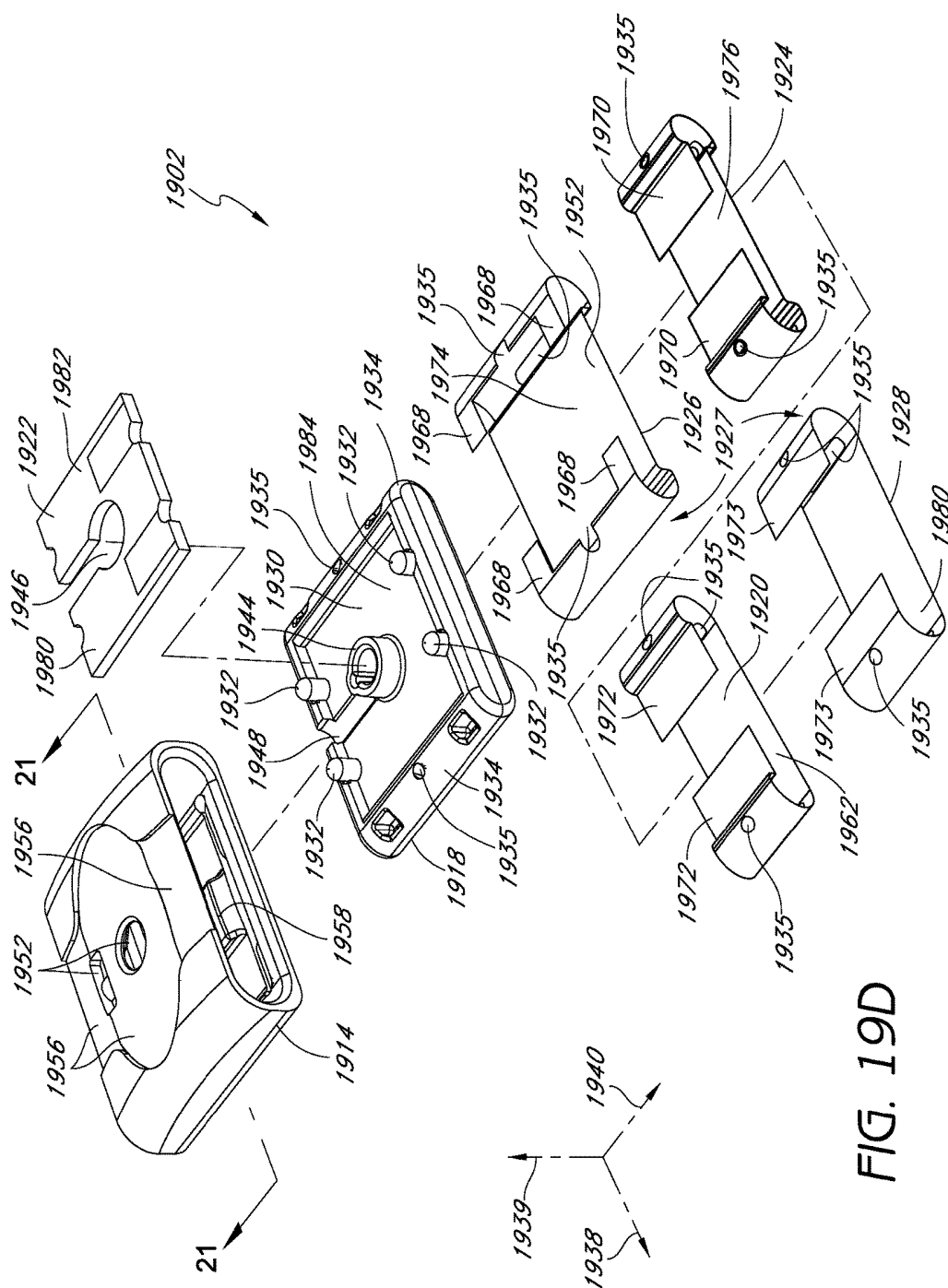


FIG. 19C



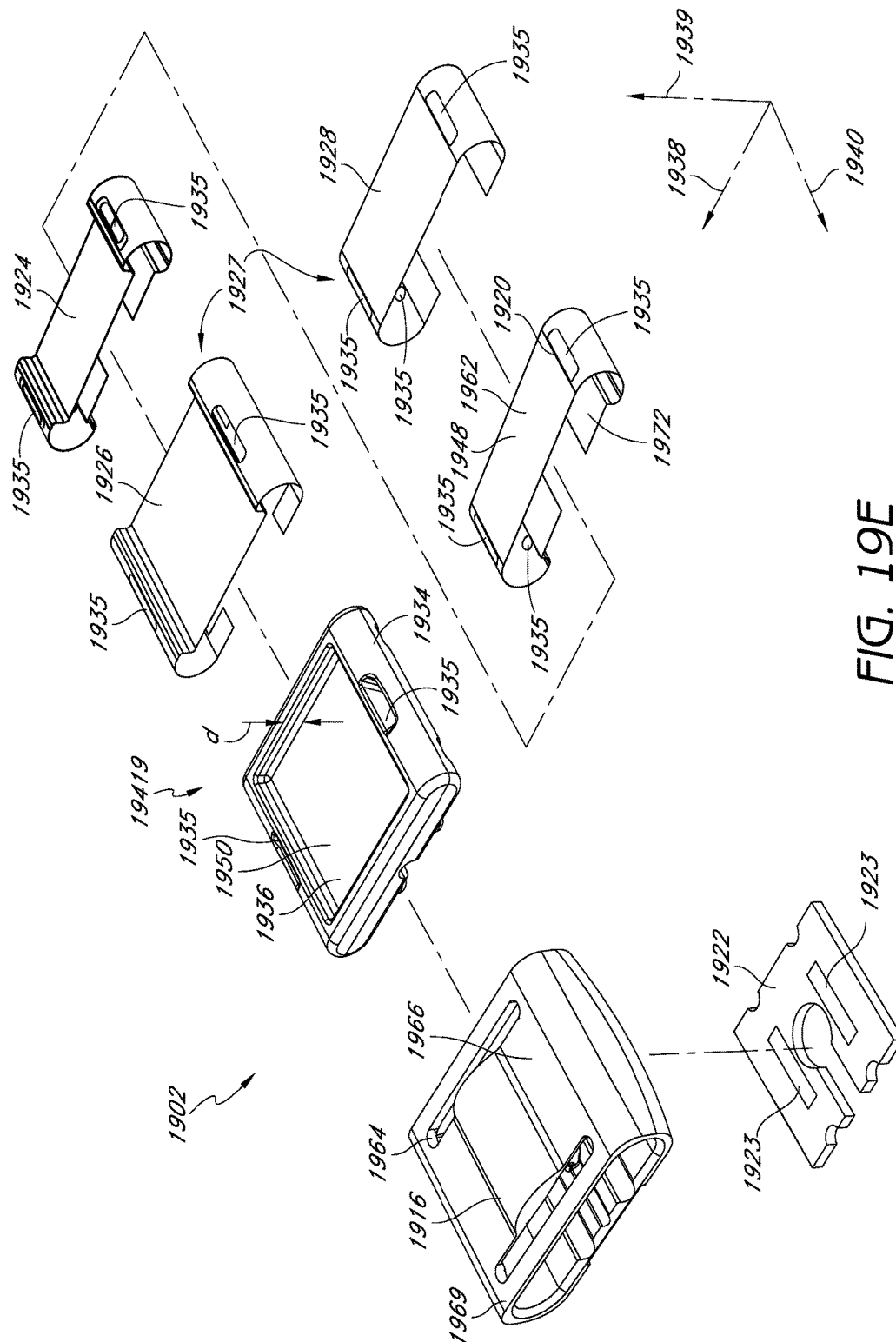


FIG. 19E

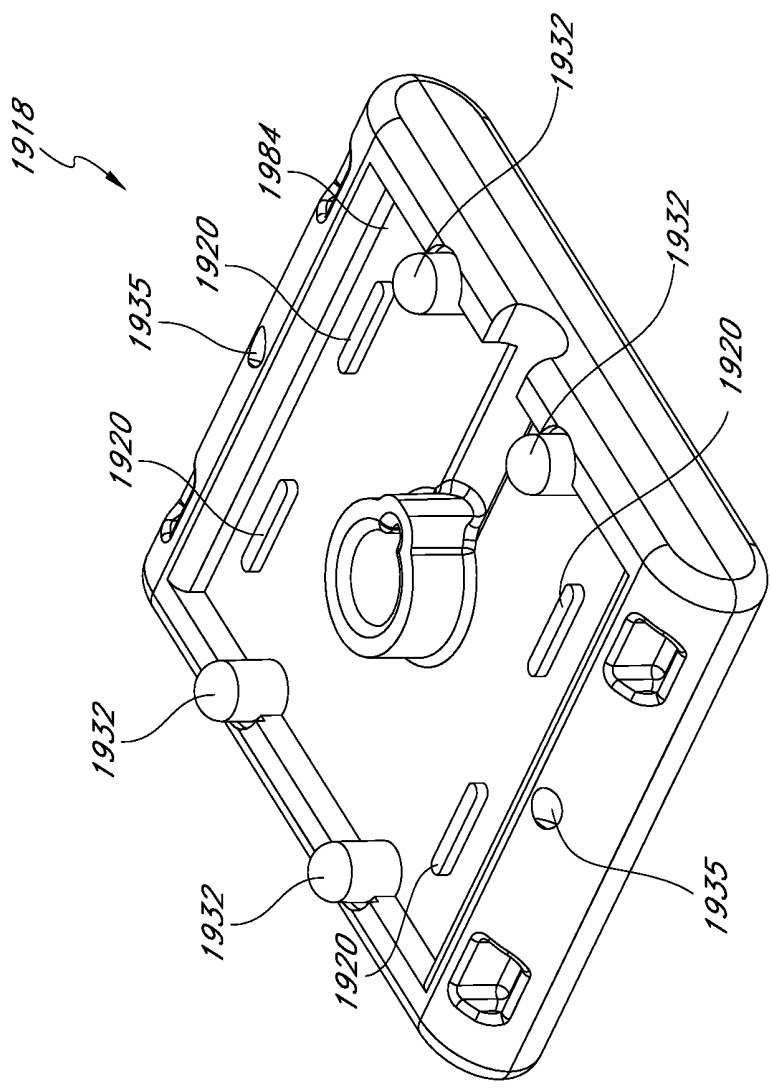
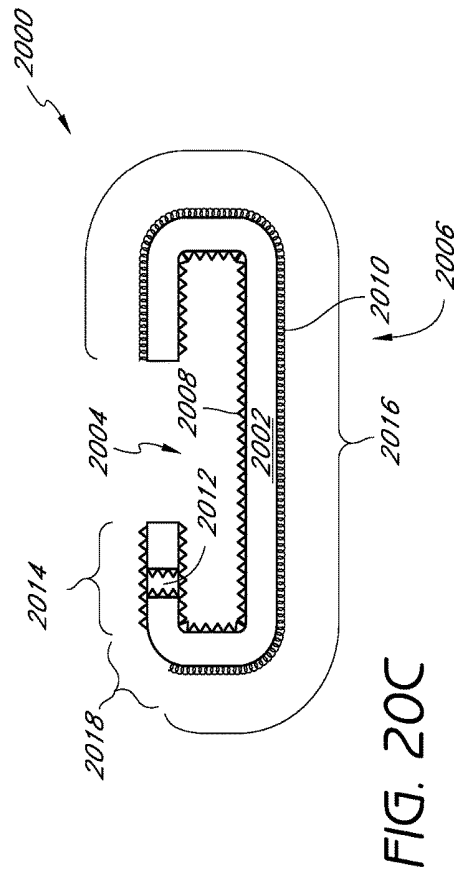
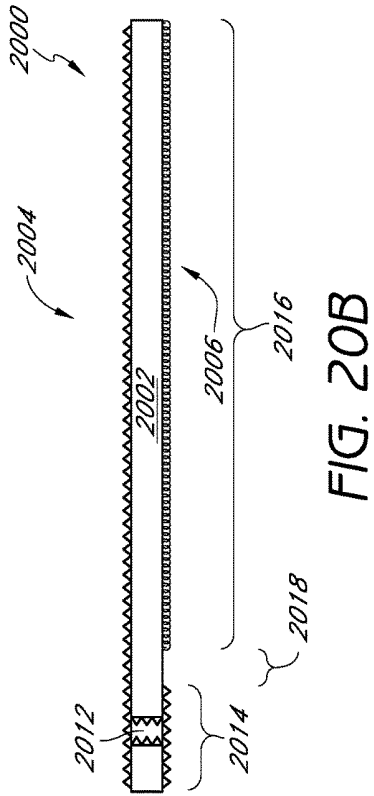
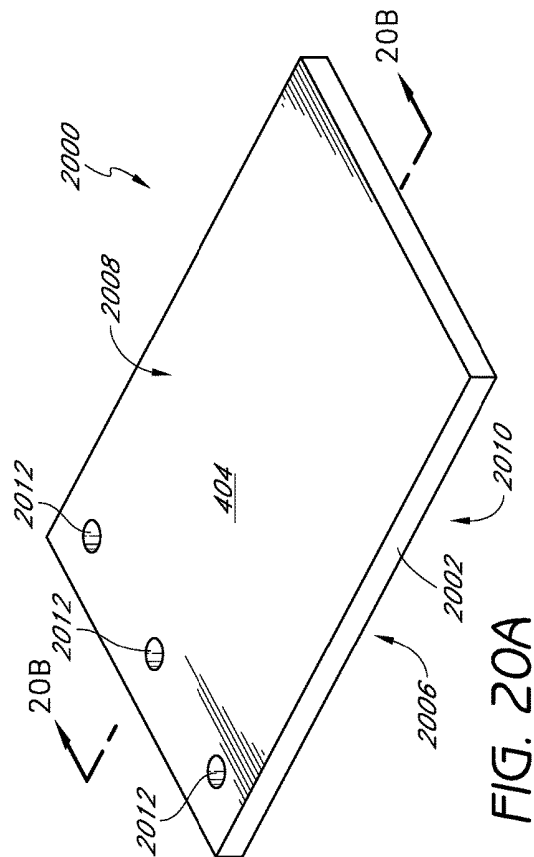


FIG. 19F



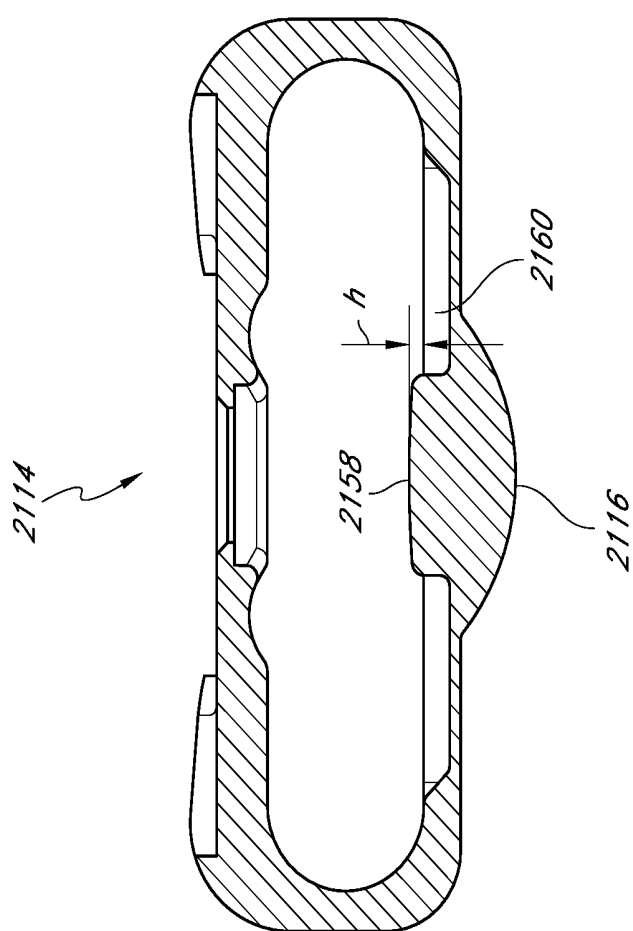


FIG. 21

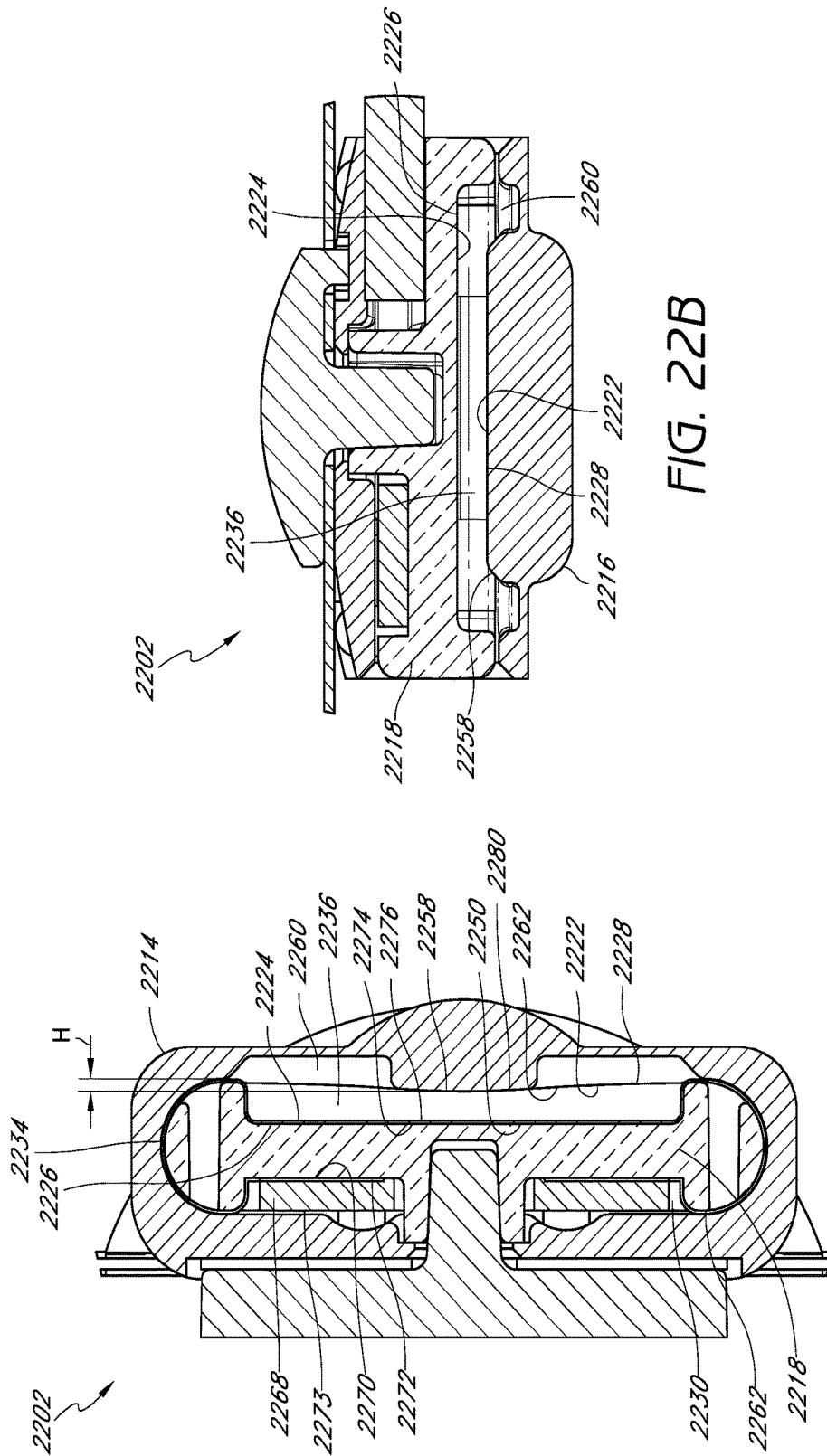


FIG. 22B

FIG. 22A

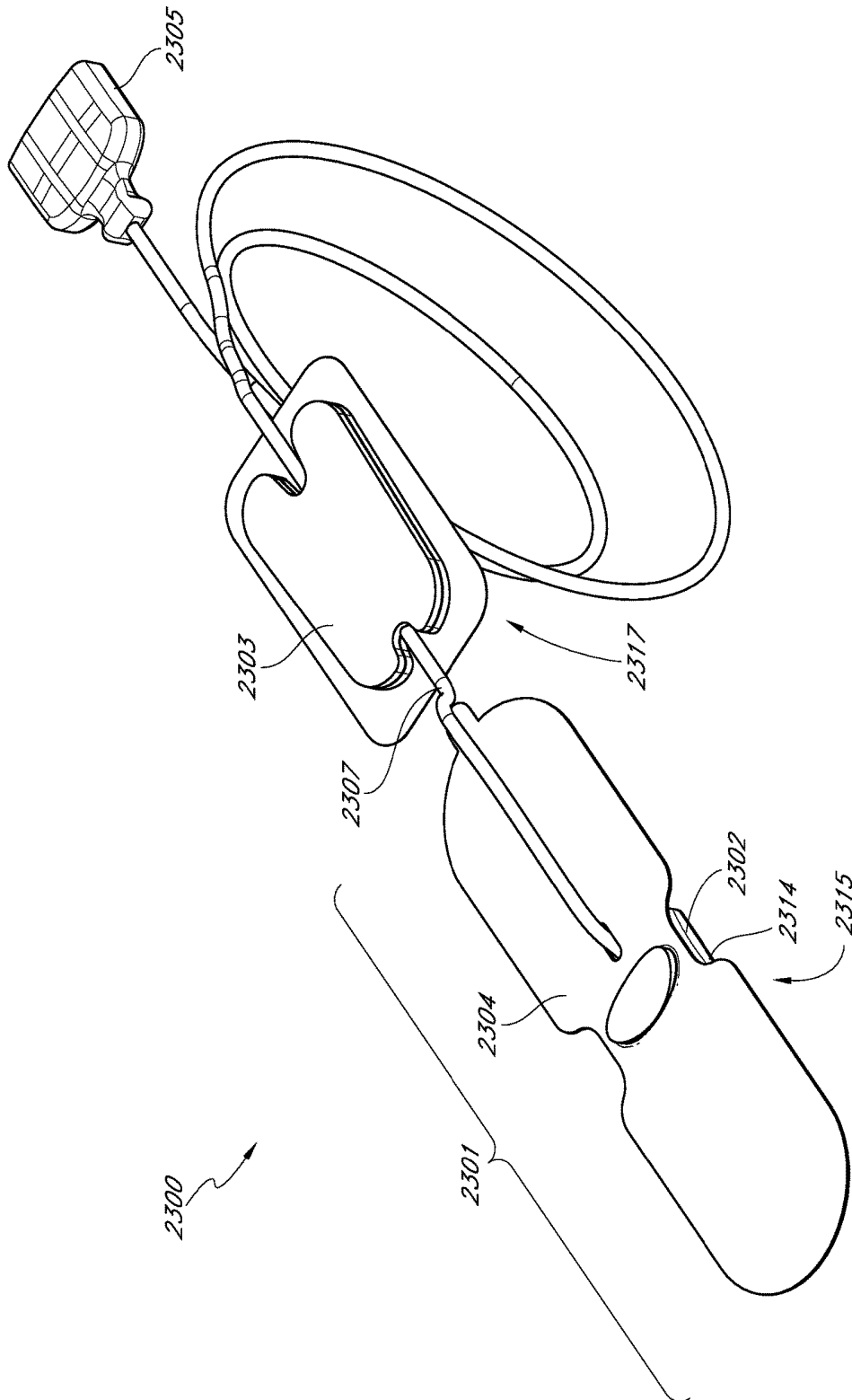


FIG. 23A

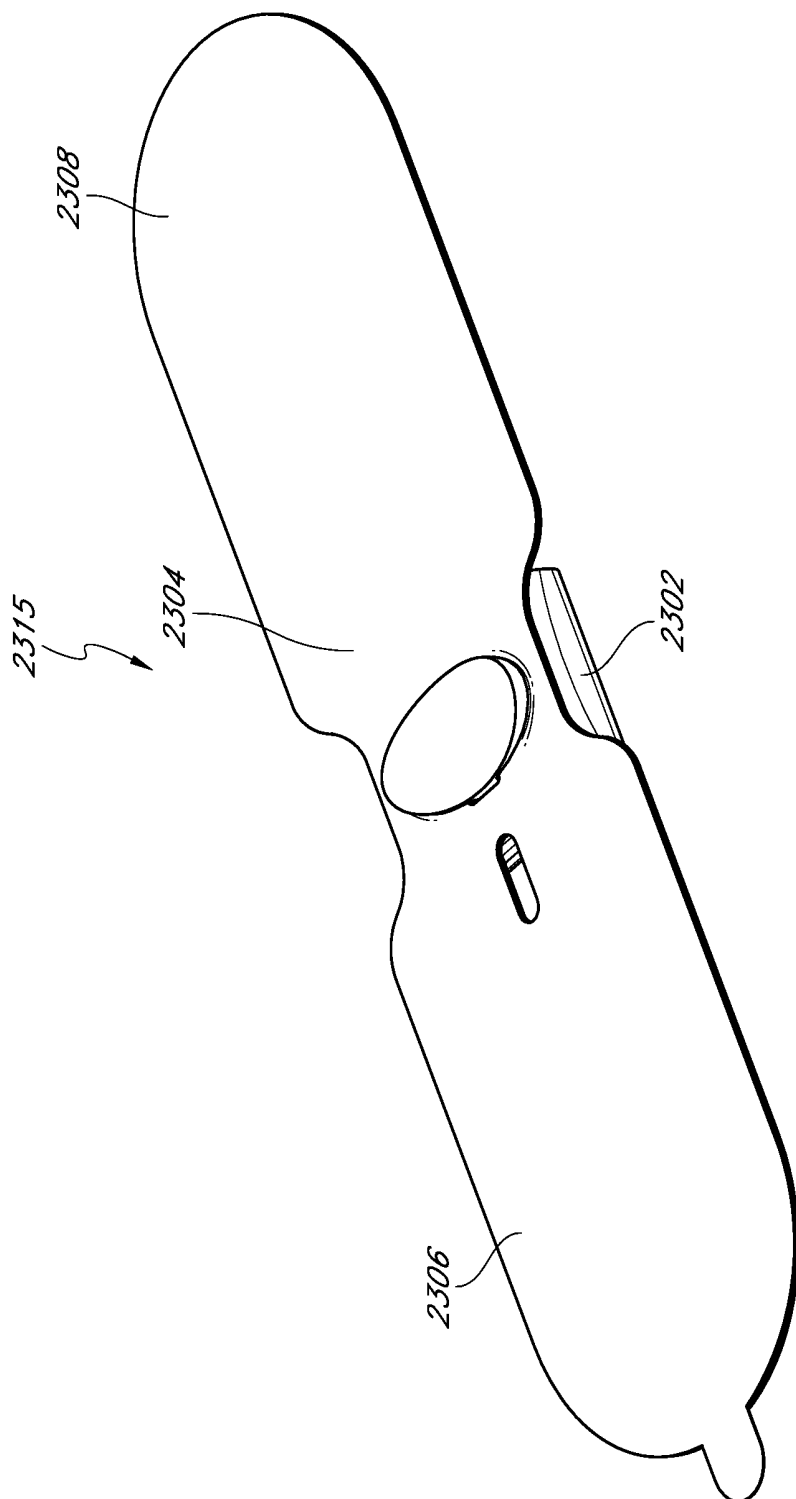


FIG. 23B

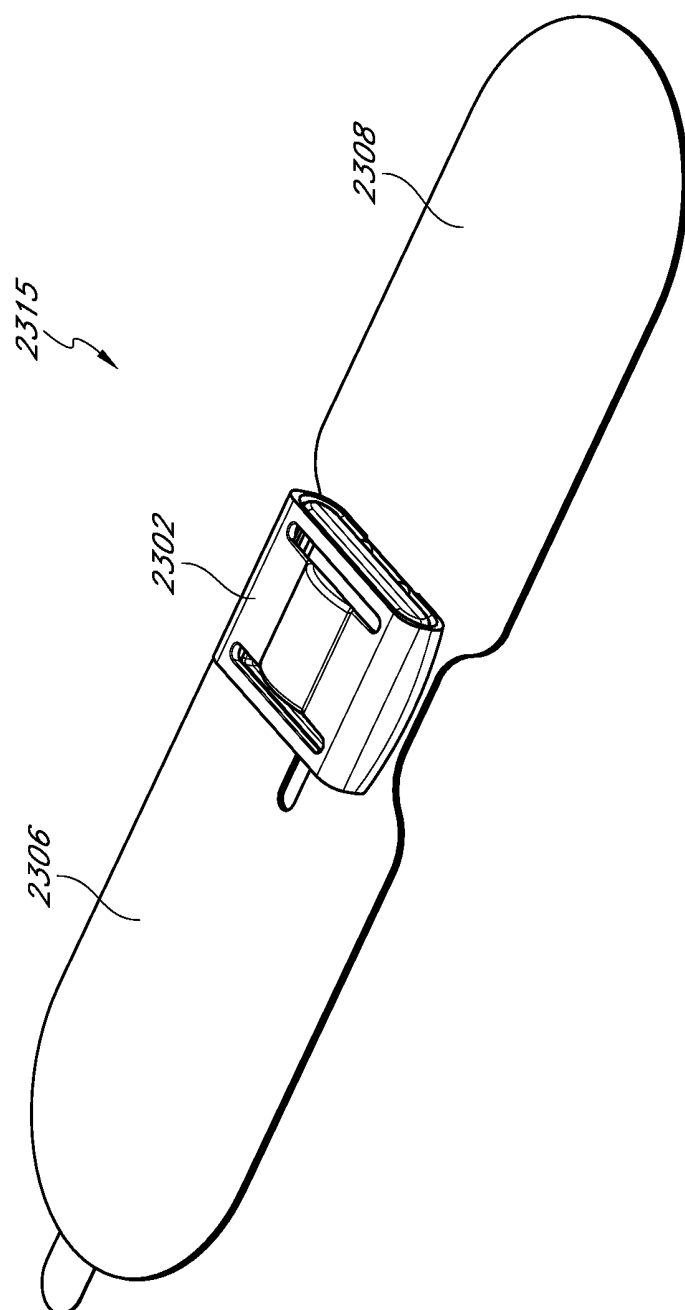


FIG. 23C

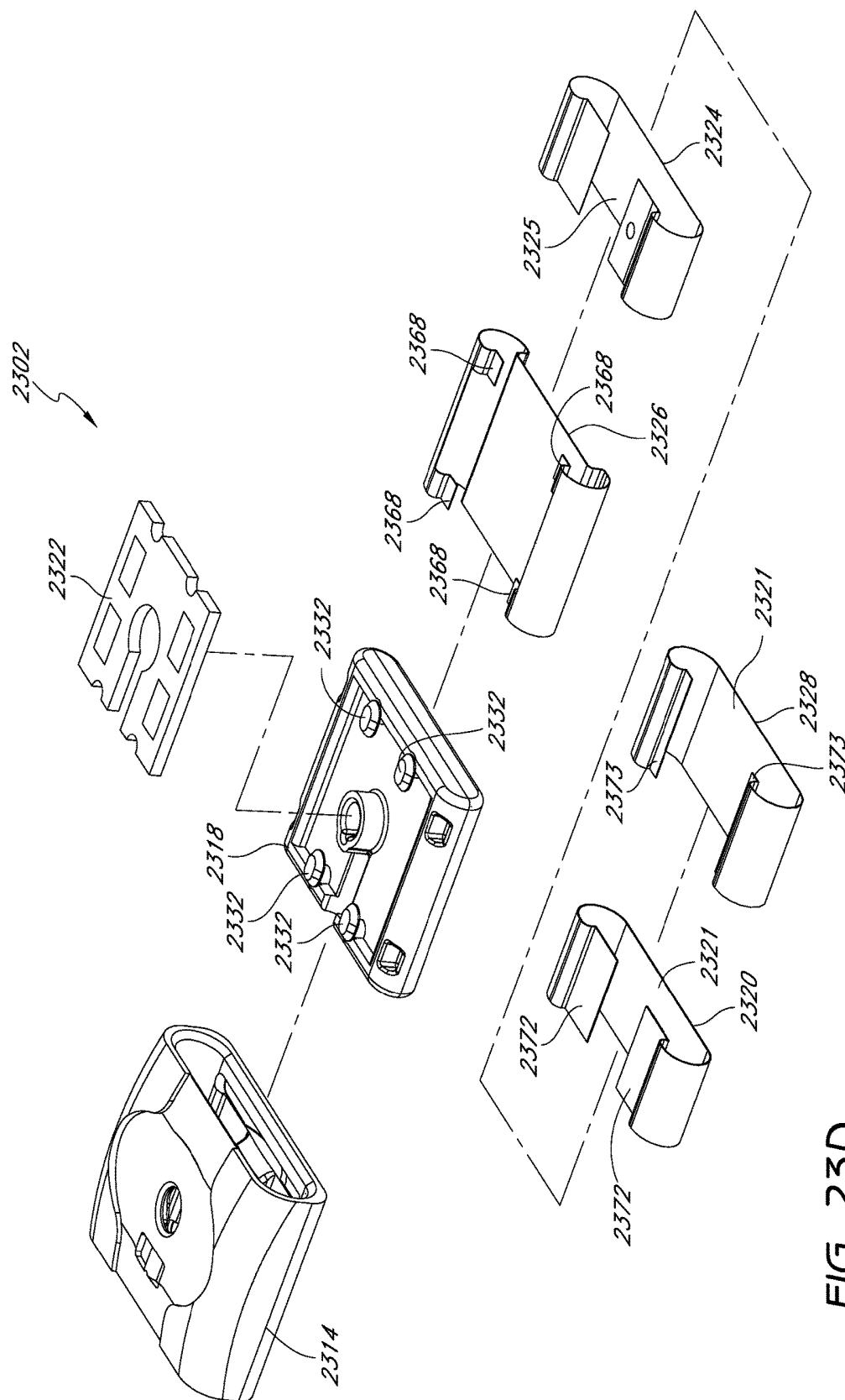


FIG. 23D

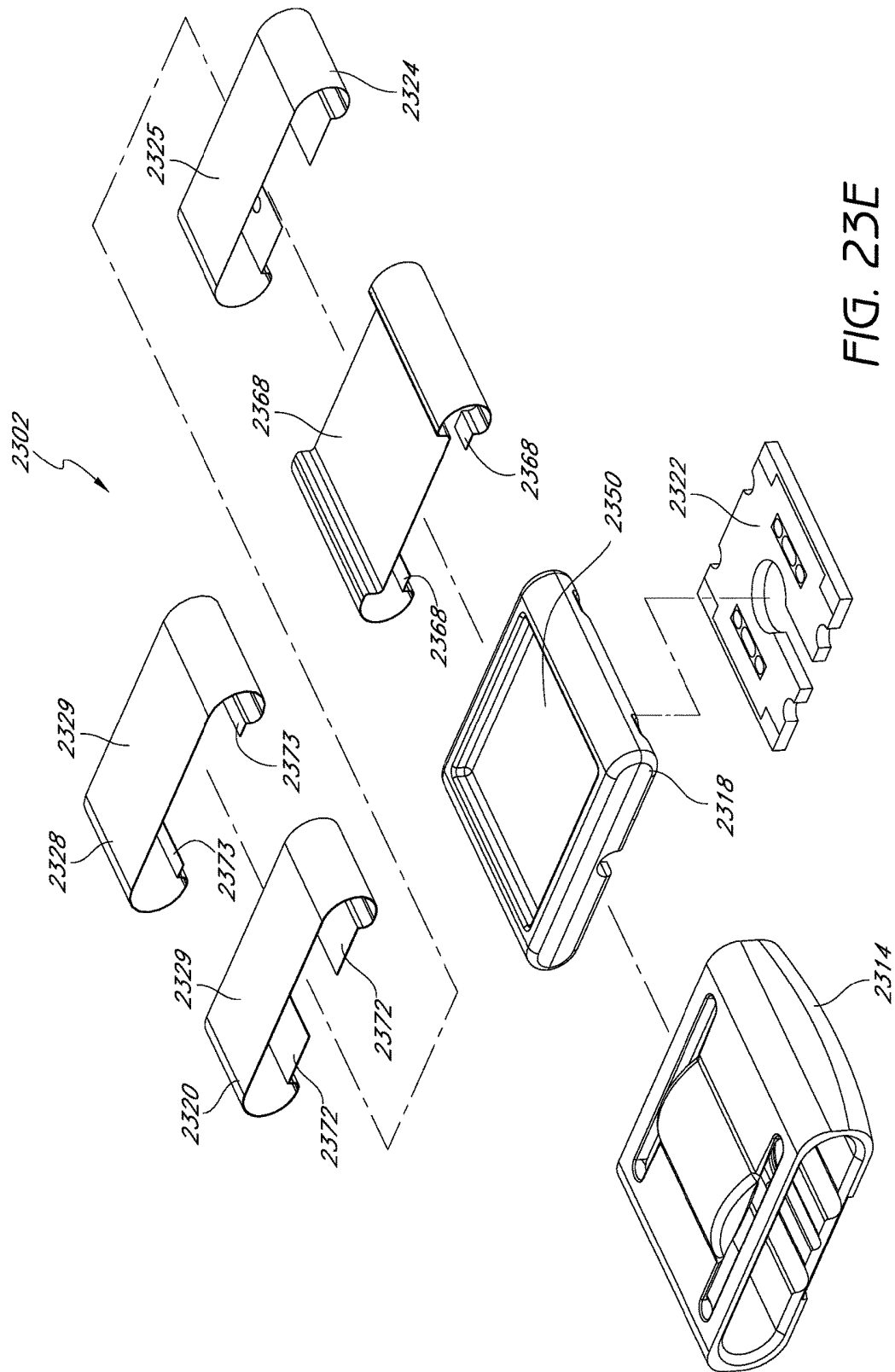


FIG. 23E

ACOUSTIC RESPIRATORY MONITORING SENSOR HAVING MULTIPLE SENSING ELEMENTS

CROSS-REFERENCE TO RELATED APPLICATIONS

This application is a continuation of U.S. patent application Ser. No. 14/247,120, filed Apr. 7, 2014, which is a continuation of U.S. patent application Ser. No. 12/904,931, filed Oct. 14, 2010, which application claims the benefit of priority under 35 U.S.C. § 119(e) of U.S. Provisional Application No. 61/252,099, filed Oct. 15, 2009, and U.S. Provisional Application No. 61/313,645, filed Mar. 12, 2010. The disclosures of all of the above identified applications are hereby incorporated by reference herein in their entireties.

Additionally, this application relates to the following U.S. patent applications, the disclosures of which are incorporated in their entirety by reference herein:

application Ser. No.	Filing Date	Title
60/893,853	Mar. 8, 2007	MULTI-PARAMETER PHYSIOLOGICAL MONITOR
60/893,850	Mar. 8, 2007	BACKWARD COMPATIBLE PHYSIOLOGICAL SENSOR WITH INFORMATION ELEMENT
60/893,858	Mar. 8, 2007	MULTI-PARAMETER SENSOR FOR PHYSIOLOGICAL MONITORING
60/893,856	Mar. 8, 2007	PHYSIOLOGICAL MONITOR WITH FAST GAIN ADJUST DATA ACQUISITION
12/044,883	Mar. 8, 2008	SYSTEMS AND METHODS FOR DETERMINING A PHYSIOLOGICAL CONDITION USING AN ACOUSTIC MONITOR
61/252,083	Oct. 15, 2009	DISPLAYING PHYSIOLOGICAL INFORMATION
12/904,836	Oct. 14, 2010	BIDIRECTIONAL PHYSIOLOGICAL INFORMATION DISPLAY
12/904,823	Oct. 14, 2010	BIDIRECTIONAL PHYSIOLOGICAL INFORMATION DISPLAY
61/141,584	Dec. 30, 2008	ACOUSTIC SENSOR ASSEMBLY
61/252,076	Oct. 15, 2009	ACOUSTIC SENSOR ASSEMBLY
12/643,939	Dec. 21, 2009	ACOUSTIC SENSOR ASSEMBLY
12/904,890	Oct. 14, 2010	ACOUSTIC RESPIRATORY MONITORING SENSOR HAVING MULTIPLE SENSING ELEMENTS
12/904,938	Oct. 14, 2010	ACOUSTIC RESPIRATORY MONITORING SENSOR HAVING MULTIPLE SENSING ELEMENTS
12/904,907	Oct. 14, 2010	ACOUSTIC PATIENT SENSOR
12/904,789	Oct. 14, 2010	ACOUSTIC RESPIRATORY MONITORING SYSTEMS AND METHODS
61/252,062	Oct. 15, 2009	PULSE OXIMETRY SYSTEM WITH LOW NOISE CABLE HUB
61/265,730	Dec. 1, 2009	PULSE OXIMETRY SYSTEM WITH ACOUSTIC SENSOR
12/904,775	Oct. 14, 2010	PULSE OXIMETRY SYSTEM WITH LOW NOISE CABLE HUB
12/905,036	Oct. 14, 2010	PHYSIOLOGICAL ACOUSTIC MONITORING SYSTEM
61/331,087	May 4, 2010	ACOUSTIC RESPIRATION DISPLAY
61/391,098	Oct. 8, 2010	ACOUSTIC MONITOR

Many of the embodiments described herein are compatible with embodiments described in the above related applications. Moreover, some or all of the features described herein can be used or otherwise combined with many of the features described in the applications listed above.

BACKGROUND

The “piezoelectric effect” is the appearance of an electric potential and current across certain faces of a crystal when it is subjected to mechanical stresses. Due to their capacity to convert mechanical deformation into an electric voltage, piezoelectric crystals have been broadly used in devices such as transducers, strain gauges and microphones. However, before the crystals can be used in many of these applications they must be rendered into a form which suits the requirements of the application. In many applications, especially those involving the conversion of acoustic waves into a corresponding electric signal, piezoelectric membranes have been used.

Piezoelectric membranes are typically manufactured from polyvinylidene fluoride plastic film. The film is endowed with piezoelectric properties by stretching the plastic while it is placed under a high-poling voltage. By stretching the film, the film is polarized and the molecular structure of the plastic aligned. A thin layer of conductive metal (typically nickel-copper) is deposited on each side of the film to form electrode coatings to which connectors can be attached.

Piezoelectric membranes have a number of attributes that make them interesting for use in sound detection, including: a wide frequency range of between 0.001 Hz to 1 GHz; a low acoustical impedance close to water and human tissue; a high dielectric strength; a good mechanical strength; and piezoelectric membranes are moisture resistant and inert to many chemicals.

Due in large part to the above attributes, piezoelectric membranes are particularly suited for the capture of acoustic waves and the conversion thereof into electric signals and, accordingly, have found application in the detection of body sounds. However, there is still a need for a reliable acoustic sensor, particularly one suited for measuring bodily sounds in noisy environments.

SUMMARY

Embodiments of an acoustic sensor and physiological monitoring system described herein are configured to provide accurate and robust measurement of bodily sounds under a variety of conditions, such as in noisy environments or in situations in which stress, strain, or movement can be imparted onto the sensor with respect to a patient.

While certain embodiments described herein are compatible with single-sensing element designs, according to certain aspects, multiple acoustic sensing elements are employed to provide enhanced physiological monitoring. For example, multiple acoustic sensing elements can be included in one or more sensor packages coupled to a patient and/or at various other locations in the monitoring environment, such as on one or more sensor packages or other components not coupled to the patient.

In some configurations, a plurality of acoustic sensing elements are advantageously arranged in a single acoustic sensor package. In some such embodiments, physical and/or electrical symmetry between the sensing elements can be exploited. In some cases, for example, the electrical poles of two or more sensing elements are connected so as to provide improved electrical shielding, enhanced signal to noise ratio, reduced design complexity and associated cost. In one such configuration, multiple sensing elements are arranged in stack on a sensor frame or other support structure. Generally, shielding can be beneficially achieved using one or more portions that are integral to the sensing elements rather than using physically separate components.

Systems and methods described herein achieve noise compensation in a variety of ways. For example, sensing elements (or groups thereof) can be arranged such that a physiological signal sensing element provides a physiological signal having both a component indicative of a target physiological signal (e.g., respiratory, heart or digestive sounds) and an interfering noise component. At least one other sensing element, on the other hand, provides a reference signal. The reference signal may include a significant noise component, but not a significant target physiological component, for example, and can advantageously be used to produce a physiological signal having a reduced noise component. For example, certain embodiments employ adaptive filtering techniques to attenuate the noise component. In various embodiments, the noise component can come from a variety of sources, and can include, without limitation, ambient noise, interfering bodily sounds emanating from the patient (e.g., respiratory, heart or digestive sounds), noise coming from skin-coupled devices (e.g., surgical or other medical equipment), etc., further specific examples of which are provided herein.

Moreover, according to certain aspects, the sensing elements are selectively configurable in a plurality of modes. For example, the sensing elements can be configured as either physiological signal sensing elements or noise sensing elements, as desired. As one illustrative example, a first sensor is used to detect respiratory sounds, while a second sensor is used to detect heart sounds. In a first monitoring mode, the system uses the first sensor to detect the target respiratory sounds, and uses the second sensor as a noise reference sensor to minimize the effect of heart sounds (and/or other interfering noise) on the respiratory signal. Conversely, the system can switch to a second mode where the first sensor is used as the reference sensor to reduce the effect of respiratory sounds (and/or other interfering noise) on the signal produced by the second sensor. A wide variety of embodiments incorporating selective sensing element configurations are described herein.

Additionally, sensing elements (or groups thereof) can be arranged with respect to one another such that components of their output signals resulting from a common source (e.g., the patient's body) will be correlated or otherwise generally similar. The signal components from interfering noise sources, on the other hand, can be expected to be uncorrelated or otherwise have certain dissimilarities (e.g., phase or time shift). In these cases, the output signals from the first and second acoustic sensing elements can be combined in ways that accentuate commonalities between the two signals while attenuating differences.

According to yet another aspect of the disclosure, an acoustic sensor includes one or more sensing elements supported by a frame or other support structure. The sensing elements contact the frame at certain locations and are spaced from the frame at others. The sensing elements and frame define a cavity in which the sensing elements vibrate in response to acoustic signals received from a medical patient. However, skin elasticity and the force used to attach the acoustic sensor to the medical patient's skin can affect the volume and/or air pressure within the cavity defined by the sensing elements and frame. Variability in skin elasticity or attachment force can lead to variability in cavity resonance, which can cause unwanted variability in sensor performance. For example, an acoustic sensor that is attached to very elastic skin may provide a different output signal than an acoustic sensor that is attached to firmer or tighter skin. Similarly, an acoustic sensor loosely attached to

patient's skin may provide a different output signal than an acoustic sensor tightly attached to a patient's skin.

To compensate for skin elasticity and attachment variability, in one embodiment the acoustic sensor support includes one or more pressure equalization pathways. The pathways provide an air-flow channel from the cavity defined by the sensing elements and frame to the ambient air pressure. By equalizing pressure within the cavity with ambient during sensing, variability in sensor performance may be reduced and/or eliminated. In some embodiments, the pressure equalization pathways include one or more holes, notches, ports, or channels that extend from within the sensor's cavity to a location in communication with ambient air pressure.

In certain embodiments, a medical device is provided for non-invasively outputting a reduced noise signal responsive to acoustic vibrations indicative of one or more physiological parameters of a medical patient. In some embodiments, the medical device includes a first acoustic sensing element configured to be acoustically coupled to the body of a patient, the first acoustic sensing element being configured to output a first signal comprising a physiological signal component and a noise component. The medical device can also include a second acoustic sensing element being configured to output a second signal comprising at least a noise component. The medical device of some embodiments includes a noise attenuator configured to produce a reduced noise signal in response to the first and second signals. The reduced noise signal can include a physiological signal component and a noise component. In certain embodiments, the ratio of the physiological signal component of the reduced noise signal to the noise component of the reduced noise signal is greater than the ratio of the physiological signal component of the first signal to the noise component of the first signal.

According to certain aspects, a method of providing a reduced noise signal responsive to acoustic vibrations indicative of one or more physiological parameters of a medical patient is provided. The method can include outputting a first signal using first acoustic sensing element coupled to the body of a patient. The signal may comprise a physiological component and a noise component. The method can further include outputting a second signal using the second acoustic sensing element, the second signal comprising at least a noise component. In certain embodiments, the method further includes processing the first and second signals using a noise attenuator to produce a reduced noise signal in response to the first and second signals. The reduced noise signal can include a physiological signal component and a noise component. In certain embodiments, the ratio of the physiological signal component of the reduced noise signal to the noise component of the reduced noise signal is greater than the ratio of the physiological signal component of the first signal to the noise component of the first signal.

In certain embodiments, a medical device is provided for non-invasively generating a reduced noise signal responsive to acoustic vibrations indicative of one or more physiological parameters of a medical patient. The medical device can include at least one first acoustic sensing element configured to generate a first signal in response to acoustic vibrations. The medical device of certain embodiments also includes at least one second acoustic sensing element configured to generate a second signal in response to acoustic vibrations. In certain embodiments, the medical device further includes a noise attenuation module configured to generate a reduced

noise signal indicative of one or more physiological parameters of a medical patient in response to at least one of the first and second signals.

A medical sensor is provided in some embodiments for non-invasively outputting signals responsive to acoustic vibrations indicative of one or more physiological parameters of a medical patient. The medical sensor can include a first acoustic sensing element for generating a first signal. The medical sensor can also include a second acoustic sensing element for generating a second signal. The first and second signals in some embodiments are configured to be provided to a noise attenuator adapted to reduce a noise component of the first or second signal.

In certain embodiments, an acoustic sensor is provided for non-invasively outputting signals responsive to acoustic vibrations indicative of one or more physiological parameters of a medical patient. In certain embodiments, the acoustic sensor includes a sensor support. The acoustic sensor can also include a first acoustic sensing element at least partially supported by the sensor support and configured to output a first signal responsive to acoustic vibrations. The acoustic sensor of some embodiments includes a second acoustic sensing element at least partially supported by the sensor support and configured to output a second signal responsive to acoustic vibrations. In some embodiments, the first and second acoustic sensing elements are configured to provide the first and second signals to a noise attenuator configured to output a reduced noise signal having a higher signal to noise ratio than either of the first and second signals.

In certain embodiments, a method is provided of non-invasively outputting signals responsive to acoustic vibrations indicative of one or more physiological parameters of a medical patient. The method can include providing a sensor comprising a sensor support, a first acoustic sensing element at least partially supported by the sensor support, and a second acoustic sensing element at least partially supported by the sensor support. The method can further include outputting a first signal using the first acoustic sensing element. In certain embodiments, the first signal is responsive to acoustic vibrations, and the first acoustic sensing element is coupled to a medical patient. The method can include outputting a second signal using the second acoustic sensing element. In certain embodiments, the second signal responsive to acoustic vibrations, and the second acoustic sensing element coupled to the medical patient. In certain embodiments, the method includes providing the first signal and the second signal to a noise attenuator configured to output a reduced noise signal having a higher signal to noise ratio than either of the first and second signals.

In certain embodiments, an acoustic sensor is provided for non-invasively outputting signals responsive to acoustic vibrations indicative of one or more physiological parameters of a medical patient. The acoustic sensor can include a sensor support, and a first piezoelectric film at least partially supported by the sensor support and comprising a first electrode and a second electrode. In certain embodiments, the sensor includes a second piezoelectric film at least partially supported by the sensor support and comprising a first electrode and second electrode. In some embodiments, the first electrode of the first piezoelectric film and the first electrode of the second piezoelectric film are coupled to a common potential, and the second electrode of the first piezoelectric film and the second electrode of the second piezoelectric film are coupled to a noise attenuator.

In certain embodiments, an acoustic sensor is provided for non-invasively outputting signals responsive to acoustic

vibrations indicative of one or more physiological parameters of a medical patient. In some embodiments, the acoustic sensor includes a sensor support. In some embodiments, the acoustic sensor includes a first acoustic sensing element at least partially supported by the sensor support and comprising an inner portion and an outer portion. In some embodiments, the acoustic sensor includes a second acoustic sensing element at least partially supported by the sensor support and comprising an inner portion and an outer portion. In certain embodiments, the acoustic sensor is configured such that the inner portions are positioned between the outer portions, the outer portions forming an electrical shielding barrier around the inner portions.

In certain embodiments, a method is provided of manufacturing an acoustic sensor for non-invasively outputting signals responsive to acoustic vibrations indicative of one or more physiological parameters of a medical patient. The method can include providing a first acoustic sensing element comprising an inner portion and an outer portion. The method can also include providing a second acoustic sensing element comprising an inner portion and an outer portion. In certain embodiments, the method includes attaching the first acoustic sensing element to a sensor support. The method in some embodiments includes attaching the second sensing element to the sensor support over the first acoustic sensing element. In certain embodiments, the inner portions of the first and second acoustic sensing elements are disposed between the outer portions of the first and second acoustic sensing elements, and the outer portions form an electrical shielding barrier around the inner portions.

An acoustic sensor is provided in some embodiments that is configured to non-invasively detect acoustic vibrations associated with a medical patient, the acoustic vibrations indicative of one or more physiological parameters of the medical patient. The sensor can include a sensor support and first and second sensing membranes supported by the sensor support, each of said first and second sensing membranes comprising first and second surfaces on opposite sides of each of said first and second sensing membranes. In some embodiments, the first and second sensing membranes are aligned such that said first surfaces face each other. The first surfaces in some embodiments are configured to provide an electrical signal indicative of a physiological parameter of a medical patient, and said second surfaces are configured to provide electrical shielding around said first surfaces.

In some embodiments, an acoustic sensor is provided that is configured to non-invasively detect acoustic vibrations associated with a medical patient. The acoustic vibrations can be indicative of one or more physiological parameters of the medical patient. In certain embodiments, the sensor includes at least one sound-sensing membrane is configured to detect acoustic vibrations associated with a medical patient when the acoustic sensor is attached to the medical patient. The sensor can also include a sensor support defining an acoustic cavity and configured to support the at least one sensing membrane over the acoustic cavity. The sensor support may include at least one pressure equalization pathway formed in a wall of the sensor support, the at least one pressure equalization pathway extending from the acoustic cavity to ambient air pressure.

In certain embodiments, an acoustic sensor is configured to non-invasively detect acoustic vibrations associated with a medical patient, the acoustic vibrations indicative of one or more physiological parameters of the medical patient. The sensor can include at least one sound-sensing membrane configured to detect acoustic vibrations associated with a medical patient when the acoustic sensor is attached to the

medical patient. The sensor can further include a sensor support configured to support the at least one sensing membrane against the medical patient's skin. In some embodiments, the sensor is configured to provide an electrical signal in response to acoustic vibrations detected by the at least one sound-sensing membrane substantially independent of a force used to attach the sensor to the medical patient's skin.

For purposes of summarizing the disclosure, certain aspects, advantages and novel features of the inventions have been described herein. It is to be understood that not necessarily all such advantages can be achieved in accordance with any particular embodiment of the inventions disclosed herein. Thus, the inventions disclosed herein can be embodied or carried out in a manner that achieves or optimizes one advantage or group of advantages as taught herein without necessarily achieving other advantages as can be taught or suggested herein.

BRIEF DESCRIPTION OF THE DRAWINGS

Throughout the drawings, reference numbers can be used to indicate correspondence between referenced elements. The drawings are provided to illustrate embodiments of the inventions described herein and not to limit the scope thereof.

FIGS. 1A-B are block diagrams illustrating physiological monitoring systems in accordance with embodiments of the disclosure.

FIG. 1C is a top perspective view illustrating portions of a sensor system in accordance with an embodiment of the disclosure.

FIGS. 2A-2B are block diagrams of example embodiments of patient sensors that including first and second physiological signal acoustic sensing elements and at least one acoustic coupler for acoustically coupling both of the first and second physiological signal acoustic sensing elements to a patient's body.

FIG. 3A is a schematic illustration of an embodiment of a circuit for improving signal-to-noise ratio by combining physiological signals from two or more acoustic sensing elements.

FIG. 3B is a schematic illustration of an embodiment of a circuit for improving signal-to-noise ratio by combining physiological signals from two or more acoustic sensing elements arranged in a stacked configuration.

FIG. 4A is a cross-sectional schematic drawing of an embodiment of an acoustic sensor that includes first and second acoustic sensing elements in a stacked configuration.

FIG. 4B shows a cross-sectional schematic drawing of a portion of the first and second stacked sensing elements of FIG. 4A.

FIGS. 5A-5D show views of example acoustic sensing elements having electrode coating configurations tailored for use in a stacked configuration.

FIGS. 6A-6B are top and bottom exploded, perspective views, respectively, of a sensor incorporating multiple sensing elements in accordance with embodiments described herein.

FIG. 7 is a block diagram of an example acoustic physiological monitoring system having noise compensation features.

FIG. 8 is a block diagram of an embodiment of an acoustic physiological monitoring system with an acoustic sensor that includes first and second acoustic sensing elements.

FIG. 9A is a block diagram of an embodiment of an acoustic physiological monitoring system with first and second acoustic sensing elements disposed in separate acoustic sensors.

FIG. 9B is a block diagram of an embodiment of an acoustic physiological monitoring system with an acoustic sensor that includes a first acoustic sensing element, and a physiological monitor unit that includes a second acoustic sensing element.

FIGS. 9C-9D illustrate example systems including dual acoustic sensors applied to a patient according to certain embodiments.

FIG. 10 is a block diagram of an embodiment of an acoustic sensor that includes a physiological signal acoustic sensing element with an acoustic coupler for acoustically coupling it to a patient's body, and a noise acoustic sensing element.

FIG. 11 is a block diagram of an embodiment of an acoustic sensor that includes a physiological signal acoustic sensing element with an acoustic coupler for increasing acoustic coupling between it and a patient's body, and a noise acoustic sensing element with an acoustic decoupler for decreasing acoustic coupling between it and the patient's body.

FIG. 12 is a cross-sectional schematic drawing of an embodiment of an acoustic sensor that includes a physiological signal acoustic sensing element and a noise acoustic sensing element.

FIG. 13 is a cross-sectional schematic drawing of another embodiment of an acoustic sensor that includes a physiological signal acoustic sensing element and a noise acoustic sensing element.

FIG. 14 is a cross-sectional schematic drawing of another embodiment of an acoustic sensor that includes a physiological signal acoustic sensing element and a noise acoustic sensing element.

FIG. 15 is a cross-sectional schematic drawing of an embodiment of an acoustic sensor that includes a piezoelectric physiological signal acoustic sensing element and a separate noise microphone.

FIG. 16 illustrates a time plot of an acoustic physiological signal corrupted by noise, as well as a time plot of the noise.

FIG. 17 is a block diagram of a noise attenuator of an acoustic physiological monitoring system.

FIG. 18 is a block diagram of an embodiment of a signal quality calculator in an acoustic physiological monitoring system.

FIG. 19A is a top perspective view illustrating portions of a sensor assembly in accordance with an embodiment of the disclosure.

FIGS. 19B-19C are top and bottom perspective views, respectively, of a sensor including a sensor subassembly and an attachment subassembly of FIG. 19A.

FIGS. 19D-19E are top and bottom exploded, perspective views, respectively, of the sensor subassembly of FIGS. 19A-19C.

FIG. 19F shows a top perspective view of an embodiment of a support frame.

FIG. 20A a perspective view of a sensing element according to an embodiment of the disclosure usable with the sensor assembly of FIG. 19A.

FIG. 20B is a cross-sectional view of the sensing element of FIG. 20A along the line 20B-20B.

FIG. 20C is a cross-sectional view of the sensing element of FIGS. 20A-B shown in a wrapped configuration.

FIG. 21 is a cross-sectional view of the coupler of FIGS. 19A-19E taken along the line 21-21 shown in FIG. 19D.

FIGS. 22A-22B are cross-sectional views of the sensor subassembly of FIGS. 19B-19C along the lines 22A-22A and 22B-22B, respectively.

FIG. 23A is a top perspective view illustrating portions of a sensor assembly in accordance with another embodiment of the disclosure.

FIGS. 23B-23C are top and bottom perspective views, respectively, of a sensor including a sensor subassembly and an attachment subassembly of FIG. 23A.

FIGS. 23D-23E are top and bottom exploded, perspective views, respectively, of the sensor subassembly of FIGS. 23A-C.

DETAILED DESCRIPTION

Various embodiments will be described hereinafter with reference to the accompanying drawings. These embodiments are illustrated and described by example only, and are not intended to be limiting.

Overview

In various embodiments, an acoustic sensor configured to operate with a physiological monitoring system includes an acoustic signal processing system that measures and/or determines any of a variety of physiological parameters of a medical patient. For example, in an embodiment, the physiological monitoring system includes an acoustic monitor. The acoustic monitor may be an acoustic respiratory monitor which can determine any of a variety of respiratory parameters of a patient, including respiratory rate, expiratory flow, tidal volume, minute volume, apnea duration, breath sounds, riles, rhonchi, stridor, and changes in breath sounds such as decreased volume or change in airflow. In addition, in some cases the acoustic signal processing system monitors other physiological sounds, such as heart rate to help with probe off detection, heart sounds (S1, S2, S3, S4, and murmurs), and change in heart sounds such as normal to murmur or split heart sounds indicating fluid overload. Moreover, the acoustic signal processing system may (1) use a second probe over the chest for additional heart sound detection; (2) keep the user inputs to a minimum (example, height); and/or (3) use a Health Level 7 (HL7) interface to automatically input patient demography.

In certain embodiments, the physiological monitoring system includes an electrocardiograph (ECG or EKG) that measures and/or determines electrical signals generated by the cardiac system of a patient. The ECG includes one or more sensors for measuring the electrical signals. In some embodiments, the electrical signals are obtained using the same sensors used to obtain acoustic signals.

In still other embodiments, the physiological monitoring system includes one or more additional sensors used to determine other desired physiological parameters. For example, in some embodiments, a photoplethysmograph sensor determines the concentrations of analytes contained in the patient's blood, such as oxyhemoglobin, carboxyhemoglobin, methemoglobin, other dyshemoglobins, total hemoglobin, fractional oxygen saturation, glucose, bilirubin, and/or other analytes. In other embodiments, a capnograph determines the carbon dioxide content in inspired and expired air from a patient. In other embodiments, other sensors determine blood pressure, pressure sensors, flow rate, air flow, and fluid flow (first derivative of pressure). Other sensors may include a pneumotachometer for measuring air flow and a respiratory effort belt. In certain embodiments, these sensors are combined in a single processing system which processes signal output from the sensors on a single multi-function circuit board.

Referring to the drawings, FIGS. 1A through 1C illustrate example patient monitoring systems, sensors, and cables that can be used to provide acoustic physiological monitoring of a patient, such as respiratory monitoring. FIGS. 2A-18 illustrate embodiments of sensors and systems, such as those incorporating multiple acoustic sensing elements to provide certain beneficial results, including enhanced signal-to-noise ratio (SNR), electrical shielding and noise compensation, for example. Embodiments of FIGS. 2A-18 can be implemented at least in part using the systems and sensors described in FIGS. 1A through 1C. FIGS. 19A-23E show additional acoustic sensors and associated components compatible with embodiments described herein.

Turning to FIG. 1A, an embodiment of a physiological monitoring system 10 is shown. In the physiological monitoring system 10, a medical patient 12 is monitored using one or more sensor 13, each of which transmits a signal over a cable 15 or other communication link or medium to a physiological monitor 17. The physiological monitor 17 includes a processor 19 and, optionally, a display 11. The one or more sensors 13 include sensing elements such as, for example, acoustic piezoelectric devices, electrical ECG leads, pulse oximetry sensors, or the like. The sensors 13 can generate respective signals by measuring a physiological parameter of the patient 12. The signals are then processed by one or more processors 19. The one or more processors 19 then communicate the processed signal to the display 11. In an embodiment, the display 11 is incorporated in the physiological monitor 17. In another embodiment, the display 11 is separate from the physiological monitor 17. In one embodiment, the monitoring system 10 is a portable monitoring system. In another embodiment, the monitoring system 10 is a pod, without a display, that is adapted to provide physiological parameter data to a display.

For clarity, a single block is used to illustrate the one or more sensors 13 shown in FIG. 1A. It should be understood that the sensor 13 shown is intended to represent one or more sensors. In an embodiment, the one or more sensors 13 include a single sensor of one of the types described below. In another embodiment, the one or more sensors 13 include at least two acoustic sensors. In still another embodiment, the one or more sensors 13 include at least two acoustic sensors and one or more ECG sensors, pulse oximetry sensors, bioimpedance sensors, capnography sensors, and the like. In each of the foregoing embodiments, additional sensors of different types are also optionally included. Other combinations of numbers and types of sensors are also suitable for use with the physiological monitoring system 10.

In some embodiments of the system shown in FIG. 1A, all of the hardware used to receive and process signals from the sensors are housed within the same housing. In other embodiments, some of the hardware used to receive and process signals is housed within a separate housing. In addition, the physiological monitor 17 of certain embodiments includes hardware, software, or both hardware and software, whether in one housing or multiple housings, used to receive and process the signals transmitted by the sensors 13.

As shown in FIG. 1B, the acoustic sensor 13 can include a cable 25. The cable 25 can include three conductors within an electrical shielding. One conductor 26 can provide power to a physiological monitor 17, one conductor 28 can provide a ground signal to the physiological monitor 17, and one conductor 28 can transmit signals from the sensor 13 to the physiological monitor 17. For multiple sensors 103, one or more additional cables 115 can be provided.

In some embodiments, the ground signal is an earth ground, but in other embodiments, the ground signal is a patient ground, sometimes referred to as a patient reference, a patient reference signal, a return, or a patient return. In some embodiments, the cable **25** carries two conductors within an electrical shielding layer, and the shielding layer acts as the ground conductor. Electrical interfaces **23** in the cable **25** can enable the cable to electrically connect to electrical interfaces **21** in a connector **20** of the physiological monitor **17**. In another embodiment, the sensor **13** and the physiological monitor **17** communicate wirelessly.

FIG. 1C illustrates an embodiment of a sensor system **100** including a sensor **101** suitable for use with any of the physiological monitors shown in FIGS. 1A and 1B. The sensor system **100** includes a sensor **101**, a sensor cable **117**, a patient anchor **103** attached to the sensor cable **117**, and a connector **105** attached to the sensor cable **117**. The sensor **101** includes a shell **102** configured to house certain componentry of the sensor **101**, and an attachment subassembly **104** positioned the sensor **101** and configured to attach the sensor **101** to the patient.

The sensor **101** can be removably attached to an instrument cable **111** via an instrument cable connector **109**. The instrument cable **111** can be attached to a cable hub **120**, which includes a port **121** for receiving a connector **112** of the instrument cable **111** and a second port **123** for receiving another cable. In certain embodiments, the second port **123** can receive a cable connected to a pulse oximetry or other sensor. In addition, the cable hub **120** could include additional ports in other embodiments for receiving additional cables. The hub includes a cable **122** which terminates in a connector **124** adapted to connect to a physiological monitor (not shown). In another embodiment, no hub is provided and the acoustic sensor **101** is connected directly to the monitor, via an instrument cable **111** or directly by the sensor cable **117**, for example.

The component or group of components between the sensor **101** and the monitor in any particular embodiment may be referred to generally as a cabling apparatus. For example, where one or more of the following components are included, such components or combinations thereof may be referred to as a coupling apparatus: the sensor cable **117**, the connector **105**, the cable connector **109**, the instrument cable **111**, the hub **120**, the cable **122**, and/or the connector **124**. It should be noted that one or more of these components may not be included, and that one or more other components may be included between the sensor **101** and the monitor, forming the cabling apparatus.

The acoustic sensor **101** can further include circuitry for detecting and transmitting information related to biological sounds to the physiological monitor. These biological sounds can include heart, breathing, and/or digestive system sounds, in addition to many other physiological phenomena. The acoustic sensor **101** in certain embodiments is a biological sound sensor, such as the sensors described herein. In some embodiments, the biological sound sensor is one of the sensors such as those described in U.S. patent application Ser. No. 12/044,883, filed Mar. 7, 2008, which is incorporated in its entirety by reference herein (the '883 application). In other embodiments, the acoustic sensor **101** is a biological sound sensor such as those described in U.S. Pat. No. 6,661,161 or U.S. patent application Ser. No. 12/643,939, filed on Dec. 21, 2009 (the '939 application), both of which are incorporated by reference herein in their entirety. Other embodiments include other suitable acoustic sensors. For example, in certain embodiments, compatible acoustic sensors can be configured to provide a variety of auscultation

functions, including live and/or recorded audio output (e.g., continuous audio output) for listening to patient bodily or speech sounds. Examples of such sensors and sensors capable of providing other compatible functionality can be found in U.S. patent application Ser. No. 12/905,036 embodiment, the sensing elements **920**, **921** can be configured to sense and process ultrasonic signals (e.g., for ultrasonic imaging). Examples of sensors capable of various types, entitled PHYSIOLOGICAL ACOUSTIC MONITORING SYSTEM, filed on Oct. 14, 2010, which is incorporated by reference herein in its entirety.

In an embodiment, the acoustic sensor **101** includes one or more sensing elements (not shown), such as, for example, a piezoelectric device or other acoustic sensing device. Where a piezoelectric membrane is used, a thin layer of conductive metal can be deposited on each side of the film as electrode coatings, forming electrical poles. The opposing surfaces or poles may be referred to as an anode and cathode, respectively. Each sensing element can generate a voltage potential across the electrical poles that is responsive to vibrations generated by the patient.

The shell **102** according to certain embodiments houses a frame (not shown) or other support structure configured to support various components of the sensor **101**. The one or more sensing elements can be generally wrapped in tension around the frame. For example, the sensing elements can be positioned across an acoustic cavity disposed on the bottom surface of the frame. Thus, the sensing elements according to some embodiments are free to respond to acoustic waves incident upon them, resulting in corresponding induced voltages across the poles of the sensing elements.

Additionally, the shell **102** can include an acoustic coupler (not shown), which advantageously improves the coupling between the source of the signal to be measured by the sensor (e.g., the patient's body) and the sensing element. The acoustic coupler of one embodiment includes a bump positioned to apply pressure to the sensing element so as to bias the sensing element in tension. For example, the bump can be positioned against the portion of the sensing element that is stretched across the cavity of the frame.

The attachment sub-assembly **104** in some embodiments includes first and second elongate portions **106**, **108**. The first and second elongate portions **106**, **108** can include patient adhesive (e.g., in some embodiments, tape, glue, a suction device, etc.). The adhesive on the elongate portions **106**, **108** can be used to secure the sensor subassembly **102** to a patient's skin. One or more resilient backbone members **110** included in the first and/or second elongate portions **106**, **108** can beneficially bias the sensor subassembly **102** in tension against the patient's skin and/or reduce stress on the connection between the patient adhesive and the skin.

While an example sensor system **100** has been provided, embodiments described herein are compatible with a variety of sensors and associated components. For example, compatible acoustic couplers, support frames, attachment sub-assemblies, sensing elements, and other components are described with respect to FIGS. 19-23 below and in the '939 application.

Improving Signal-To-Noise Ratio Using Multiple Sensors
FIG. 2A is a block diagram of an embodiment of a patient sensor **215** that includes first and second physiological signal acoustic sensing elements **220**, **221**. The sensing elements **220**, **221** are generally adapted to detect physiological sounds from a patient **201**, and can be any of the sensing elements described herein, such as piezoelectric membranes.

The patient sensor **215** can also include at least one acoustic coupler for acoustically coupling the first and second physiological signal acoustic sensing elements **220**, **221** to a patient's body **201**. In FIG. 2, both acoustic sensing elements **220**, **221** are acoustically coupled to the patient. As shown in FIG. 1C, the acoustic coupling can be achieved using a single acoustic coupler **212** for both sensing elements.

According to one configuration, the acoustic sensing elements **220**, **221** are supported in a stacked configuration on a sensor frame (not shown) or other support. Example stacked configurations are described below with respect to FIGS. 3B, 4A-4B and 6A-6B.

As shown in FIG. 2B, first and second acoustic couplers **213**, **214** can be used in alternative embodiments. The acoustic couplers **213**, **214** can be similar, for example, to the others described herein. In some embodiments, the acoustic sensing elements **220**, **221** are supported in a side-by-side configuration on a frame, similar to what is illustrated in FIG. 14 below (except that both sensing elements **220**, **221** are acoustically coupled to the body of the patient, whereas only one of the sensing elements **1420**, **1421** is coupled to the body in FIG. 14). In other embodiments, no acoustic coupler is included.

In some embodiments, the acoustic coupler, or couplers, **213**, **214** are designed to provide a substantially equal amount of coupling between each of the sensing elements **220**, **221** and the patient's body **201**, though this is not required. Example acoustic couplers compatible with the sensor **215** are described in greater detail throughout the disclosure.

As described, the first and second physiological signal acoustic sensing elements **220**, **221** can be specially adapted to detect physiological sounds from a patient. However, the signals output by the acoustic sensing elements **220**, **221** may also include noise (e.g., random noise, white Gaussian noise, etc.) from a variety of sources, which decreases the signal-to-noise ratio (SNR) of the signals.

The SNR of these signals can be improved, however, by collecting the desired physiological signal from more than one acoustic sensing element, and then combining (e.g., summing, subtracting, averaging, etc.) the respective outputs from the acoustic sensing elements in a manner that tends to reinforce the physiological signal components of the signals while tending to cancel or reduce the noise components of the signals. For example, the sensor **215**, monitor, or other intermediate component, can include a noise attenuator which performs the combining of the signals from the sensing elements **220**, **221** to achieve the improved SNR signal. Some embodiments of this approach are illustrated in FIGS. 3A-3B, 4A-4B and 6A-6B.

Generally, where sensors, sensing elements, couplers, etc., are described throughout the disclosure as being coupled to the patient's body, this may mean that one or more of the acoustic couplers are directly coupled to the patient's skin or other body part, such as where an acoustic coupler **212** is directly coupled to the skin **201** and transmits acoustic signals to one or more sensing elements **220**, **221** as shown in FIG. 2A. However, this is not necessarily the case. For example, in some embodiments, the entire sensor, including couplers, where used, and/or sensing elements may be spaced from the patient's body and still receive acoustic signals emanating from the patient.

FIG. 3A is a schematic illustration of an embodiment of a circuit for improving signal-to-noise ratio by combining physiological signals from two or more acoustic sensing elements **320**, **321**. The two acoustic sensing elements **320**,

321 may be acoustically coupled to the patient's body. In some embodiments, each of the first and second physiological signal acoustic sensing elements **320**, **321** is a piezoelectric film, each having an anode and a cathode. The acoustic sensing elements **320**, **321** detect physiological sounds from the patient's body and generate electrical waveforms corresponding to the physiological sounds. Example compatible piezoelectric films are described herein, with respect to FIGS. 4A-4B, 5A-5D, 6A-6B and 20A-20C, for example.

In FIG. 3A, the piezoelectric films **320**, **321** are configured so as to generate output signals where the physiological signal components are 180° or approximately 180° out of phase. For example, in FIG. 3, the acoustic sensing elements **320**, **321** generate voltage waveforms **330**, **331** in response to physiological sounds from the patient. In the figure, the voltage waveform **330** is a positive pulse, while the voltage waveform **331** is a negative pulse, 180° out of phase from the positive pulse **330**. Each of the physiological signal acoustic sensing elements **320**, **321** is communicatively coupled to a sensing circuit **340**. For example, the sensing circuit **340** may comprise or be referred to as a noise attenuator. Other example noise attenuators are described below with respect to FIGS. 7, 8, 9, and/or 17, for example. In the illustrated embodiment, the sensing circuit **340** is a difference amplifier, though other sensing circuits **340** can be used.

In some embodiments, the 180° phase shift between the outputs from the two piezoelectric films **320**, **321** is achieved by differentially connecting the piezoelectric films to the difference amplifier **340**. For example, the cathode **320b** of the first piezoelectric film **320** can be connected to the non-inverting terminal of the difference amplifier, while the anode **321a** of the second piezoelectric film **321** can be connected to the inverting terminal of the difference amplifier **340**. The anode **320a** and the cathode **321b** of the first and second films **320**, **321**, respectively, can be connected to ground (or be otherwise operatively coupled or coupled to a common potential). In some embodiments, the 180° phase shift is facilitated by mounting the two piezoelectric films **320**, **321** such that one is flipped with respect to the other. For example, the two piezoelectric films **320**, **321** can be mounted such that the cathode of one of the films faces toward the patient's body, while the anode of the other film faces toward the patient's body.

Since, in some embodiments, the physiological signal component of the second voltage waveform **331** is substantially a negative copy of the physiological signal component of the first voltage waveform **330**, when these two waveforms **330**, **331** are subtracted by the sensing circuit **340**, they combine constructively, as indicated by the output waveform **341** from the sensing circuit **340**. However, the outputs from the first and second piezoelectric films **320**, **321** may also each include a noise component (not illustrated in the waveforms **330**, **331**). If the noise in the outputs from the piezoelectric films is random or otherwise uncorrelated, then at least a portion of the noise will tend to be combined destructively by the sensing circuit **340**. Thus, the sensing circuit **340** can amplify the physiological signal component from the first and second piezoelectric films **320**, **321** while attenuating random noise. The result in certain embodiments is that the physiological signal is emphasized while the random noise component of the output signals from the piezoelectric films **320**, **321** is deemphasized.

For example, in one embodiment, the physiological signal is at least approximately doubled while the noise component is increased but less than doubled. The noise component

might not double due to the random or uncorrelated nature of the noise, resulting in some portions of the noise combining additively while others combine negatively. Because the increase in the physiological signal can be greater than the increase in the noise, the sensor assembly configuration shown in FIG. 3A can improve signal to noise ratio (SNR).

While the configuration of FIG. 3A shows sensing elements 320, 321 in a side-by-side configuration, other configurations are possible. For example, FIG. 3B illustrates an embodiment of a circuit for improving signal-to-noise ratio where the sensing elements 320, 321 are in a stacked configuration with respect to one another. As described in further detail below with respect to FIGS. 4A-5B, the first sensing element 320 may be wrapped around a frame, and the second sensing element 321 may be wrapped around the first sensing element 320 and the frame.

Similar to the sensor configuration of FIG. 3A, the cathode 320b of the first piezoelectric film 320 can be connected to the non-inverting terminal of the sensing circuit 340, while the anode 321a of the second piezoelectric film 321 can be connected to the inverting terminal of the sensing circuit 340. Thus, in the illustrated embodiment the inner electrodes 320b, 321a of the first and second sensing elements 320, 321 generally face one another in the stacked configuration. The inner electrodes 320b, 321a are shown connected to the terminals of the sensing circuit 340, while the outer electrodes 320a, 321b are connected to ground.

Depending on the embodiment, the configuration shown in FIG. 3B can provide similar improved SNR advantages as described above with respect to FIG. 3A. In addition, as described herein (e.g., with respect to FIGS. 4A-6B), such a configuration can also provide enhanced electrical shielding. For example, the outer electrodes 320a, 321b of the sensing elements 320, 321, respectively, can be used to shield the inner electrodes 320b, 321a from electrical noise. As used herein, the terms "shield," "shielding," and the like, in addition to having their ordinary meaning, can mean reducing or attenuating noise, rather than completely eliminating noise. However, in some embodiments, the terms "shield," "shielding," and the like can also mean completely eliminating noise.

Generally, a variety of different sensing circuits 340 can be used in the embodiments of FIGS. 3A-3B and in generally any of the embodiments described herein where appropriate. Moreover, depending on the sensing circuit 340 used, the electrodes can be connected in a number of arrangements to achieve a similar SNR improvement. For example, a similar result could be obtained by connecting either both anodes or both cathodes, of the piezoelectric films 320, 321 to the inputs of a summing amplifier instead of a sensing circuit. In such embodiments, the physiological signal components of the outputs from the piezoelectric films can be approximately in phase and, therefore, can combine constructively when added by the summing amplifier. Still, at least a portion of random noise from the two output signals from the piezoelectric films 320, 321 will combine destructively, thereby attenuating noise and improving SNR. In some embodiments, more than two physiological signal acoustic sensing elements are used, and their inputs are summed together by, for example, a summing amplifier, a digital signal processor, etc. In some embodiments, one or more of the outer electrodes 320a, 321b can be operatively coupled to the sensing circuit 340, and one or more of the inner electrodes 320b, 321a are connected to ground. In yet other embodiments, the sensing circuit 340 comprises a coupling junction coupling together one or more of the electrodes of the respective sensing elements 320, 321.

Moreover, the number and arrangement of the sensing elements 320, 321 can vary according to certain aspects. For example, in some embodiments, more than two physiological signal acoustic sensing elements 320, 321 are used, and their inputs are summed together by, for example, a summing amplifier, a digital signal processor, etc. A variety of configurations including more than two sensing elements are possible. For example, in one embodiment a pair of stacked sensing elements is arranged in a side-by-side configuration on a frame with respect to another pair of stacked sensing elements. In other embodiments, more than two sensing elements (e.g., 3, 4, 5 or more) are arranged in a stacked configuration. In yet other embodiments, more than two sensing elements (e.g., 3, 4, 5 or more) are arranged side-by-side with respect to one another.

FIG. 4A is a cross-sectional schematic drawing of an embodiment of an acoustic sensor 415 that includes first and second acoustic sensing elements 420, 421 in a stacked configuration. When connected to a sensing circuit (not shown, e.g., a difference amplifier) in the manner described above with respect to FIG. 3B, the acoustic sensor 415 can advantageously provide improved signal-to-noise ratio.

In the depicted embodiment, the first acoustic sensing element 420 is wrapped around a portion of the frame 418 and the second acoustic sensing element 421 is generally wrapped around the first acoustic sensing element 420 and also supported by the frame. In the illustrated embodiment, the physiological signal acoustic sensing elements 420, 421 are piezoelectric films. An acoustic coupler 414 acoustically couples the sensing elements 420, 421 to the patient's body 401, and can be aligned with both the first and second sensing elements 420, 421, as shown. In some other embodiments, an acoustic coupler 414 is not used. In the embodiment of FIG. 4A, the two piezoelectric films 420, 421 both extend over the acoustic cavity 436 of the frame 2118. Thus, the films 420, 421 are free to respond to acoustic waves incident upon them, resulting in induced voltages.

In the depicted embodiment, a PCB 422 is disposed in the upper cavity 438 of the frame 418, and is in electrical contact with one or more of the electrodes of the first and second sensing elements 420, 421. For example, the PCB 422 can be in electrical contact with the anode and cathode of each of the sensing elements 420, 421. While other configurations are possible, first and second ends 424, 426 of the first sensing element 420 can generally extend underneath opposite sides of the PCB 422. A first end 428 of the second sensing element 421 extends underneath the PCB 422, while a second end 430 of the second sensing element 421 extends over the opposing side of the PCB 422.

The upper side of the first ends 424, 428 of the first and second sensing elements 420, 422 can include contacts (not shown) corresponding to both electrodes of the respective sensing elements 420, 421. These contacts can be coupled to corresponding contacts on the underside of the PCB 422. One or more through holes or vias may be used to extend the electrodes on the underside of the ends 424, 428 of the sensing elements 420, 421 up to the upper side, enabling contact with appropriate PCB 422 contacts. Example first and second sensing elements compatible with the arrangement of FIG. 4 are described with respect to FIGS. 5A-6B. Additionally, another example piezoelectric membranes including through holes or vias are described below with respect to FIGS. 20A-20C.

While not shown for the purpose of clarity, in one embodiment, at least one additional layer (not shown) can be disposed between the sensing elements 420, 421. The additional layer can include an adhesive that adhesively couples

the sensing elements **420**, **421** together. This adhesive coupling can help ensure that the sensing elements **420**, **421** move uniformly together in response to vibrations, reducing losses and improving the response of the sensor. The adhesive coupling can also at least partially maintain tension of one or more of the sensing elements **420**, **421**.

The additional layer can further be configured to insulate the sensing elements **420**, **421** from one another, preventing shorts, noise and/or other undesirable electrical behavior. For example, the additional layer can include a dielectric material. In an embodiment, the adhesive described above acts as a dielectric material. Additional adhesive layers are described below with respect to FIGS. **6A-6B**, **19D-19E** and **6D-6E**, for example.

The ends of the sensing elements **420**, **422** may be configured to provide improved sensor performance, reliability, etc. For example, the additional layer may extend to the ends of one or more of the sensing element **420**, **422**. In one embodiment, the additional layer is an adhesive layer extending to the underside of the second end **430** of the second sensing element **420**, helping secure the connection between the second sensing element **422** and the PCB **422**. Moreover, in such embodiments, the second end **430** may be generally stretched across the top of the PCB **422**, biasing one or more of the sensing elements **420**, **421** in tension and thus providing an improved piezoelectric response.

Depending on the embodiment, one or more of the ends of the sensing elements **420**, **421** can also include a dielectric material. For example, in one embodiment, the underside of the second end **430** of the second sensing element **421** includes a dielectric material, thereby insulating the second end **430** and the PCB **422**. Additionally, the electrode coatings can be configured to reduce the possibility of electrical shorts or other undesirable behavior. In one embodiment, for example, the electrode coating on the underside of the second sensing element **421** does not extend to the second end **430**, thereby reducing the risk of undesirable electrical contact between the second end **430** and the top surface of the PCB **422**. In another embodiment, a dielectric material is placed on the underside of the PCB **422** instead of or in addition to providing a dielectric material on the end of the sensing element **420** or **421**.

A variety of other configurations are possible for the arrangement of the sensing elements **420**, **421**. For example, in one embodiment, the ends of the sensing elements **420**, **421** which are not connected to the PCB **422** do not extend over or under the PCB **422**. In another embodiment, each end of the sensing elements **420**, **421** includes one electrode contact, and all four ends are thus in electrical contact with corresponding contacts on the PCB **422**. This is in contrast with the arrangement described above, in which the upper side of the first ends **424**, **428** each include both anode and cathode electrode contacts for the respective sensing elements **420**, **421**.

As discussed, and as with many of the embodiments described herein, the piezoelectric films **420**, **421** are shown in FIG. **4A** spaced apart for clarity and ease of illustration. However, in addition to the additional layers described above, the two piezoelectric films **420**, **421** can be separated by one or more mechanical supports, acoustic decouplers, shielding layers, or other layers or components. Additionally, any of these layers may be disposed between the frame **418** and the first piezoelectric film **420** and/or wrapped around the outside of the second sensing element **421**.

Shielding Using Multiple Sensing Elements

In certain embodiments, multiple sensing elements can be employed to form an electrical noise shielding barrier,

providing electrical shielding. Moreover, using the sensing elements or portions thereof to form the barrier can simplify the design of the sensor, reducing costs. For example, one or more stacked sensing elements can be configured to electrically shield the sensor. In some configurations, where the stacked sensing elements are piezoelectric films, the inner, facing electrodes of the films in the stack are used to communicate voltage signals generated by the piezoelectric elements to the sensing circuitry of the sensor (and/or monitor). The outer electrodes of the films in the stack can advantageously be configured to shield the inner electrodes from electrical noise. Generally, throughout the disclosure, the term "inner" refers to the sensing element surface and/or electrode coating which is facing the other sensing element in the active region of the stack (e.g., across the acoustic cavity). Conversely, the term "outer" refers to the sensing element surface and/or electrode which is facing away from the other sensing element in the active region of the stack.

The electrical noise shielding barrier can electrically shield the electrical poles of the sensing element from external electrical noises. In some embodiments the outer portions of the sensing element form a Faraday cage or shield around the inner portions. Thus, the outer portions can distribute external electrical noise substantially equally to the electrical poles of the piezoelectric sensing element. The shield can act to reduce the effect of noise on the sensing element from sources such as external static electrical fields, electromagnetic fields, and the like.

Using a second sensing element to form an electrical shielding barrier can also help to reduce costs by reducing the complexity involved in constructing the sensor and reducing material costs. For example, such embodiments may not include one or more shielding layers which are physically separate from the sensing elements (e.g., copper shielding layers), reducing manufacturing costs associated with purchasing and handling such components. However, certain aspects of shielding barriers formed from multiple sensing elements described herein are compatible with shielding barriers formed from separate layers and aspects thereof. Example shielding barriers including those formed from separate shielding layers are described with respect to FIGS. **2D-2E** below and throughout the '939 application, including, without limitation, paragraphs [0120]-[0146] and FIGS. **2D-2E** of the '939 application which are incorporated by reference herein.

FIG. **4B** shows a partial cross-sectional schematic drawing of a portion **440** of the first and second stacked piezoelectric films **420**, **421** of FIG. **4A**. As shown, each of the first and second piezoelectric films **420**, **421** respectively include an anode **420a**, **421a** and a cathode **420b**, **421b** on opposing sides of the films **420**, **421**. In some embodiments, the films **420**, **421** include one of the piezoelectric films described with respect to FIG. **2B-E** or **3A-C**, for example.

As shown, the films **420**, **421** are disposed with respect to each other in a stacked configuration such that the cathode **420b** of the first film **420** is facing the anode **421a** of the second film **421**. Thus, these two inner electrodes **420b**, **421a** of the stack are generally sandwiched between the anode **420a** of the first film **420** and the cathode **421b** of the second film **421**, which form the outer electrodes of the stack. The inner electrodes **420b**, **421a** can be operationally coupled to a sensing circuit (e.g., a differential amplifier) in the manner shown in FIG. **20B**, advantageously providing improved signal-to-noise-ratio in some embodiments.

In addition, the outer electrodes **420a**, **421b** of the films **420**, **421** can be configured to form layers of an electrical noise shielding barrier, providing the additional benefit of

electrically shielding the sensor from external electrical noises. The electrical noises shielded (or at least partially shielded) can include electromagnetic interference (EMI) from various sources, such as 50 or 60 Hz (AC) noise, noise from other medical devices, and so forth. In some embodiments for example, the outer electrodes **420a**, **421b** of the first and second films **420**, **421** form a barrier around the inner electrodes **420b**, **421a** of the first and second films **420**, **421**. Thus, a significant amount of external electrical noise is not directly incident on the inner electrodes **420b**, **421a**. The outer electrodes **420a**, **421b** can, for example, distribute at least a portion of the external electrical noise substantially equally to the inner electrodes **420b**, **421a**, which form the electrical poles of the sensor. For example, because the outer electrodes **420a**, **421b** may share a common potential (e.g., ground), noise incident on either of the outer electrodes **420a**, **421b** can be distributed equally to each electrode **420a**, **421b**. The equally distributed noise can then be capacitively coupled to the inner electrodes **420b**, **421a**.

Thus, in certain embodiments, because the noise is equally distributed, the noise signal components on the inner electrodes **420b**, **421a** will be substantially in phase. The physiological signal components can be substantially out of phase, on the other hand, due to the differential orientation of the inner electrodes **420b**, **421a** with respect to one another in some implementations. The noise signals can advantageously be removed or substantially removed, such as through a common-mode rejection technique as described herein. In certain embodiments, at least some of the external electrical noise is shunted or otherwise directed to ground instead of, or in addition to, being equally distributed to the inner electrodes **420b**, **421a**.

A variety of alternative configurations are possible. For example, more than two sensing elements (e.g., 2, 3, 4, 5 or more) may be arranged to provide electrical shielding and/or improved signal-to-noise ratio in some embodiments. Moreover, the particular polarities of the sensing elements **420**, **421** of FIG. 4 are not intended to be limiting. In another embodiment, one or more of the sensing elements **420**, **421** are flipped. For example, the sensing elements **420**, **421** are flipped such that the anode **420a** of the first sensing element **420** faces the cathode **421b** of the second sensing element **421**.

Additionally, shielding barriers formed using stacked sensing elements **420**, **421** can provide improved coupling of bodily sounds to the sensor, improving sensor operation (e.g., sensor sensitivity, measurement reliability, etc.). Generally, portions of both the shielding barrier and the sensing element will tend to vibrate in response to the patient sounds. Thus, an uneven mechanical response between the shielding barrier and the sensing element may result in lost signal, affecting sensor performance. For example, shielding barriers including layers that are physically separate from the sensing element can be, in some cases, relatively stiffer than the sensing element. This can limit movement of the sensing element in response to vibrations, producing a corresponding limiting affect on sensor sensitivity. In contrast, where electrodes of the sensing elements are used as shielding layers, the shielding barrier and the sensing element are generally formed from the same type material and integrally connected. Thus, the sensor may be relatively more responsive to vibrations, improving sensor operation.

Moreover, each of the outer electrode shield layers in the stacked configuration can be evenly spaced from the respective inner electrode sensor poles, particularly across the mechanically active portions of the sensor (e.g., across the frame cavity **436** of FIG. 4A). The capacitance between the

shield layer and sensor pole on a first side of the sensing element stack can be very highly matched (e.g., substantially equal to) with the capacitance between the shield layer and sensor pole on the opposing side of the stack. Thus, a stacked sensing element configuration can provide a more even distribution of external electrical noise to the poles of the sensing element, improving noise rejection.

According to certain aspects, the physical configuration of the electrodes of the first and second films **420**, **421** can be tailored to provide improved electrical shielding. For example, the outer electrodes **420b**, **421a** can be plated using a material selected to provide enhanced shielding. Although other materials may be used, in one embodiment, the outer electrodes **420b**, **421a** are plated with silver ink. Moreover, in certain embodiments, the outer electrode coatings of the piezoelectric stack cover a greater portion of the surface area of the respective piezoelectric films than the inner electrode coatings. For example, the outer electrode coatings may cover a significantly larger portion of the surface area of the respective piezoelectric films than the inner electrode coatings. In certain embodiments, for example, the outer electrodes generally envelope or surround the inner electrodes or a substantial portion thereof when the films **420**, **421** are in a stacked configuration. Thus, the amount of surface area of the inner electrodes which is exposed to electrical noise is reduced due to the mechanical and/or electrical barrier created by the surrounding outer electrodes.

FIGS. 5A-5D illustrate example sensing elements **520**, **521** having electrode coating configurations tailored for use in a stacked configuration. FIGS. 5A-5B show example first and second (e.g., inner and outer) surfaces **524**, **526** of a first example acoustic sensing element **520**. FIGS. 5C-5D show example first and second (e.g., inner and outer) surfaces **528**, **530** of a second acoustic sensing element **521**. While the films **520**, **521** are shown in an unfolded configuration for the ease of illustration, the second sensing element **521** may be wrapped around the first sensing element **520** on a frame as shown in FIGS. 4A-4B. Thus, the sensing elements **520**, **521** are also referred to as the interior and exterior sensing elements, respectively.

The interior sensing element **520** includes an anode electrode coating **520a** on the outer surface **526** which extends via a through hole **532** to a portion on one end of the inner surface **524**. The inner surface **524** of the first sensing element **520** also includes a cathode coating **520b**. The exterior sensing element **521** includes an anode electrode coating **521a** on the inner surface **528** which extends via a through hole **534** to a portion on one end of the outer surface **530**. The outer surface of the exterior sensing element **521** also includes a cathode electrode coating **521b**.

As shown in FIG. 5B, the outer electrode surface of the first (interior) film **520** covers a substantially greater percentage of the surface area of the outer surface **526** of the film **520** than do the inner electrode surfaces on the opposing, inner surface **524** of the film **520**, shown in FIG. 5A. For example, in the illustrated embodiment, the outer electrode coating shown on FIG. 5B covers substantially the entire outer surface **526** area of the film **520**, while the electrode coatings on the inner surface **524** form a pair of generally rectangular strips covering only a portion of the inner surface **524** area of the film **520**. Similarly, as shown in FIGS. 5C-D, the outer electrode coatings on the outer surface **530** of the second (exterior) film **521** covers a substantially greater surface area of the outer surface **530** of film **521** than the inner electrode coating on the inner surface **528** of the film **521**. For example, in certain embodiments, the electrode coating on the exterior surface of one or more

of the films **520**, **521** covers at least 2 percent more of the film surface area than the do the interior electrodes. In other embodiments, the exterior electrodes cover at least 1, 5, 10, 15 or greater percent more of the exterior surface area than the do the interior electrodes. Additionally, the exterior electrode can cover at least 90 percent of the exterior film surface in some embodiments. In other embodiments, the exterior electrode covers at least 70, 75, 80, 85, 95 or more percent of the exterior film surface.

As described with respect to FIGS. **4A-4B**, the through holes **532**, **534** facilitate electrical contact between the respective electrodes and one or more components of the sensor (e.g., a PCB contact). Moreover, the electrode which is extended to the opposing side through the at least one through hole **540** can be electrically isolated from the other electrode on the respective film the by gaps **536**, **538** in the electrode coatings.

In such embodiments, where an electrode coating covers substantially the entire surface area of the piezoelectric film, or otherwise covers a significantly larger portion of the surface area of the piezoelectric film than the electrode coating on the opposing side, the electrode coating may be referred to as "flooded." Thus, the configuration of FIG. **5** generally includes un-flooded inner electrodes generally sandwiched between flooded outer electrodes. Such configurations can reduce surface area of the inner electrodes that is exposed to electrical noise, improving electrical shielding.

A wide variety of flooded electrode configurations are possible. For example, in some embodiments, the sizes and shapes of the electrode coatings may differ from the illustrated embodiment. The relative sizes of the inner electrode coatings versus the outer electrode coatings can also vary. For example, the inner electrode coatings are much smaller in relation to the outer electrode coatings than is shown.

In some alternative embodiments, the outer and inner electrode coatings are both flooded or otherwise cover about the same surface area, or the electrode coating on the inner electrode coating covers more surface area than the outer electrode. Such embodiments may, in some cases, provide relatively less shielding than embodiments where the outer electrode coatings cover more surface area than the inner electrodes, but nonetheless provide some significant amount of electrical shielding.

Example Sensor

FIGS. **6A-6B** illustrate an exploded view of an example sensor **600** configured to detect acoustic physiological sounds from the patient incorporating certain beneficial aspects described herein. For example, the sensor **600** provides improved SNR using multiple sensing elements according to techniques described above with respect to FIGS. **2A-4B**. Moreover, the sensor **600** includes a stacked, multiple sensing element configuration providing enhanced shielding, compatible with the techniques described above with respect to FIGS. **4A-5D**.

The sensor **600** is generally attachable to a patient and can be coupled to a patient monitor. For example, the sensor **600** can be used with the system **10** of FIGS. **1A-1B**. Additionally, the sensor **600** may be compatible with the sensor system **100** of FIG. **1C**. For example, the sensor **600** may be the sensor **101** of FIG. **1C**, and can include an attachment mechanism (not shown) for attaching the sensor to a patient, such as the attachment subassembly **104** of FIG. **1C**.

Referring to FIG. **6A**, the sensor **600** of certain embodiments includes an acoustic coupler shell **602**, a printed circuit board (PCB) **604**, a frame **606**, first and second acoustic sensing elements **620**, **621**, and multiple adhesive layers **608**, **610**, **612**. The coupler shell **602** houses the frame

606, which is generally configured to support various components of the sensor **600** in an assembled state, including the PCB **604**, sensing elements **620**, **621**, and adhesive layers **608**, **610**, **612**. The sensing elements **620**, **621** are piezoelectric films in the illustrated embodiment, although other types of sensing elements can be used.

The components of the sensor **600** can be assembled similarly to the sensor **415** of FIG. **4A**. For example, the first piezoelectric film **620** is wrapped around a portion of the frame **606** and extends across an acoustic cavity **614** (FIG. **6B**) of the frame **606** in tension. When assembled, the adhesive portions **608**, **610** are positioned between interior opposing sides of the first film **620** and corresponding sides of the sensor frame **606**, thereby adhering the first film **620** in place with respect to the frame **606**.

The adhesive layer **612** is wrapped around the first sensing element **621**, and the second sensing element **621** is in turn wrapped around the adhesive layer **612**, generally forming a piezoelectric stack. As discussed with respect to FIG. **4A**, the active portions of the films **620**, **621** that extend across the acoustic cavity **614** are thus generally free to move in response to received vibrations, enabling detection of a physiological signal when the sensor **600** is attached to the patient. In certain embodiments, the acoustic cavity **614** or a portion thereof extends all the way through the frame **606**. For example, the cavity may form one or more holes in the interior portion of the frame **606**.

The PCB **604** is positioned in the cavity **616** (FIG. **6A**) such that the underside of the PCB **604** comes into contact with the regions **617**, **618** of the second film **621** and the regions **622**, **624** of the first film **620**. The flap **626** of the second film **621** rests on top of the PCB **604** in the illustrated embodiment, allowing electrical coupling of the first sensing element **620** to the PCB **604** and associated circuitry.

The coupler shell **602** is generally configured to transmit vibrations received from the patient to the films **620**, **621** in the piezoelectric stack. The acoustic coupler **602** can include a lower protrusion or bump **628** (FIG. **6B**) configured to press against the patient's body when the acoustic sensor **600** is fastened into place on the patient. The acoustic coupler **602** can also include a protrusion **630** (FIG. **6A**) designed to abut against the films **620**, **621** and to bias them in tension across the acoustic cavity **614**. The coupler shell **602** can be similar to any of the acoustic couplers described herein, such as those described below with respect to FIGS. **19A-19E**, **21**, and **22A-22B**.

Generally, the piezoelectric films **620**, **621** can be any of those described herein. In the illustrated embodiment, for example, the films **620**, **621** are the piezoelectric films described in FIGS. **5A-5D** having flooded electrode surfaces **632**, **644**, respectively, which form the outer surfaces of the piezoelectric stack. Moreover, the films **620**, **621** include one or more vias or through holes extending an electrode from one surface of the film **620**, **621** to a corresponding region **622**, **617** on the opposing surface of the respective film **620**, **621**. As discussed above, this configuration enables coupling of the four electrodes (e.g., the anode and cathode for each film **620**, **621**) to the appropriate contacts on the underside of the PCB **222**.

For example, in one embodiment, the region **618** (FIG. **6A**) of the flooded cathode coating on the outer surface of the second film **621** touches one or more of the contacts **636** on the underside of the PCB **604** (FIG. **6B**). Meanwhile, the through-holed region **617** (FIG. **6A**) of the outer surface of the second film **621**, which includes an anode coating, touches the contact **638** on the underside of the PCB **604** (FIG. **6B**). Regarding the first film **620**, the region **624** (FIG.

6A) of the cathode coating on the inner surface touches one or more of the contacts **640** on the underside of the PCB **604** (FIG. 6B). Meanwhile, the through-holed region **622** (FIG. 6A) of the inner surface of the first film **620**, which includes an anode coating, touches one or more of the contacts **642** on the underside of the PCB **604** (FIG. 6B).

According to the above-described connection scheme, the films **620**, **621** can be coupled to circuitry (not shown) residing on the PCB **222** or other system component (e.g., the hub or monitor) to provide improved SNR and/or electrical shielding. For example, the electrodes of the films **620**, **621** can each be coupled to an input of an attenuation circuit (e.g., a differential amplifier) or ground (or other common potential) in the manner illustrated schematically with respect to FIG. 3B above. Specifically, although other connections schemes are possible, in one embodiment, the contact **636** on the PCB **604** couples the flooded, outer cathode of the second, exterior film **621** to ground, and the contact **642** couples the outer, flooded anode of the first, interior film **620** to ground. Moreover, the contacts **642** couple the inner, un-flooded anode of the second, exterior film **621** to a first (e.g., positive) terminal of a difference amplifier or other noise attenuation circuit. Finally, the contacts **638** couple the un-flooded, inner cathode of the first, interior film **620** to a second (e.g., negative) terminal of the difference amplifier.

The frame **606** can include one or more pressure equalization pathways **650**. The pressure equalization pathways **650** provide an air communication pathway between the lower acoustic cavity **614** and ambient air pressure. The pressure equalization pathways **650** allow the sensor's membrane(s) or film(s) **621**, **622** to vibrate within the cavity **614** independent of skin elasticity or the force used to attach the sensor to a patient's skin.

Indeed, variability in skin elasticity or the force used to attach the acoustic sensor to the medical patient's skin can affect the volume and/or air pressure within the cavity **614** defined by the sensing elements **621**, **622** and frame **606**. Variability in skin elasticity or attachment force can lead to variability in cavity resonance, which can cause unwanted variability in sensor **600** performance. For example, an acoustic sensor **600** that is attached to very elastic skin may provide a different output signal than an acoustic sensor **600** that is attached to firmer or tighter skin. Similarly, an acoustic sensor **600** that is loosely attached to patient's skin may provide a different output signal than an acoustic sensor **600** that is tightly attached to a patient's skin.

To compensate for attachment variability, in one embodiment the acoustic sensor frame **606** includes one or more pressure equalization pathways **650**. The pathways **650** provide an air-flow channel from the cavity **614** to the ambient air pressure. By equalizing pressure within the cavity **614** with ambient during sensing, variability in sensor performance may be reduced and/or eliminated. In some embodiments, the pressure equalization pathways **650** include one or more holes, notches, ports, or channels that extend from within the sensor's cavity **614** to a location in communication with ambient air pressure.

In one embodiment, the pressure equalization pathways **650** are provided on opposite sides of the frame **606** portion that defines an acoustic cavity **614**. Symmetrically arranging the pressure equalization pathways **650** can further improve sensor **600** performance. In another embodiment the pressure equalization pathways **650** are provided in portions of the sensor frame **606** which do not contact the sensor's sensing elements, membranes, and/or films **621**, **622**. By preventing contact between the pressure equalization path-

ways **650** and the sensor's sensing membrane, sensor **600** performance may be further improved.

In one embodiment, the sensor frame **606** includes one, two, three, four, or five pressure equalization pathways **650** on each of two opposite sides of the sensor frame **606**. In another embodiment, the sensor frame **606** includes at least one pressure equalization pathway **650** on each of its sides. In one embodiment, each pressure equalization pathway **650** is formed as a notch. A frame **606** that includes notches as its pressure equalization pathways **650** may be easier to fabricate than a frame that includes other pressure equalization pathways **650** (e.g., holes). For example, when the frame **606** is made by molding plastic, creating notches in the frame's **606** side wall requires less complicated tooling than forming holes.

Aspects of some of the components of the sensor **600** are described in greater detail herein with respect to other embodiments. For example, one or more of the coupling shell **602**, PCB **604**, frame **606**, sensing elements **620**, **621**, adhesive layers **608**, **610**, **612**, or portions or aspects thereof are compatible with the corresponding components shown in FIGS. 19A-23E and described in the accompanying text.

Noise Compensation Overview

Embodiments of systems generally including at least first and second acoustic sensing elements and configured to provide noise compensation will now be described with respect to FIGS. 7-18. As will be described, according to some aspects, one of the sensing elements is used as a physiological signal sensing element, and another is used as a noise sensing element for generating a noise reference signal. The noise reference signal can be used to generate a physiological signal have a reduced noise component according to a variety of techniques described in further detail herein (e.g., adaptive filtering techniques). Moreover, according yet other embodiments, the sensing elements are selectively configurable for use as either physiological signal sensing elements or noise sensing elements, as desired, as described in further detail herein.

According to various aspects, the multiple acoustic sensing elements can be beneficially arranged in a variety of configurations. For example, the first and second sensing elements can be incorporated into the same sensor package, as shown in the embodiments illustrated in FIGS. 8 and 10-15. In some embodiments, the first and second sensing elements are included in separate sensor packages, or can otherwise be strategically positioned at a variety of locations in the monitoring environment. For example, such sensors can be positioned at multiple locations on the patient, as is shown in and described with respect to FIG. 9A. Moreover, one or more sensing elements can be positioned at the physiological monitor or some other appropriate location in monitoring environment, as is disclosed in FIG. 9B and the accompanying text.

Generally speaking, the interfering noise signals described herein (e.g., with respect to FIGS. 7-18) can include any acoustic signal, and can include vibrational, sonic, infrasonic, or ultrasonic waves. Such signals can be transmitted in gases, liquids and/or solids. For example, depending on the physiological signal being monitored, the interfering noise can include patient sounds generated from physiological processes, such as breathing sounds, heart sounds, digestive sounds, combinations of the same and the like. Interfering noise can further include speech sounds, snoring, coughing, gasping, etc., and can emanate from the patient or other individuals in the monitoring environment. Further sources of noise can also include humming or other acoustic noise coming from computers or other electronic

equipment in the operating environment, ambient traffic or airplane noise, combinations thereof and the like.

Interfering noise can additionally emanate from one or more noisy devices that are coupled to the patient, such as medical devices that are coupled to the patient during use. Examples of such devices can include, without limitation, powered surgical equipment (e.g., electrosurgical tools for cauterizing, coagulating, welding, cutting, etc.), ventilation equipment (e.g., continuous positive airway pressure (CPAP) machines), nebulizers, combinations of the same and the like.

Particularly where a noise source is readily identifiable, the noise sensing element according to certain aspects may be positioned in physical proximity to the noise source, so as to obtain a signal including a relatively clean noise reference signal, allowing for improved noise compensation according to techniques described herein. Specific example cases are provided below with respect to FIGS. 9A-9B, for example.

According to yet other described embodiments, it can be expected that the components of their output signals resulting from one source (e.g., the patient's body) will be generally similar while signal components from other sources (e.g., noise components) can be expected to have certain dissimilarities (e.g., phase or time shift). In these cases, the output signals from the first and second acoustic sensing elements can be advantageously combined in ways that accentuate commonalities between the two signals while attenuating differences between the two output signals, or vice versa, producing a reduced noise output signal.

Moreover, while shown and described as first and second sensing elements with respect to many of the embodiments described below, there may be more than two (e.g., 3, 4, 5 or more) sensing elements in certain embodiments. Additionally, while described as individual sensing elements for the purposes of illustration, in certain embodiments one or more of the first and second sensing elements each include multiple acoustic transducers or other types of sensing elements. In some embodiments, for example, the first and/or second sensing elements each include at least two piezoelectric films arranged in a stacked configuration, wrapped around a support frame, as described above with respect to FIGS. 3B-4B and 6A-6B.

FIG. 7 is a block diagram of an embodiment of an acoustic physiological monitoring system 700 having noise compensation features. The noise compensation features can be useful for reducing any deleterious effect of acoustic noise on the accuracy of physiological characteristics determined using the monitoring system 700.

The acoustic physiological monitoring system 700 includes a first acoustic sensing element 720 and a second acoustic sensing element 721. In some embodiments, these acoustic sensing elements are passive devices. In some embodiments, the first acoustic sensing element 720 is used to produce a physiological signal 730 that is indicative of one or more physiological sounds (e.g., sounds resulting from physiological processes) emanating from a patient's body. For example, the first acoustic sensing element 720 may be used to produce a physiological signal 730 that is indicative of a particular type of physiological sound, which is sometimes referred to herein as the target physiological sound. A variety of target physiological sounds are possible, including breathing sounds, heart sounds, digestive sounds, and the like. For example, the sensing elements 720, 721 can be piezoelectric films. In general, this physiological signal 730 can include unwanted noise as a result of interfering noise in the patient's surroundings being picked up by the

first acoustic sensing element 720. The physiological component and the noise component of the signal 730 can overlap in time and/or frequency content. Devices for detecting primarily physiological sounds emanating from the patient's body are disclosed more fully herein.

In some embodiments, the second acoustic sensing element 721 is used to produce a noise signal that is substantially representative of, or otherwise meaningfully correlated with, any noise picked up by the first acoustic sensing element 720. The noise signal 731 may not necessarily duplicate the noise component of the physiological signal 730. For example, the signal strength of the noise in the two signals 730, 731 can differ. Other differences between the noise signal 731 and the noise component of the physiological signal 730 are also possible. However, it can be advantageous for the second acoustic sensing element to be positioned and designed such that the noise signal 731 has some degree of commonality with the noise present in the physiological signal 730. In this way, the noise signal 731 can provide useful information to meaningfully reduce, remove, filter, cancel, separate out, etc. the noise from the physiological signal 730. Devices for detecting primarily noise sounds are disclosed more fully herein.

In addition, the second acoustic sensing element 721 can also be positioned and designed such that the noise signal 731 is substantially free of the physiological sounds picked up by the first acoustic sensing element 720, or such that such physiological sounds are a less-significant component of the noise signal 731 than they are of the physiological signal 730. While illustrated as producing a noise signal 731, in other embodiments discussed more fully herein the second acoustic sensing element is positioned and designed to provide a second physiological signal rather than a noise reference signal. For example, like the first sensing element 720, the second acoustic sensing element 721 may include both a significant physiological signal component and an interfering noise component. In such embodiments, the first and second physiological signals can be combined in certain ways so as to reinforce the physiological components of the two signals while reducing any noise components that can exist in the two physiological components. In other embodiments, this can be carried out using more than two acoustic sensing elements.

In some embodiments, the physiological signal mixed with noise 730 and the noise signal 731 are input to a processing unit 790. In some embodiments, the processing unit 790 includes a noise attenuator 740, a signal quality calculator 750, and a physiological characteristic calculator 760. The processing unit 790 can be implemented as one or more digital signal processors, one or more analog electric processing components, combinations of the same or the like, etc.

In some embodiments, the noise attenuator 740 reduces the amount of noise present in the physiological signal 730 based on information gleaned from the noise signal 731, as discussed in more detail herein. For example, the noise attenuator 740 can reduce the signal energy of the noise component of the physiological signal 730. Alternatively, or in addition, the noise attenuator 740 can reduce or remove a portion of the noise component of the physiological signal 730 over a particular frequency range. In some embodiments, the processing unit 790 outputs a physiological signal with reduced noise 741 using the noise attenuator 740. The signal 741 can also be provided to other sub-blocks of the processing unit 790 (e.g., the physiological characteristic calculator 760).

The signal quality calculator **750** is a device that is used to determine, for example, an objective indicator of the quality of the physiological information obtained from one or more acoustic sensing elements. This can be done, for example, by comparing the physiological signal **730** with the noise signal **731**, as discussed further herein. The signal quality calculator **750** can also output an objective indicator of the degree of confidence in the accuracy of a physiological characteristic (e.g., respiratory rate) determined based on the physiological information collected from one or more acoustic sensors. The signal quality calculator **750** can also output a binary confidence indicator that selectively indicates low confidence and/or high confidence in the accuracy of the physiological characteristic. The processing unit **790** then outputs one or more signal quality indicators **751**.

The physiological characteristic calculator **760** is used to determine, for example, one or more values or signals that are indicative of a physiological characteristic of the patient. For example, the physiological characteristic can be respiratory rate, expiratory flow, tidal volume, minute volume, apnea duration, breath sounds, riles, ronchi, stridor, and changes in breath sounds such as decreased volume or change in airflow. In some embodiments, a physiological characteristic is calculated using a processing algorithm applied to the physiological signal with reduced noise **741** that is outputted by the noise attenuator **740**.

The physiological signal with reduced noise **741**, the signal quality indicator **751**, and the physiological characteristic indicator can be output to a display and/or speaker **780** to be viewed or heard by a caregiver. For example, in some embodiments, the physiological signal with reduced noise **741** is converted back to an audible sound by way of a speaker or other acoustic transducer so that it can be heard by a doctor and used for diagnosis of the patient. In some embodiments, the signal quality indicator **751** and the physiological characteristic indicator **761** are displayed on a screen. This information can take the form of a numerical value, a plotted signal, an icon, etc.

Although both the noise attenuator **740** and the signal quality calculator **750** are included in the example processing unit **790** shown, the processing unit **790** could include either the noise attenuator **740** or the signal quality calculator **750** in some embodiments.

In various embodiments, the first and second acoustic sensing elements **720**, **721** can be either the same or different types of acoustic sensing elements. For example, in one embodiment, both of the sensing elements are piezoelectric films such as any of the films described herein. In such a configuration, each of the sensing elements **720**, **721** may be housed in a separate sensor packaging. As an example where different types of sensing elements are used, the first sensing element **720** in one embodiment is a piezoelectric film, while the second sensing element is a microphone, vibrational sensor or other type of acoustic pickup device. Such an embodiment is described with respect to FIG. **15** below.

Additionally, the sensing elements **720**, **721** may be physically separate from one another. For example, the sensing elements **720**, **721** can be physically separated within a single wearable sensor package. In other embodiments, the first sensing element **720** may be located on a wearable sensor package, such as any of those described herein, while the second sensing element **721** may be located at some other location, such as, for example, on a cable, hub, monitor, or in another wearable sensor package at a different location on the patient, etc. Further embodiments of sensors including physically separate sensing elements are discussed herein, with respect to FIGS. **8-9B**, for example.

While embodiments described herein advantageously employ multiple sensing elements to achieve noise compensation, in certain embodiments, noise compensation is achieved using a single sensing element. For example, the sensing element may be coupled to the patient and thus produce a signal including both physiological and noise components. However, in such embodiments, the noise reference signal may be extracted during periods when the physiological signal is inactive (e.g., in between patient breaths, heart beats, etc.). The extracted reference signal can then be used in accordance with techniques described herein to provide noise compensation.

FIG. **8** is a block diagram of an embodiment of an acoustic physiological monitoring system **800** with a wearable acoustic sensor **815** that includes first and second acoustic sensing elements **820**, **821**. The first and second acoustic sensing elements **820**, **821** are, for example, transducers for converting sound waves into some other form of energy (e.g., electrical voltage or current signals) to be processed, measured, etc. The first and second acoustic sensing elements **820**, **821** can be packaged in a common housing as shown in FIG. **8**, or in separate housings, as shown in FIG. **9A**, described below. In some embodiments, the first and second acoustic sensing elements **820**, **821** are both the same type of acoustic transducer. For example, in some embodiments, the first and second acoustic sensing elements **820**, **821** are both piezoelectric films.

Even in cases where the first and second acoustic sensing elements **820**, **821** are generally the same type of acoustic transducer, they need not be identical. For example, in the case where both of the first and second acoustic sensing elements **820**, **821** are piezoelectric films, the material properties of the two films can be separately adapted based on known characteristics of the aural signals they are intended to sense. The first and second acoustic sensing elements **820**, **821** can be made of different piezoelectric materials, they can have different shapes and thicknesses, they can have different support/mounting structures, and they can have different packaging. For example, in a given application (e.g., a medical sensing application), system designers can have foreknowledge regarding the characteristics of the sought-after acoustic signals.

As described herein, in some embodiments, the first acoustic sensing element **820** is used to primarily sense physiological signals, while the second acoustic sensing element **821** is used primarily to sense noise. In such cases, the type of piezoelectric material, and its shape, thickness, its mounting and packaging, etc. can be adapted for each of the acoustic sensing elements **820**, **821** based on unique characteristics (e.g., frequency range, amplitude, etc.) of the physiological signals and the expected noise, respectively, if such unique characteristics exist and are identifiable.

In other embodiments, it is advantageous for the properties (e.g., material properties, mounting, packaging, etc.) of the first and second acoustic sensing elements **820**, **821** to be substantially similar or even identical. This can be the case, for example, where the acoustic signals to be sensed by the two acoustic sensing elements **820**, **821** have no important pre-identifiable differing characteristics.

It can also be advantageous for the first and second acoustic sensing elements **820**, **821** to be substantially similar or even identical in terms of material properties, mounting, and packaging so that their signal outputs will likewise have shared characteristics in response to excitation of the acoustic sensing elements by a common source. This can be the case where the outputs of the first and second acoustic sensing elements **820**, **821** are to be combined using

techniques for selecting or rejecting signal components from the two sensing element outputs based on their common or distinguishing features. Examples of such techniques are described in further detail herein.

In other embodiments, the first and second acoustic sensing elements **820**, **821** are different types of acoustic transducers. For example, the first and second acoustic sensing elements **820**, **821** can be independently selected from a group including, but not limited to, piezoelectric acoustic transducers, condenser acoustic transducers, MEMS acoustic transducers, and electromagnetic induction acoustic transducers. Other types of acoustic transducers can also be used.

The first and second acoustic sensing elements **820**, **821** can exhibit directionality or not. In cases where both of the first and second acoustic sensing elements **820**, **821** exhibit directionality, they can be aimed at a common location (e.g., the patient's skin) or a different location (e.g., the first acoustic sensing element **820** could be aimed at the patient's skin to detect physiological sounds, while the second acoustic sensing element could be directed away from the patient's skin so as to detect ambient noise). In addition, in some embodiments, one of the acoustic sensing elements can exhibit directionality while the other does not. For example, in some embodiments the first acoustic sensing element **820** can exhibit directionality and be aimed at the patient's skin for detecting physiological sounds, while the second acoustic sensing element **821** does not exhibit directionality so as to detect noise from all directions.

As described herein (e.g., with respect to acoustic sensor **201**), the acoustic sensor **815** can include a cable **806**, or other communication link, for communicating with a physiological monitor **807**. For example, one or more connectors, hubs, or other cables may be included as described herein. The acoustic sensor can also include one or more devices (e.g., electrical circuits) for detecting, processing, and transmitting the outputs from the first and second acoustic sensing elements **820**, **821**. The sensor can also include a fastener for fastening the sensor to the body of a patient. In some embodiments, the fastener is specially adapted to attach to the patient's neck or chest region in order to sense breathing sounds. The acoustic sensor **815** can also include other features described with respect to acoustic sensor **201**.

In some embodiments, the acoustic sensor **815** is adapted to be communicatively coupled with a separate physiological monitor **807** that is not worn by the patient **801**. (The physiological monitor **807** can include, for example, a display **880**, a physiological characteristic calculator **860**, a noise attenuator **840**, a speaker **881**, and a signal quality calculator **850**, as described herein.) Thus, in some embodiments, the first and second acoustic sensing elements **820**, **821** are disposed on or in an acoustic sensor **815** that is adapted to be worn by the patient **801**, while the signal outputs from the first and second acoustic sensing elements **820**, **821**, which can include the raw signals directly from the acoustic sensing elements **820**, **821** as well as processed signals derived therefrom, are transmitted to a separate physiological monitor **807** that is not worn by the patient **801**. In other embodiments, however, the acoustic sensor **815** and the physiological monitor **807** can both be wearable by the patient **801**.

As discussed herein, in some embodiments the first acoustic sensing element **820** is designed and used primarily to sense an acoustic physiological signal emanating from a patient's body, while the second acoustic sensing element **821** is used primarily to sense the acoustic noise. The first acoustic sensing element **820** can, however, also detect

acoustic noise. In this case, the noise signal from the second acoustic sensing element **821** can be used as a noise reference to yield information that can be used to reduce or remove the presence of the acoustic noise from the physiological signal at the output of the first acoustic sensing element **820**.

In cases where the second acoustic sensing element **821** is used to produce a noise reference signal, it can be advantageous for the first and second acoustic sensing elements **820**, **821** to be designed and positioned with respect to one another such that the noise reference signal produced by the second acoustic sensing element **821** shares one or more characteristics with the noise component of the physiological signal output by the first acoustic sensing element. For example, the noise reference signal can be meaningfully correlated with the noise component of the physiological signal. In some embodiments, the noise reference signal from the second acoustic sensing element **821** and the noise component of the physiological signal from the first acoustic sensing element **820** are related by, for example, a scalar factor, a time shift, a phase shift, or combinations of the same. Other relationships between the noise reference signal and the noise component of the physiological signal are also possible.

In some embodiments, clinically meaningful correlation between the noise reference signal and the noise component of the physiological signal is achieved, at least in part, by placing the first and second acoustic sensing elements **820**, **821** in proximity to one another. For example, as illustrated in FIG. 8, the first and second acoustic sensing elements **820**, **821** can be commonly located on a wearable acoustic sensor **815**. Disposing the first and second acoustic sensing elements **820**, **821** in proximity to one another can improve correlation between the noise reference signal and the noise component of the physiological signal by reducing differences in, for example, the amplitude, frequency content, and phase between the noise sensed at the first acoustic sensing element **820** as compared to the noise sensed at the second acoustic sensing element **821**.

The physical distance between the first and second acoustic sensing elements **820**, **821** can vary from embodiment to embodiment depending upon, for example, the expected frequency content of the noise, the presence of acoustically dispersive materials, acoustic reflectors or absorbers, or the like, that are located, for example, between the two sensing elements. For example, a physiological monitoring system **800** operated in an environment with relatively lower frequency noise (e.g., ambient noise) can be able to tolerate larger physical distances between the first and second acoustic sensing elements since such distances will be smaller relative to the wavelength of the noise than in the case of noise with higher frequency content. Thus, even despite a relatively larger physical separation between the first and second acoustic sensing elements, the noise sensed by the second acoustic sensing element can still be reasonably indicative of, or related to, the noise sensed by the first acoustic sensing element.

In some embodiments, the actual tolerable physical distance between the first and second acoustic sensing elements **820**, **821** can depend upon the particular application and/or noise-reducing requirements imposed by the application. In some embodiments, the first and second acoustic sensing elements **820**, **821** can be physically disposed in close enough proximity to one another such that a noise reference signal detected by the second acoustic sensing element **821** contains a sufficient amount of information regarding the noise component of the physiological signal detected by

the first acoustic sensing element **820** so as to provide a clinically significant reduction in the noise component of the physiological signal. This can be manifested, for example, by a clinically significant improvement in the accuracy of a physiological characteristic (e.g., respiratory rate) determined by the physiological monitoring system from a noise-reduced version of the physiological signal detected by the first acoustic sensing element **820**.

In some embodiments, the first and second acoustic sensing elements are physically located within a 1 m radius of one another. In some embodiments the first and second acoustic sensing elements are physically located within a 0.1 m radius of one another. In some embodiments the first and second acoustic sensing elements are physically located within a 0.01 m radius of one another. In some embodiments the first and second acoustic sensing elements are physically located within a 0.001 m radius of one another.

In some embodiments, the first and second sensing elements **820**, **821** can be disposed in separate sensor packages or otherwise be disposed at different locations throughout the operating environment. For example, FIG. 9A is a block diagram of an embodiment of an acoustic physiological monitoring system **900** with first and second acoustic sensing elements **920**, **921** disposed in or otherwise being associated with separate first and second sensors **916**, **917**. While shown as being coupled to the physiological monitor **907** via a single communication link **906**, a separate communication link **906** may be used for each sensor **916**, **917** in certain embodiments. In some embodiments, each communication link **906** includes one or more cables, hubs, and/or connectors as described herein. FIG. 9B is a block diagram including a first sensing element **920** disposed on a patient and a second sensing elements **920**, **921** disposed on a physiological monitor **907**.

Referring to FIG. 9A, the first and second sensors **816**, **817** can be positioned at a variety of locations on the patient **901**. For example, in certain embodiments, one or both of the sensing elements **920**, **921** (and their associated sensors **916**, **917**) can be positioned on or around sources of sounds generated by physiological processes. Such areas can include those associated respiratory or vocal sounds including for example, the throat, back of the neck, mouth, or some other portion of the head or neck, on the back or chest around the lungs, combinations of the same and the like. Other sensing element locations can include those generally associated with heart sounds, such as on the chest around the heart, on the throat, on the wrist, etc. Yet other locations can include those typically associated with digestive sounds such as near the stomach or on some other portion of the abdomen. Moreover, while the above examples are provided for the purposes of illustration, depending on the application, the sensors **916**, **917** can additionally be positioned at generally any location on the patient's body **901** including, for example, a hand, finger, arm, foot, leg, etc.

FIG. 9C illustrates an example system **990** including dual acoustic sensors **991**, **992** applied to a patient's **993** throat and chest, respectively. FIG. 9D illustrates a second example where sensors **994**, **995** are applied to different regions of a patient's **996** chest. The dual acoustic sensors **991**, **992**, **994**, **995** can be coupled to a physiological monitor **997** via a hub and a plurality of cables, as shown. The sensors **991**, **992**, **994**, **995**, monitor **997**, cables, hub, etc., can be any of those described herein or incorporated by reference, or can be some other acoustic sensors. Where multiple sensors are attached to the patient or are otherwise spatially separated throughout the operating environment, such an arrangement

may be referred to as a stereo monitoring environment that allows for stereo body sound monitoring.

The sensing elements **920**, **921** and, where present, associated sensor packages, can additionally be positioned at one or more locations in the operating environment not on the patient's body. For example, FIG. 9B is a block diagram of an embodiment of an acoustic physiological monitoring system **902** with a wearable acoustic sensor **915** that includes a first acoustic sensing element **920**, and a physiological monitor unit **907** that includes a second acoustic sensing element **921**. The physiological monitor unit **907** is adapted to be communicatively coupled with the wearable acoustic sensor **915** via, for example, a cable **906**. In some embodiments, the physiological monitor unit **907** is a non-wearable unit with one or more devices for processing signal outputs from the first and second acoustic sensing elements **920**, **921**. The physiological monitoring system **902** of FIG. 9B is similar to the physiological monitoring systems **800**, **900** except that the second acoustic sensing element **921** is physically located at the non-wearable physiological monitor **907** instead of at the wearable acoustic sensor **915**.

While shown on the monitor **907**, the second sensing element **921** can be positioned at a variety of other locations. For example, in cases where the physiological monitor **907** and the acoustic sensor **915** are communicatively coupled using a physical cable **906**, the cable **906** can be useful in placing a limit on the distance between the first and second acoustic sensing elements **920**, **921** to ensure that they remain in close enough proximity with one another to provide for meaningful noise reduction for a given medical sensing application. In other embodiments, the second acoustic sensing element **921** can be at any intermediate location between the monitor and the sensor, such as on or in the cable **906**, a connector, or a hub (not shown) such as the hub **120** of FIG. 1C, or generally at any separate location independent of the physiological monitor **907** or the acoustic sensor **915**. Where the second sensing element **921** is used to generate a noise reference, positioning the second sensing element **921** on or in the monitor **907**, hub, or at another intermediate location, rather than on the sensor **915** can advantageously reduce the wiring overhead in the system. On the other hand, it can be beneficial to locate the second sensing element **921** near the first sensing element **920** so as to generate a noise reference signal that is substantially correlated with the noise component of the signal detected by the first sensing element **920**. Thus, in certain cases, a trade off generally exists between locating the second sensing element **921** in proximity to the first sensing element **920** to improve noise rejection on the one hand, and locating the second sensing element remote from the first sensing element **920** to reduce wiring overhead on the other. Thus, in circumstances, locating the second sensing element **921** at the hub or at another intermediate location between the monitor **907** and the first sensing element **920** provides the desired balance between reduced wiring overhead and adequate noise rejection.

As mentioned, where a noise source is readily identifiable, the second sensing element **921** can be positioned in physical proximity to the noise source. In this manner, the second sensing element **921** can be used to produce a signal including a relatively clean noise reference signal, allowing for improved noise compensation. Such noise sources can be those generating any of the interfering noise described herein such as non-target physiological sounds emanating from the patient (e.g., heart, breathing or digestive sounds), ambient noise (e.g., traffic, ambient speech sounds, computer humming, and the like), or vibrations or other noise

emanating from skin-coupled devices (e.g., electrosurgical devices, CPAP machines, nebulizers, etc.).

Several example scenarios incorporating multiple sensing elements **920**, **921** strategically located at separate locations in the operating environment will now be described. These examples are provided for the purposes of illustration, and are not intended to be limiting. As a first illustrative example, referring to FIG. **9A**, the first sensor **916** is a physiological signal sensor and is positioned on or around a source of breathing sounds (e.g., the neck), while the second sensor **917** is a noise sensor and is positioned on or around the heart to detect heart sounds and/or other noise components. Thus, the signal from the second sensor **917** can be used to cancel or otherwise attenuate any residual heart sounds (and/or ambient or other noise) that may bleed into the signal produced by the first sensor **916**.

In another example scenario, a CPAP machine or other medical device is coupled to the patient. The first sensor **916** is a physiological signal sensor positioned on the patient's heart to detect heart sounds, and the second sensor **917** is a noise sensor positioned on the CPAP machine or other medical device. Thus, the signal produced by the second sensor **917** can be used to cancel any residual noise from the CPAP machine (and/or ambient or other noise) that bleeds into the signal detected by the first sensor **916**.

In yet another illustrative example, the first sensor **916** is a physiological signal sensor positioned to detect breathing sounds, and the second sensor **917** is a noise sensor positioned on the patient near a planned electrosurgical site (or on an electrosurgical device itself). The second sensor **917** can be used in such a situation to cancel noise generated by the electrosurgical device (and/or ambient or other noise) that bleeds into the signal detected by the first sensor **916**.

Selective Configuration of Multiple Sensing Elements

Depending on the desired application, the multiple sensing elements can be selectively configured in a plurality of modes. For example, referring still to FIGS. **9A-9B**, the sensing elements **920**, **921** can be configured as either physiological signal sensors or noise sensors in some embodiments. In addition to physiological sensing and noise modes, the sensing elements can be configured in a variety of other modes. For example, in one embodiment, one or more of the sensing elements **920**, **921** is configurable in an auscultation mode. For example, the sensing elements **920**, **921** can be configured in a listening mode in which an operator can generally continuously listen to audio output indicative of patient bodily or voice sounds. In yet another embodiment, the sensing elements **920**, **921** can be configured to sense and process ultrasonic signals (e.g., for ultrasonic imaging). Examples of sensors capable of various types of audio output, ultrasonic sensing, and other compatible functionality are provided in U.S. patent application Ser. No. 12/905,036, entitled **PHYSIOLOGICAL ACOUSTIC MONITORING SYSTEM**, filed on Oct. 14, 2010, incorporated by reference herein in its entirety.

As one example, the first sensor **916** is positioned on or around a source of breathing sounds (e.g., on the throat), while the second sensor **917** is positioned on or around the heart to detect heart sounds. In a first mode, the first sensor **916** is configured in a physiological sensing mode and the second sensor **917** is configured in a noise sensing mode, while in a second mode, the roles of the sensors are generally switched. In this manner, breathing sounds are monitored and the effect of heart sounds (and/or other noise) is reduced according to noise cancelling techniques described herein. Moreover, in the second mode, heart sounds are monitored, and the effect of any residual breathing sounds (and/or other

noise) is reduced. Thus, according to such techniques, a user can flexibly and efficiently switch between monitoring reduced noise versions of a wide variety of physiological signals.

Moreover, the sensing elements can be configured for use in more than one mode at a time in certain embodiments. For example, each of the sensing elements **920**, **921** can be configured simultaneously as both physiological signal sensing elements and noise sensing elements. In the above example scenario, the first sensing element **920** can be used to monitor breathing sounds and also generally simultaneously provide a noise reference to the second sensing element **921**. Conversely, the second sensing element **921** can be used to monitor heart sounds and also generally simultaneously provide a noise reference to the first sensing element **920**. While other modes are possible, in various embodiments, the sensing elements **920**, **921** can be configured generally simultaneously for two or more of physiological signal sensing, noise sensing, auscultation, and ultrasonic sensing.

The configuration of the sensing elements **920**, **921** may be manually selectable by a user, or can be automatically configurable by the system. For example, one or more user-actuable inputs (e.g., buttons, switches, keypad inputs, etc.) may be provided to the user for setting the sensing element **920**, **921** modes. Such inputs may be located on the monitor **907**, in proximity to the sensing elements **920**, **921** themselves, such as on the respective sensor packaging, or at some other appropriate location.

Moreover, the modes of the sensing elements **920**, **921** can be configurable either as a group or individually in various embodiments. For example, referring to the above example where the first sensing element **920** is positioned to detect breathing sounds and a second sensing element **921** is positioned to detect heart sounds, the system may allow the user to select either of a breathing sound monitoring mode or a heart sound monitoring mode. Based on the selection, the system will appropriately automatically configure each sensing element **920**, **921** mode. In another embodiment, the user sets each of the respective sensing element **920**, **921** modes separately.

Where multiple sensing elements are present and are configured or selectively configurable for use as noise sensing elements, the system according to some embodiments automatically selects which sensing element or group thereof to use in the noise cancellation algorithm. Moreover, the outputs from multiple noise sensing elements or a selected combination thereof can be combined so as to provide improved noise rejection.

As one example, a first sensing element **920** is disposed on a wearable acoustic sensor **915** positioned on the patient's neck and is configured to receive a signal including physiological signal components and noise components. Second, third and fourth acoustic sensing elements are disposed on the cable, at the hub, and in the monitor, respectively, and are configured to receive noise signals.

In such embodiments, the physiological monitor **907** or other system component can generally use signals received from at least one of the noise acoustic sensing elements to perform noise reduction. For example, in the above example, each of the signals from the second, third and fourth sensing elements can be combined or otherwise used to perform noise compensation. In other cases, only a subset of one or more of the signals may be used as desired.

The system **900** can allow for manual selection of the noise acoustic sensing element(s) to use during monitoring, or can alternatively automatically select which of the noise

acoustic sensors (e.g., the second third, or fourth sensing elements or a combination thereof) to use. Automatic selection can be performed in a variety of ways.

For example, in one embodiment, the system **900** evaluates the signals from each of the noise acoustic sensors, such as by assessing the magnitude or quality of the respective noise signals, and selects one or more of the signals to use based on the evaluation. For example, in some embodiments, the noise sensing element or combination of noise sensing elements that provides one or more of the highest amplitude noise reference signal or the cleanest noise reference signal is selected. In another embodiment, the system **900** assesses the degree of noise compensation achieved using the different noise acoustic sensing elements and/or combinations thereof, and selects the noise acoustic sensing element or combination thereof that provides the highest (or otherwise desirable) level of noise compensation to use during monitoring.

Noise Compensation Using Signal or Noise Correlation Between Sensing Elements

As described, it can be advantageous in certain embodiments for the first and second acoustic sensing elements to be substantially similar or even identical in terms of material properties, mounting, and packaging so that their signal outputs will likewise have shared characteristics in response to excitation of the acoustic sensing elements by a common source. This can be the case where the outputs of the first and second acoustic sensing elements are to be combined using techniques for selecting or rejecting signal components from the two sensing element outputs based on their common or distinguishing features.

For example, referring to FIGS. **9A-9B** for the purposes of illustration, in some applications it can be expected that, owing to similarities in the design and placement of the first and second acoustic sensing elements **920, 921** or other factors, the components of their output signals resulting from a common source (e.g., the patient's body) will be generally similar while signal components from other sources (e.g., noise components) can be expected to have certain dissimilarities (e.g., phase or time shift). In these cases, the output signals from the first and second acoustic sensing elements **920, 921** can be combined in ways that accentuate commonalities between the two signals while attenuating differences between the two output signals.

In one example scenario, referring to FIG. **9A**, the first and second acoustic sensing elements **920, 921** are substantially the same type and are included in separate sensor packages each placed on the patient. As described, the physiological signal components produced by the sensing elements **920, 921** are substantially correlated with respect to one another. In some cases, the correlation can be enhanced via strategic placement of the sensing elements **920, 921** with respect to one another. For example, the sensor packages can be placed generally symmetrically about the signal source (e.g., the throat or chest). In contrast, the noise signal components produced by the sensing elements **920, 921** are substantially uncorrelated with respect to one another.

In such a scenario, the components can be uncorrelated for a variety of reasons. For example, noise signals emanating from external sources may reflect off of the skin or sensor package before reaching the respective sensing element **920, 921**. The signal may also propagate through a portion of the sensor package before reaching the respective sensing element **920, 921**, causing additional distortions. Moreover, the degree and quality of distortion in the noise signal received by the sensing elements **920, 921** can differ

significantly between the sensing elements **920, 921**. For example, in addition to other possible reasons, the variation in distortion can be caused by a variation in the respective angle of arrival of the noise signal at each of the sensor packages. This can be due to the difference in the orientation of the noise source from one sensor package to another.

The output signals from the first and second acoustic sensing elements **920, 921** in such a scenario can be combined to accentuate the correlated physiological signal components and attenuate the uncorrelated noise components between the two output signals. For example, while a variety of techniques can be used, the outputs from the sensing elements are summed together in one embodiment. The correlated components will tend to additively combine, while the uncorrelated components will not, resulting in an overall improved SNR. In other embodiments, more than two (e.g., three, four, five or more) sensing elements **820, 821** are used.

In some other embodiments, certain noise components (e.g., ambient noise components) of the signals produced by the first and second sensing elements **920, 921** may be correlated, while the physiological signal components may be uncorrelated. In such cases, additional appropriate techniques can be used to generate a reduced noise signal. Examples of such techniques, including cross-correlation, are described in U.S. application Ser. No. 12/904,789, entitled ACOUSTIC RESPIRATORY MONITORING SYSTEMS AND METHODS, filed on Oct. 14, 2010, the entirety of which is incorporated by reference herein.

Additional Noise Compensation Embodiments

FIG. **10** is a block diagram of an embodiment of an acoustic sensor **1015** that includes a physiological signal acoustic sensing element **1020** with an acoustic coupler **1014** for acoustically coupling it to a patient's body, and a noise acoustic sensing element **1021**. In some embodiments, the acoustic coupler **1014** is any device or structure, made using any material, that effectively enhances the transmission of acoustic signals from a patient's body to the physiological signal acoustic sensing element **1020**. In the case where the physiological signal acoustic sensing element **1020** is a piezoelectric film, the acoustic coupler **1014** can be a mechanical structure in contact with both the patient's skin **1001** and the acoustic sensing element **1020** so as to transmit vibrations from the patient's body to the physiological signal acoustic sensing element. The acoustic coupler **1014** can be, for example, similar to the acoustic coupler **214** described herein. Other acoustic couplers can also be used. The acoustic sensing elements **1020, 1021** and the acoustic coupler **1014** can be physically supported in a desired spatial relationship with respect to one another using, for example, a suitable frame.

The acoustic coupler **1014** provides an amount of acoustic coupling between the physiological signal acoustic sensing element **1020** and the patient **1001** that is greater than the amount of acoustic coupling that can exist between the noise acoustic sensing element **1021** and the patient. This increased amount of acoustic coupling is illustrated in FIG. **10** by solid double arrows. Of course, the physiological signal from the patient's body **1001** can also be picked up by the noise acoustic sensing element **1021**, just as noise can be picked up by both of the acoustic sensing elements **1020, 1021**.

However, the strength of the physiological signal present in the output of the noise acoustic sensing element **1021** will typically be less than the strength of the physiological signal present in the output of the physiological signal acoustic sensing element **1020**, as a result of the lack of an acoustic

coupler between the patient's body **1001** and the noise acoustic sensing element **1021**. This is illustrated in FIG. **10** by the dashed double arrows between the patient's skin **1001** and the noise acoustic sensing element **1021**. For example, in some embodiments, the strength of the physiological signal in the output of the noise acoustic sensing element **1021** is less than 50% of the strength of the physiological signal in the output of the physiological signal acoustic sensing element **1020**. In some embodiments, the signal strength of the physiological signal at the output of the noise acoustic sensing element **1021** is less than 25%, or less than 10%, or less than 5%, of its strength at the output of the physiological signal acoustic sensing element **1020**.

In some embodiments, it is advantageous for the strength of the physiological signal in the output of the noise acoustic sensing element **1021** to be significantly less than the strength of the physiological signal in the output of the physiological signal acoustic sensing element **1020**. In this way, the output of the noise acoustic sensing element **1021** can be effectively used as a noise reference signal to provide useful information for reducing the amount of noise present in the output of the physiological signal acoustic sensing element **1020**.

While in some embodiments it is advantageous for the two acoustic sensing elements **1020**, **1021** to be in close proximity so as to improve the degree of correlation between the noise picked up by each acoustic sensing element, it can be likewise advantageous for the noise acoustic sensing element **1021** to be located further away from the patient's body **1001** to reduce the strength of the physiological signal picked up by the noise acoustic sensing element **1021**. In some cases, these two design goals can work in opposition to one another. However, in some embodiments, both advantages can be had by the addition of one or more acoustic decouplers or isolators to the acoustic sensor.

FIG. **11** is a block diagram of an embodiment of an acoustic sensor **1115** that includes a physiological signal acoustic sensing element **1120** with an acoustic coupler **1114** for increasing acoustic coupling between it and a patient's body, and a noise acoustic sensing element **1121** with an acoustic decoupler **1116** for decreasing acoustic coupling between it and the patient's body **1101**. The acoustic decoupler **1116** reduces further the amount of physiological sounds from the patient's body that is picked up by the noise acoustic sensing element **1121**. Acoustic decoupling can include, for example, complete acoustic isolation or substantial acoustic isolation of the sensing element **1121** from the patient's skin **1101**. Thus, in certain embodiments, the acoustic decoupler **1116** can reduce sounds from being transmitted from the patient's skin **1101** to the sensing element **1121**, or prevent the transmission of these sounds entirely.

This can be advantageous since the acoustic decoupler **1116** can provide for a higher degree of certainty that any similarities or correlation between the output of the noise acoustic sensing element **1121** and the output of the physiological signal acoustic sensing element **1120** are more likely to be indicative of the acoustic noise than the target physiological sounds. This can, in turn, allow a noise attenuator device to more accurately or fully reduce the strength of the acoustic noise component from the output of the physiological signal acoustic sensing element **1120**.

The acoustic decoupler **1116** can be any device or structure, made using any material, that can effectively acoustically isolate different components. For example, the acoustic decoupler **1116** can be a device or structure that is known to effectively reflect or absorb acoustic waves. In some

embodiments, the acoustic sensor **1115** also includes one or more additional acoustic decouplers. For example, an acoustic decoupler **1117** can be physically positioned between the physiological signal acoustic sensing element **1120** and any expected source of noise, thereby reducing the amount of noise picked up by the physiological signal acoustic sensing element. The acoustic sensing elements **1120**, **1121** and any acoustic decouplers **1116**, **1117** can be physically supported in a desired spatial relationship with respect to one another using, for example, a suitable frame.

FIG. **12** is a cross-sectional schematic drawing of an embodiment of an acoustic sensor **1215** that includes a physiological signal acoustic sensing element **1220** and a noise acoustic sensing element **1221**. A frame **1218** supports the two acoustic sensing elements **1220**, **1221**. In some embodiments, the frame **1218** is similar to the frame **218** described herein. For example, the frame **1218** can provide an upper cavity **1230** and a lower cavity **1236**. The lower cavity **1236** can be used to form an acoustic cavity for an acoustic sensing element, while the upper cavity **1230** can be used to house printed circuit boards and electrical components.

As discussed herein, in some embodiments, the two acoustic sensing elements **1220**, **1221** are piezoelectric films, for example, similar to those illustrated in FIGS. **3A-3C**. Each of the piezoelectric films can include electrical poles across which a voltage is induced by acoustic waves in the piezoelectric films, as described herein. In the illustrated embodiment, the physiological signal acoustic sensing element **1220** is a piezoelectric film wrapped around a portion of the frame **1218** and extending across the lower cavity **1236** in tension. Thus, the lower cavity **1236** serves as an acoustic cavity, and the piezoelectric film **1220** stretched in tension across the acoustic cavity **1236** is free to respond to acoustic waves incident upon it.

In some embodiments, the noise acoustic sensing element **1221** is likewise a piezoelectric film wrapped around a portion of the frame **1218**. The piezoelectric film **1221** can be bonded to the frame **1218** using, for example, an adhesive layer. In this way, the piezoelectric film **1221** can vibrate in conjunction with the frame **1218** in response to acoustic waves that are incident upon it.

The piezoelectric films **1220**, **1221** are shown in FIG. **12** spaced apart for clarity and ease of illustration. It should also be understood that, in some embodiments, other layers can be present, such as any of the additional layers described above. The two piezoelectric films **1220**, **1221** can be separated by one or more adhesive layers, electrical insulators, mechanical supports, acoustic decouplers, etc.

The acoustic sensor **1215** also includes an acoustic coupler **1214**. In some embodiments, the acoustic coupler **1214** is similar to the acoustic coupler **214** described herein. The acoustic coupler **1214** can include a lower protrusion or bump configured to press against the skin **1201** of a patient when the acoustic sensor is fastened into place on the patient. The acoustic coupler **1214** can also include a protrusion **1212** designed to abut against the physiological signal acoustic sensing element **1220** and to bias it in tension across the acoustic cavity **1236**. The acoustic coupler **1214** can also include sidewalls **1213** that extend upward and enclose at least a portion of the frame **1218**.

For clarity of illustration, not all of the components of the acoustic sensor **1215** are illustrated. The frame **1218**, the piezoelectric film **1220**, and the acoustic coupler **1214** can all include any of the features described herein or illustrated with respect to FIGS. **2A-6E**. In addition, the acoustic sensor **1215** can include any of the features disclosed or illustrated

with respect to the same figures, including bonding layers, electrical shielding layers, sealing layers, etc. The acoustic sensor **1215** can also include electrical components (e.g., a voltage detector circuit to detect the electrical voltages induced across the poles of each of the piezoelectric films **1220**, **1221**), printed circuit boards, cables, patient fasteners, and other features disclosed herein.

While FIG. **12** illustrates that the two acoustic sensing elements **1220**, **1221** are layered one on top of the other, they could instead be disposed with other layouts. For example, the two acoustic sensing elements **1220**, **1221** could be supported by the frame **1218** side-by-side. In addition, while both acoustic sensing elements **1220**, **1221** are illustrated as being supported by a common frame **1218** inside a common housing, they could instead each be supported by a separate frame and/or have separate housings. Of course, the frame **1218** could also take many different shapes than the one illustrated.

FIG. **13** is a cross-sectional schematic drawing of another embodiment of an acoustic sensor **1315** that includes a physiological signal acoustic sensing element **1320** and a noise acoustic sensing element **1321**. The acoustic sensing elements **1320**, **1321** and the acoustic coupler **1314** are as already described with respect to FIG. **12**. The frame **1318**, however, includes another cavity **1332** in addition to the upper cavity **1330** and the lower cavity **1336**. As illustrated, the noise acoustic sensing element **1321**, a piezoelectric film, stretches across the cavity **1332** in tension to form an acoustic cavity for the noise acoustic sensing element. The presence of the acoustic cavity **1332** allows the noise acoustic sensing element **1321** greater freedom to vibrate in response to acoustic waves that are incident upon it.

As illustrated in FIG. **13**, the acoustic cavity **1332** for the noise acoustic sensing element **1321** can be provided as a depression inside the floor of the acoustic cavity **1336** for the physiological signal acoustic sensing element **1320**. The acoustic cavity **1332** could also be formed in one or both of the sidewalls of the acoustic cavity **1336**. Alternatively, the acoustic cavity **1332** could be formed in some other portion of the frame **1318** independent of the acoustic cavity **1336** for the physiological signal acoustic sensing element **1320**. In some embodiments, all or a portion of the upper cavity **1330** provided by the frame **1318** can serve as an acoustic cavity for the noise acoustic sensing element **1321**. For example, the noise acoustic sensing element **1321** could stretch across the upper cavity **1330** in tension. Many other multiple-acoustic-cavity layouts are also possible.

FIG. **14** is a cross-sectional schematic drawing of another embodiment of an acoustic sensor **1415** that includes a physiological signal acoustic sensing element **1420** and a noise acoustic sensing element **1421**. Once again, in this embodiment, the physiological signal acoustic sensing element is a piezoelectric film **1420**. An acoustic coupler **1414** acoustically couples the piezoelectric film **1420** to the patient's body **1401**. The noise acoustic sensing element **1421** is likewise a piezoelectric film. However, the position of the noise acoustic sensing element **1421** differs from that of the embodiment illustrated in, for example, FIG. **13** in that the piezoelectric film **1421** shares the acoustic cavity **1436**. In the embodiment of FIG. **14**, the two piezoelectric films **1420**, **1421** both extend over the acoustic cavity **1436** adjacent to one another. This is shown in the bottom view **1450** of the two piezoelectric films **1420**, **1421**. Other physical layouts where the two acoustic sensing elements share a common acoustic cavity are also possible.

While in the embodiment of FIG. **14** the two acoustic sensing elements **1420**, **1421** both extend over the acoustic

cavity **1436**, in some embodiments, the acoustic coupler **1414** only acoustically couples the physiological signal acoustic sensing element **1420** to the patient's skin **1401**, not the noise acoustic sensing element **1421**. For example, the acoustic coupler **1414** can only be in physical contact with the physiological signal acoustic sensing element **1420** without substantially contacting the noise acoustic sensing element **1421**. In cases where the acoustic coupler **1414** is a bump such as the one described herein, the bump can only be aligned with the physiological signal acoustic sensing element **1420**, as indicated by the dashed circle **1414** in the bottom view **1450** of the acoustic sensing elements **1420**, **1421**.

FIG. **15** is a cross-sectional schematic drawing of an embodiment of an acoustic sensor **1515** that includes a piezoelectric physiological signal acoustic sensing element **1520** and a separate noise microphone **1521**. The frame **1518**, the piezoelectric film **1520**, and the acoustic coupler **1514** are as described and illustrated with respect to, for example, FIG. **13**. However, the acoustic sensor **1515** does not include a second piezoelectric film to serve as the noise acoustic sensing element but instead includes a separate microphone **1521**. The noise microphone **1521** can be housed, for example, in the upper cavity **1530** of the frame **1518**. Other locations can also be suitable. The noise microphone **1521** can be, for example, a condenser microphone, a MEMS microphone, or an electromagnetic induction microphone, a light-modulation microphone, or a piezoelectric microphone. The noise microphone **1521** can exhibit directionality such that it is more sensitive, for example, in the upward direction away from the patient's skin **1501** in order to reduce its sensitivity to the physiological sounds picked up by the physiological signal acoustic sensing element **1520**.

FIG. **16** illustrates a time plot **1602** of an acoustic physiological signal corrupted by noise, as well as a time plot **1618** of the noise. The plot **1602** of the acoustic physiological signal corrupted with noise is a simplified representation of a patient breathing. Each of the pulses **1604**, **1610**, **1612** represents either an inhalation or exhalation. Three bursts of noise **1606**, **1608**, **1614** are superimposed on the physiological signal. The plot **1602** represents an output from a physiological signal acoustic sensing element (e.g., **1020**, **1220**, **1320**, **1420**, **1520**), as described herein. The breathing sounds are acoustically coupled to the physiological signal acoustic sensing element via an acoustic coupler, as described herein. However, the physiological signal acoustic sensing element also picks up noise from the patient's surroundings.

The plot **1618** is a simplified representation of noise detected by a noise acoustic sensing element (e.g., **1021**, **1221**, **1321**, **1421**, **1521**), as described herein. In particular, there are three bursts **1620**, **1622**, **1624** of noise. In some embodiments, it is advantageous that the bursts of noise **1620**, **1622**, **1624** in the plot **1618** share certain characteristics, and/or that they be meaningfully correlated with, the bursts of noise **1606**, **1608**, **1614** in the physiological signal. Generally, this will be dependent upon the positioning and design of both the physiological signal acoustic sensing element and the noise acoustic sensing element. For example, the amplitude of the corresponding noise bursts in the respective plots **1602**, **1618** can be related by a scalar factor, a time shift, a phase shift, or in some other way depending upon, for example, the relative placement of the two acoustic sensing elements. The output of the noise acoustic sensing element can also contain a signal component representative of the physiological sounds from the

patient, though, in some embodiments, this signal component is weaker in the output from the acoustic sensing element than it is in the physiological signal acoustic sensing element, as a result of the acoustic coupler.

FIG. 17 is a block diagram an embodiment of a noise attenuator 1740 of an acoustic physiological monitoring system. As described herein, the noise attenuator 1740 can be communicatively coupled with first and second acoustic sensing elements 1720, 1721. In some embodiments, the output of the first acoustic sensing element 1720 is a physiological signal with noise 1730, as illustrated in plot 1602 in FIG. 16. In some embodiments, the output of the second acoustic sensing element 1721 is a noise reference signal 1731, as illustrated in plot 1618 in FIG. 16. Each of these signals 1730, 1731 is input to the noise attenuator 1740. The noise attenuator 1740 then reduces or removes the noise component from the physiological signal 1730 based on information regarding the noise component that is gleaned from the noise reference signal 1731.

The noise attenuator 1740 can use any of numerous methods and components for reducing, removing, filtering, canceling, subtracting, or separating out noise in a signal based on a noise reference signal, or combinations of the same or the like. For example, the noise attenuator 1740 may be an adaptive noise filter or an adaptive noise canceler. The noise attenuator 1740 can perform time domain and/or frequency domain operations. In some embodiments, the noise attenuator 1740 employs spectral subtraction methods such as power-based, magnitude-based, or non-linear spectral subtraction techniques. The noise attenuator 1740 can include time shift modules, phase shift modules, scalar and/or complex multiplier modules, filter modules, etc., each of which can be implemented using, for example, hardware (e.g., electrical components, FPGAs, ASICs, general-purpose digital signal processors, etc.) or a combination of hardware and software.

In some embodiments, the noise attenuator 1740 includes a self-adjusting component whose effect on the physiological signal corrupted by noise 1730 continuously varies in response to information derived from the noise reference signal 1731. For example, the self-adjusting component can be an adaptive filter 1742 whose transfer function, or some other characteristic, is iteratively updated based on analysis of the noise reference signal 1731. The adaptive filter 1742 can be implemented, for example, using a digital signal processor with iteratively updated filter coefficients. Other methods of implementing the adaptive filter 1742 can also be used. Filter coefficients can be updated using, for example, a least mean squares algorithm (LMS), or a least squares algorithm, a recursive least squares algorithm (RLS). The noise attenuator 1740 can also use, for example, a Kalman filter, a joint process estimator, an adaptive joint process estimator, a least-squares lattice joint process estimator, a least-squares lattice predictor, a noise canceler, a correlation canceler, optimized time or frequency domain implementations of any of the above, combinations of the same, and the like.

FIG. 18 is a block diagram of an embodiment of a signal quality calculator 1850 in an acoustic physiological monitoring system. The signal quality calculator 1850 is communicatively coupled with first and second acoustic sensing elements 1820, 1821. In some embodiments, one input to the signal quality calculator 1850 is a physiological signal corrupted by noise 1830 (e.g., as illustrated in plot 1602 in FIG. 16), while the other input is a noise reference signal 1831 (e.g., as illustrated in plot 1618 in FIG. 16). Based, at

least in part, on these input signals, the signal quality calculator 1850 outputs an objective signal quality indicator 1851.

As described herein, the signal quality calculator 1850 is a device that is used to determine, for example, an objective indicator of the quality of the physiological information obtained from one or more acoustic sensing elements. This can be done, for example, by comparing the physiological signal 1830 with the noise signal 1831. The signal quality calculator 1850 can also output an objective indicator of the degree of confidence in the accuracy of a physiological characteristic (e.g., respiratory rate) determined based on the physiological information collected from one or more acoustic sensors.

In some embodiments, the signal quality calculator 1850 includes one or more signal envelope detectors 1852, one or more peak detectors 1854, and a comparator 1856. The envelope detectors 1852 are used, for example, to detect the respective amplitude envelopes 1616, 1626 of the physiological signal 1830 and the noise reference signal 1831, as illustrated in FIG. 16. The envelope detectors 1852 can be implemented in any way known in the art. For example, the envelope detectors 1852 can use squaring and low-pass filtering techniques and/or Hilbert transform techniques for envelope detection. Other techniques or devices can also be used for envelope detection, including analog devices.

Once the amplitude envelopes of the physiological signal 1830 and the noise reference signal 1831 have been identified, peak detectors 1854 can be used to identify different peaks in the amplitude envelopes, the temporal spacing between peaks, the relative maximum amplitude of the peaks, the time width of the peaks, etc. For example, with reference to plot 1618, the peak detector 1854 can identify three separate peaks, one for each illustrated bursts of acoustic noise. With reference to plot 1602, the peak detector 1854 can identify five separate peaks: one corresponding to the first pulse 1604 of breathing sounds, one corresponding to the first burst of acoustic noise 1606, a larger amplitude peak corresponding to the second pulse of breathing sounds with superimposed noise 1610, 1608, one corresponding to the third pulse of breathing sounds 1612, and one corresponding to the third burst of acoustic noise 1614.

Once the peaks of the amplitude envelopes have been detected, possibly along with information regarding the temporal spacing between the peaks, the relative heights of the peaks, their widths etc., this information can then be transmitted to the comparator 1856. In some embodiments, the comparator 1856 is endowed with logic for determining an objective signal quality indicator based, at least in part, on the information from the peak detectors 1854.

In some embodiments, the comparator 1856 can determine whether each of the identified peaks in the amplitude envelope of the physiological signal 1830 has a corresponding peak in the amplitude envelope of the noise signal 1831. For example, with respect to the plots 1602, 1618 in FIG. 16, the comparator 1856 can determine that the first peak in the physiological signal 1830 (the first pulse of breathing sounds 1604) does not have a corresponding peak in the noise signal 1831 at the same time. On this basis, the comparator 1856 could judge that the first peak 1604 can well likely represent physiological information. Upon analyzing the second peak in the physiological signal 1830 (the first burst of noise 1606), the comparator 1856 could note the presence of a corresponding peak 1620 in the noise reference signal 1831 at the same time and having approximately the same height and width. On this basis, the comparator 1856 could judge

that the second peak in the physiological signal **1830** can well likely represent acoustic noise.

An analysis of the third peak in the physiological signal **1830** (the second pulse of breathing sounds **1610**) can identify a corresponding peak **1622** in the noise reference signal **1831** at the same time but having a smaller width and height than the peak **1610** in the physiological signal. On this basis, the comparator **1856** can determine that it is somewhat likely that the third peak **1610** in the physiological signal **1830** is representative of physiological information. In this way, the signal quality calculator **1850** can identify, for example, individual features of the time domain physiological signal **1830** and noise reference signal **1831**, and then determine the likelihood that each feature represents physiological information or noise information.

The signal quality calculator **1850** can then calculate and output an indicator (e.g., a probability value, a percentage, an occurrence indicator, a Boolean or binary value, an alarm or alert, or some other indicator) to express the extent to which the physiological signal **1830** is viewed as being indicative of actual physiological information rather than noise. The signal quality calculator **1850** can also output an indicator to express the confidence in a physiological characteristic calculated from the physiological signal **1830**. For example, if the signal quality calculator **1850** determines that the physiological signal **1830** is primarily composed of physiological information, then it can determine a high confidence level in a physiological characteristic (e.g., respiratory rate) determined from the physiological signal **1830**. In some embodiments, the physiological signal with reduced noise (e.g., **1741**) from the noise attenuator can also serve as an input to the signal quality calculator **1850**.

While a time domain method for determining signal quality is illustrated in FIG. **18**, signal quality calculations could also be performed in the frequency domain. Also, different signal quality calculation algorithms can be used depending upon the particular type of physiological information being sensed, and the characteristics of the signals that are representative of that physiological information.

Electromagnetic Interference (EMI) Compensation

In some embodiments, the physiological monitoring systems and patient sensors described herein include electromagnetic interference compensation features. The electromagnetic interference compensation features can be useful for reducing any deleterious effect of EMI on the accuracy of physiological characteristics determined using the monitoring systems. One possible source of such EMI could be, for example, 50-60 Hz RF waves generated by the electric power distribution system in a patient care facility.

In some embodiments, the physiological monitoring systems include an electrical conductor for detecting an EMI reference signal that is indicative of EMI that may have corrupted electrical signals used by the physiological monitoring systems (e.g., a physiological signal generated by an acoustic sensing element). The EMI reference signal detector can be, for example, a dedicated antenna that is positioned at a location where the EMI that it detects is in some way representative of, or meaningfully correlated with, the EMI to which an electrical signal within the patient sensor is exposed. The EMI reference signal detector can be located, for example, on or in one or more wearable patient sensors (e.g., **215**, **815**, **915**, etc.), though it may also be located in a separate physiological monitor unit, intermediate location (e.g., cable, connector or hub), at any location described above with respect to acoustic noise reference sensing elements, or at some other location.

In some embodiments, the EMI reference signal detector is a conductive plate or wire, or some other conductive structure. In some embodiments, the EMI reference signal detector is left electrically floating. While in some embodiments, the EMI reference signal detector is a dedicated component, in other embodiments other existing components of, for example, a patient sensor described herein can be used as the EMI reference signal detector. For example, one or more electrical shielding layers (e.g., **226**, **228**) in a patient sensor can be used to detect EMI and to generate an EMI reference signal. Generally, according to certain aspects, any of the shielding barriers described herein (e.g., with respect to FIGS. **2B-E**, **5A-B**, **21-22**, etc.) can be used to detect EMI and generate an EMI reference signal.

In some embodiments, the EMI reference signal generated by the EMI reference signal detector is transmitted to a noise attenuator or other sensing circuitry. The noise attenuator can also be communicatively coupled to, for example, one or more physiological electrical signals output from the acoustic sensing elements described herein. Such physiological electrical signals can be corrupted by any EMI to which they are exposed.

The noise attenuator or other sensing circuitry reduces or removes the EMI component from the physiological signal based on information regarding the EMI that is gleaned from the EMI reference signal. The noise attenuator or other sensing circuitry can use any of numerous methods and components for reducing, removing, filtering, canceling, subtracting, or separating out EMI in a signal based on the EMI reference signal, or combinations of the same or the like. For example, the noise attenuator may be an adaptive noise filter or an adaptive noise canceler. The noise attenuator can perform time domain and/or frequency domain operations. The noise attenuator can include time shift modules, phase shift modules, scalar and/or complex multiplier modules, filter modules, etc., each of which can be implemented using, for example, hardware (e.g., electrical components, FPGAs, ASICs, general-purpose digital signal processors, etc.) or a combination of hardware and software.

In some embodiments, the noise attenuator or other sensing circuitry includes a self-adjusting component whose effect on the physiological signal corrupted by EMI continuously varies in response to information derived from the EMI reference signal. For example, the self-adjusting component can be an adaptive filter whose transfer function, or some other characteristic, is iteratively updated based on analysis of the EMI reference signal. The adaptive filter can be implemented, for example, using a digital signal processor with iteratively updated filter coefficients. Other methods of implementing the adaptive filter can also be used. Filter coefficients can be updated using, for example, a least mean squares algorithm (LMS), or a least squares algorithm, a recursive least squares algorithm (RLS). The noise attenuator can also use, for example, a Kalman filter, a joint process estimator, an adaptive joint process estimator, a least-squares lattice joint process estimator, a least-squares lattice predictor, a noise canceler, a correlation canceler, optimized time or frequency domain implementations of any of the above, combinations of the same, and the like.

Additional Sensor Embodiments

FIG. **19A** is a top perspective of a sensor system **1900** including a sensor assembly **1901** suitable for use with any of the physiological monitors shown in FIGS. **1A-C** and a monitor cable **1911**. The sensor assembly **1901** includes a sensor **1915**, a cable assembly **1917** and a connector **1905**. The sensor **1915**, in one embodiment, includes a sensor subassembly **1902** and an attachment subassembly **1904**.

The cable assembly **1917** of one embodiment includes a cable **1907** and a patient anchor **1903**. The various components are connected to one another via the sensor cable **1907**. The sensor connector subassembly **1905** can be removably attached to monitor connector **1909** which is connected to physiological monitor (not shown) through the monitor cable **1911**. In one embodiment, the sensor assembly **1901** communicates with the physiological monitor wirelessly. In various embodiments, not all of the components illustrated in FIG. **19A** are included in the sensor system **1900**. For example, in various embodiments, one or more of the patient anchor **1903** and the attachment subassembly **1904** are not included. In one embodiment, for example, a bandage or tape is used instead of the attachment subassembly **1904** to attach the sensor subassembly **1902** to the measurement site. Moreover, such bandages or tapes may be a variety of different shapes including generally elongate, circular and oval, for example.

The sensor connector subassembly **1905** and monitor connector **1909** may be advantageously configured to allow the sensor connector **1905** to be straightforwardly and efficiently joined with and detached from the monitor connector **1909**. Embodiments of sensor and monitor connectors having similar connection mechanisms are described in U.S. patent application Ser. No. 12/248,856 (hereinafter referred to as “the ‘856 application”), filed on Oct. 9, 2008, which is incorporated in its entirety by reference herein. For example, the sensor connector **1905** includes a mating feature **1913** which mates with a corresponding feature (not shown) on the monitor connector **1909**. The mating feature **1905** may include a protrusion which engages in a snap fit with a recess on the monitor connector **1909**. In certain embodiments, the sensor connector **1905** can be detached via one hand operation, for example. Examples of connection mechanisms may be found specifically in paragraphs [0042], [0050], [0051], [0061]-[0068] and [0079], and with respect to FIGS. 8A-F, 13A-E, 19A-F, 23A-D and 24A-C of the ‘856 application, for example. The sensor system **1900** measures one or more physiological parameters of the patient, such as one of the physiological parameters described above.

The sensor connector subassembly **1905** and monitor connector **1909** may advantageously reduce the amount of unshielded area in and generally provide enhanced shielding of the electrical connection between the sensor and monitor in certain embodiments. Examples of such shielding mechanisms are disclosed in the ‘856 application in paragraphs [0043]-[0053], [0060] and with respect to FIGS. 9A-C, 11A-E, 13A-E, 14A-B, 15A-C, and 16A-E, for example.

As will be described in greater detail herein, in an embodiment, the acoustic sensor assembly **1901** includes a sensing element, such as, for example, a piezoelectric device or other acoustic sensing device. The sensing element generates a voltage that is responsive to vibrations generated by the patient, and the sensor includes circuitry to transmit the voltage generated by the sensing element to a processor for processing. In an embodiment, the acoustic sensor assembly **1901** includes circuitry for detecting and transmitting information related to biological sounds to a physiological monitor. These biological sounds may include heart, breathing, and/or digestive system sounds, in addition to many other physiological phenomena. The acoustic sensor **1915** in certain embodiments is a biological sound sensor, such as the sensors described herein. In some embodiments, the biological sound sensor is one of the sensors such as those described in the ‘883 application. In other embodiments, the acoustic sensor **1915** is a biological sound sensor such as

those described in U.S. Pat. No. 6,661,161, which is incorporated by reference herein. Other embodiments include other suitable acoustic sensors.

The attachment sub-assembly **1904** includes first and second elongate portions **1906**, **1908**. The first and second elongate portions **1906**, **1908** can include patient adhesive (e.g., in some embodiments, tape, glue, a suction device, etc.) attached to a elongate member **1910**. The adhesive on the elongate portions **1906**, **1908** can be used to secure the sensor subassembly **1902** to a patient’s skin. As will be discussed in greater detail herein, the elongate member **1910** can beneficially bias the sensor subassembly **1902** in tension against the patient’s skin and reduce stress on the connection between the patient adhesive and the skin. A removable backing can be provided with the patient adhesive to protect the adhesive surface prior to affixing to a patient’s skin.

The sensor cable **1907** is electrically coupled to the sensor subassembly **1902** via a printed circuit board (“PCB”) (not shown) in the sensor subassembly **1902**. Through this contact, electrical signals are communicated from the multi-parameter sensor subassembly to the physiological monitor through the sensor cable **1907** and the cable **1911**.

FIGS. **19B-19C** are top and bottom perspective views of a sensor including subassembly **1902** and an attachment subassembly **1904** in accordance with an embodiment of the present disclosure. The attachment subassembly **1904** generally includes lateral extensions symmetrically placed about the sensor subassembly **1902**. For example, the attachment subassembly **1904** can include single, dual or multiple wing-like extensions or arms that extend from the sensor subassembly **1902**. In other embodiments, the attachment subassembly **1902** has a circular or rounded shape, which advantageously allows uniform adhesion of the attachment subassembly **1904** to an acoustic measurement site. The attachment subassembly **1904** can include plastic, metal or any resilient material, including a spring or other material biased to retain its shape when bent. In the illustrated embodiment, the attachment subassembly **1904** includes a first elongate portion **1906**, a second elongate portion **1908**, an elongate member **1910** and a button **1912**. As will be discussed, in certain embodiments the attachment subassembly **1904** or portions thereof are disposable and/or removably attachable from the sensor subassembly **1902**. The button **1910** mechanically couples the attachment subassembly **1904** to the sensor subassembly **1902**. The attachment subassembly **1904** is described in greater detail below with respect to FIGS. **9A-9D**. The attachment subassembly **1904** may also be referred to as an attachment element herein.

In one embodiment, the sensor subassembly **1902** is configured to be attached to a patient and includes a sensing element configured to detect bodily sounds from a patient measurement site. The sensing element may include a piezoelectric membrane, for example, and is supported by a support structure such as a generally rectangular support frame **1918**. The piezoelectric membrane is configured to move on the frame in response to acoustic vibrations, thereby generating electrical signals indicative of the bodily sounds of the patient. An electrical shielding barrier (not shown) may be included which conforms to the contours and movements of the piezoelectric element during use. In the illustrated embodiment, additional layers are provided to help adhere the piezoelectric membrane to the electrical shielding barrier **1927**. Embodiments of the electrical shielding barrier are described below with respect to FIGS. **3A-B** and FIGS. **5A-B**, FIGS. **21-22**, for example.

Embodiments of the sensor subassembly **1902** also include an acoustic coupler **1914**, which advantageously

improves the coupling between the source of the signal to be measured by the sensor (e.g., the patient's skin) and the sensing element. The acoustic coupler **1914** of one embodiment includes a bump positioned to apply pressure to the sensing element so as to bias the sensing element in tension. The acoustic coupler **1914** can also provide electrical isolation between the patient and the electrical components of the sensor, beneficially preventing potentially harmful electrical pathways or ground loops from forming and affecting the patient or the sensor.

The sensor subassembly **1902** of the illustrated embodiment includes an acoustic coupler **1914** which generally envelops or at least partially covers some or all of the components of the sensor subassembly **1902**. Referring to FIG. **19C**, the bottom of the acoustic coupler **1914** includes a contact portion **1916** which is brought into contact with the skin of the patient. Embodiments of acoustic couplers are described below with respect to FIGS. **19D-19E**, **4**, and **5A-B**, for example.

FIGS. **19D-19E** are top and bottom exploded, perspective views, respectively, of the sensor subassembly **1902** of FIGS. **19A-C**.

Support Frame

The frame generally supports the various components of the sensor. For example, the piezoelectric element, electrical shielding barrier, attachment element and other components may be attached to the frame. The frame can be configured to hold the various components in place with respect to the frame and with respect to one another, thereby beneficially providing continuous operation of the sensor under a variety of conditions, such as during movement of the sensor. For example, the frame can be configured to hold one or more of the components together with a predetermined force. Moreover, the frame can include one or more features which can improve the operation of the sensor. For example, the frame can include one or more cavities which allow for the piezoelectric element to move freely and/or which amplify acoustic vibrations from bodily sounds of the patient.

In the illustrated embodiment, a PCB **1922** is mounted on the frame **1918**. The frame **1918** supports a series of layers which are generally wrapped around the underside **1942** of the frame **1918** and include, from innermost to outermost, an inner shield layer **1926**, an bonding layer **1924**, a sensing element **1920** and an outer shield layer **1928**.

As shown in FIG. **19D**, the support frame **1918** has a generally rectangular shape, as viewed from the top or bottom, although the frame shape could be any shape, including square, oval, elliptical, elongated, etc. In various embodiments, the frame **1918** has a length of from between about 5 and 50 millimeters. In one embodiment, the frame **1918** has a length of about 17 millimeters. The relatively small size of the frame **1918** can allow the sensor subassembly **1902** to be attached comfortably to contoured, generally curved portions of the patient's body. For example, the sensor subassembly **1902** can be comfortably attached to portions of the patient's neck whereas a larger frame **1918** may be awkwardly situated on the patient's neck or other contoured portion of the patient. The size of the frame **1918** may allow for the sensor subassembly **1902** to be attached to the patient in a manner allowing for improved sensor operation. For example, the relatively small frame **1918**, corresponding to a relatively smaller patient contact area, allows for the sensor subassembly **1902** to be applied with substantially uniform pressure across the patient contact area.

The frame **1918** is configured to hold the various components in place with respect to the frame. For example, in

one embodiment, the frame **1918** includes at least one locking post **1932**, which is used to lock the PCB **1922** into the sensor sub-assembly **1902**, as described below. In the illustrated embodiment, the frame **1918** includes four locking posts **1932**, for example, near each of the **1918** four corners of the frame **1918**. In other embodiments, the frame **1918** includes one, two, or three locking posts **1918**. When the locking posts **1932** are brought into contact with horns of an ultrasonic welder or a heat source, they liquefy and flow to expand over the material beneath it and then harden in the expanded state when the welder is removed. When the components of the sensor sub-assembly **1902** are in place, the locking posts **1932** are flowed to lock all components into a fixed position.

In one embodiment, the locking posts **1932** are formed from the same material as, and are integral with the frame **1918**. In other embodiments, the locking posts **1932** are not formed from the same material as the frame **1918**. For example, in other embodiments, the locking posts **1932** include clips, welds, adhesives, and/or other locks to hold the components of the sensor sub-assembly **1902** in place when the locking posts **1932** are locked into place.

With further reference to FIG. **19E**, in an assembled configuration, the PCB **1922** sits inside of an upper cavity **1930** of the frame **1918** and is pressed against the sensing element **1920** to create a stable electrical contact between the PCB **1922** and electrical contact portions of the sensing element **1920**. For example, in certain embodiments, the expanded locking posts **1932** press downward on the PCB **1922** against the sensing element **1920**, which is positioned between the PCB **1922** and the frame **1918**. In this manner, a stable and sufficient contact force between the PCB **1922** and the sensing element **1920** is maintained. For example, as the sensor assembly **1900** moves due to acoustic vibrations coming from the patient or due to other movements of the patient, the electrical contact between the PCB **1922** and the sensing element **1920** remains stable, constant, uninterrupted, and/or unchanged.

In another embodiment, the sensing element **1920** may be positioned over the PCB **1922** between the expanded locking posts **1932** and the PCB **1922**. In certain embodiments, the contact force between the PCB **1922** and the sensing element **1920** is from between about 0.5 pounds and about 10 pounds. In other embodiments, the contact force is between about 1 pound and about 3 pounds. In one embodiment, the contact force between the PCB **1922** and the sensing element **1920** is at least about 2 pounds. The bonding layer **1924** is positioned between the frame **1918** and the sensing element **1920** and allows, among other things, for the sensing element **1920** to be held in place with respect to the frame **1918** prior to placement of the PCB **1922**. The PCB **1922** and frame **1918** include corresponding cutout portions **1946**, **1948** which are configured to accept the sensor cable (not shown).

The PCB cutout portion **1946** also includes a circular portion which is configured to accept a button post **1944** positioned in the center of the cavity **1930**. The button post **1944** is configured to receive the button **1912** (FIG. **19B**). The frame **1918**, shielding layers **1926**, **1928**, adhesive layer **1924**, and sensing element **1920** each include injection holes **1935** extending through opposing sides of the respective components. Additionally, in an assembled configuration the injection holes **1935** of the various components line up with the holes **1935** of the other components such that a syringe or other device can be inserted through the holes. Glue is injected into the holes **1935** using the syringe, bonding the assembled components together.

Referring now to FIG. 19E, a lower cavity 1936 is disposed on the underside of the frame 1918 and has a depth d. In an assembled configuration, the sensing element 1920 is wrapped around the frame 1918 in the direction of the transverse axis 1938 such that the lower planar portion 1962 of the sensing element 1920 stretches across the top of the lower cavity 1936. As such, the lower cavity 1936 can serve as an acoustic chamber of the multi-parameter sensor assembly. The sensing element 1920 thus has freedom to move up into the acoustic chamber in response to acoustic vibrations, allowing for the mechanical deformation of the piezoelectric sensing material and generation of the corresponding electrical signal. In addition, the chamber of certain embodiments allows sound waves incident on the sensing element to reverberate in the chamber. As such, the sound waves from the patient may be amplified or more effectively directed to the sensing element 1920, thereby improving the sensitivity of the sensing element 1920. As such, the cavity 1936 allows for improved operation of the sensor.

The frame may include one or more contacts extending from the frame which press into corresponding contact strips of the PCB, helping to ensure a stable, relatively constant contact resistance between the PCB and the sensing element. FIG. 19F shows a top perspective view of an embodiment of a support frame 1918 including such contacts. The frame 1918 may be generally similar in structure and include one or more of the features of the frame shown in FIGS. 19D-19E, such as the locking posts 332 and the upper surface 384. The frame 1918 further includes one or more contact bumps 1920 which press into corresponding contact strips 1923 (FIG. 2E) of the PCB 1922 when the sensor sub-assembly is assembled. For example, the contact bumps 1920 may include generally narrow rectangular raised segments and may be positioned on the upper surface 1984 of the frame 1918.

The contact bumps 1920 help ensure a stable, constant contact resistance between the PCB 1922 and the sensing element 1920. The contact bumps 1920 are dimensioned to press a portion of the sensing element 1920 into the PCB 1922 when the sensor subassembly 1902 is assembled. In some embodiments, the height of the contact bumps 1920 is from about 0.1 to about 1 mm. In some embodiments, the height of the contact bumps 1920 is in the range from about 0.2 to about 0.3 mm. In one embodiment, the contact bumps 1920 have a height of about 0.26 mm. The height is generally selected to provide adequate force and pressure between the sensing element 1920 and PCB 1922.

In other embodiments, the contact bumps may have different shapes. For example, the bumps 1920 may be generally circular, oval, square or otherwise shaped such that the bumps 1920 are configured to press into corresponding contact strips 1923 on the PCB 1922. The contact strips 1923 may be shaped differently as well. For example, the strips 1923 may be shaped so as to generally correspond to the cross-sectional shape of the bumps 1920. While there are two bumps 1920 per contact strip 1923 in the illustrated embodiment, other ratios of contact bumps 1920 to contact strips 1923 are possible. For example, there may be one contact bump 1920 per contact strip 1923, or more than two contact bumps 1920 per contact strip 1923.

Referring again to FIGS. 19D-19E, the frame 1918 includes rounded edges 1934 around which the various components including the inner shield 1926, the bonding layer 1924, the sensing element 1920, and the outer shield 1928 wrap in the direction of the transverse axis 1938. The rounded edges 1934 help assure that the sensing element 1920 and other layers 1926, 1924, 1928 extend smoothly

across the frame 3116, and do not include wrinkles, folds, crimps and/or unevenness. Rounded edges 1934 advantageously allow uniform application of the sensing element 1920 to the frame 1918, which helps assure uniform, accurate performance of the sensor assembly 1902. In addition, the dimensions of the rounded corners and the upper cavity 1930 can help to control the tension provided to the sensing element 1920 when it is stretched across the frame 1918.

The frame 1918 may have different shapes or configurations. For example, in some embodiments, the frame 1918 does not include a recess 1930 and the PCB 1922 sits on top of the frame 1918. In one embodiment the edges 1934 are not rounded. The frame 1918 may be shaped as a board, for example. The frame 1918 may include one or more holes. For example, the frame 1918 includes four elongate bars connected to form a hollow rectangle in one configuration. In various embodiments, the frame 1918 may not be generally rectangular but may instead be generally shaped as a square, circle, oval or triangle, for example. The shape of the frame 1918 may be selected so as to advantageously allow the sensor subassembly 1902 to be applied effectively to different areas of the body, for example. The shape of the frame 1918 may also be selected so as to conform to the shape of one or more of the other components of the sensor system 1900 such as the sensing element 1920.

In addition, in some embodiments, one or more of the inner shield 1926, the bonding layer 1924, the sensing layer 1920 and the outer shield 1928 are not wrapped around the frame 1918. For example, in one embodiment, one or more of these components are generally coextensive with and attached to the underside of the frame 1918 and do not include portions which wrap around the edges 1934 of the frame.

Sensing Element

The sensing element 1920 of certain embodiments is configured to sense acoustic vibrations from a measurement site of a medical patient. In one embodiment, the sensing element 1920 is a piezoelectric film, such as described in U.S. Pat. No. 6,661,161, incorporated in its entirety by reference herein, and in the '883 application. Referring still to FIGS. 19D-19E, the sensing element 1920 includes upper portions 1972 and lower planar portion 1962. As will be discussed, in an assembled configuration, the top of the upper portions 1972 include electrical contacts which contact electrical contacts on the PCB 1922, thereby enabling transmission of electrical signals from the sensing element 1920 for processing by the sensor system. The sensing element 1920 can be formed in a generally "C" shaped configuration such that it can wrap around and conform to the frame 1918. Sensing elements in accordance with embodiments described herein can also be found in the '883 application. In some embodiments, the sensing element 1920 includes one or more of crystals of tourmaline, quartz, topaz, cane sugar, and/or Rochelle salt (sodium potassium tartrate tetrahydrate). In other embodiments, the sensing element 1920 includes quartz analogue crystals, such as berlinite (AlPO₄) or gallium orthophosphate (GaPO₄), or ceramics with perovskite or tungsten-bronze structures (BaTiO₃, SrTiO₃, Pb(ZrTi)O₃, KNbO₃, LiNbO₃, LiTaO₃, BiFeO₃, Na_xWO₃, Ba₂NaNb₅O₁₅, Pb₂KNb₅O₁₅).

In other embodiments, the sensing element 1920 is made from a polyvinylidene fluoride plastic film, which develops piezoelectric properties by stretching the plastic while placed under a high pooling voltage. Stretching causes the film to polarize and the molecular structure of the plastic to align. For example, stretching the film under or within an electric field causes polarization of the material's molecules

into alignment with the field. A thin layer of conductive metal, such as nickel-copper or silver is deposited on each side of the film as electrode coatings, forming electrical poles. The electrode coating provides an electrical interface between the film and a circuit.

In operation, the piezoelectric material becomes temporarily polarized when subjected to a mechanical stress, such as a vibration from an acoustic source. The direction and magnitude of the polarization depend upon the direction and magnitude of the mechanical stress with respect to the piezoelectric material. The piezoelectric material will produce a voltage and current, or will modify the magnitude of a current flowing through it, in response to a change in the mechanical stress applied to it. In one embodiment, the electrical charge generated by the piezoelectric material is proportional to the change in mechanical stress of the piezoelectric material.

Piezoelectric material generally includes first and second electrode coatings applied to the two opposite faces of the material, creating first and second electrical poles. The voltage and/or current through the piezoelectric material are measured across the first and second electrical poles. Therefore, stresses produced by acoustic waves in the piezoelectric material will produce a corresponding electric signal. Detection of this electric signal is generally performed by electrically coupling the first and second electrical poles to a detector circuit. In one embodiment, a detector circuit is provided with the PCB 1922, as described in greater detail below.

By selecting the piezoelectric material's properties and geometries, a sensor having a particular frequency response and sensitivity can be provided. For example, the piezoelectric material's substrate and coatings, which generally act as a dielectric between two poles, can be selected to have a particular stiffness, geometry, thickness, width, length, dielectric strength, and/or conductance. For example, in some cases stiffer materials, such as gold, are used as the electrode. In other cases, less stiff materials, such as silver, are employed. Materials having different stiffness can be selectively used to provide control over sensor sensitivity and/or frequency response.

The piezoelectric material, or film, can be attached to, or wrapped around, a support structure, such as the frame 1918. As shown in FIGS. 19D-19E, the geometry of the piezoelectric material can be selected to match the geometry of the frame. Overall, the sensor can be optimized to pick up, or respond to, a particular desired sound frequency, and not other frequencies. The frequency of interest generally corresponds to a physiological condition or event that the sensor is intended to detect, such as internal bodily sounds, including, cardiac sounds (e.g., heart beats, valves opening and closing, fluid flow, fluid turbulence, etc.), respiratory sounds (e.g., breathing, inhalation, exhalation, wheezing, snoring, apnea events, coughing, choking, water in the lungs, etc.), or other bodily sounds (e.g., swallowing, digestive sounds, gas, muscle contraction, joint movement, bone and/or cartilage movement, muscle twitches, gastro-intestinal sounds, condition of bone and/or cartilage, etc.).

The surface area, geometry (e.g., shape), and thickness of the piezoelectric material 1920 generally defines a capacitance. The capacitance is selected to tune the sensor to the particular, desired frequency of interest. Furthermore, the frame 1918 is structured to utilize a desired portion and surface area of the piezoelectric material.

The capacitance of the sensor can generally be expressed by the following relationship: $C = \epsilon S/D$, where C is the sensor's capacitance, ϵ is the dielectric constant associated

with the material type selected, S is the surface area of the material, and D is the material thickness (e.g., the distance between the material's conductive layers). In one embodiment, the piezoelectric material (having a predetermined capacitance) is coupled to an sensor impedance (or resistance) to effectively create a high-pass filter having a predetermined high-pass cutoff frequency. The high-pass cutoff frequency is generally the frequency at which filtering occurs. For example, in one embodiment, only frequencies above the cutoff frequency (or above approximately the cutoff frequency) are transmitted.

The amount of charge stored in the conductive layers of the piezoelectric material 1920 is generally determined by the thickness of its conductive portions. Therefore, controlling material thickness can control stored charge. One way to control material thickness is to use nanotechnology or MEMS techniques to precisely control the deposition of the electrode layers. Charge control also leads to control of signal intensity and sensor sensitivity. In addition, as discussed above, mechanical dampening can also be provided by controlling the material thickness to further control signal intensity and sensor sensitivity.

In addition, controlling the tension of the sensing element 1920 in the region where the mechanical stress (e.g., mechanical stress due to acoustic vibration from a patient's skin) is incident upon the sensing element 1920 can serve to improve the sensitivity of the sensing element 1920 and/or the coupling between the source of the signal (e.g., the patient's skin) and the sensing element 1920. This feature will be discussed in greater detail below with respect to the coupler 1914.

One embodiment of a piezoelectric sensing element 2000 is provided in FIGS. 20A-C. The sensing element 2000 includes a substrate 2002 and coatings 2004, 2006 on each of its two planar faces 2008, 2010. The planar faces 2008, 2010 are substantially parallel to each other. At least one through hole 2012 extends between the two planar faces 2008, 2010. In one embodiment, the sensing element 2000 includes two or three through holes 2012.

In one embodiment, a first coating 2004 is applied to the first planar face 2008, the substrate 2002 wall of the through holes 2012, and a first conductive portion 2014 of the second planar face 2010, forming a first electrical pole. By applying a first coating 2004 to the through holes 2012, a conductive path is created between the first planar face 2008 and the first conductive portion 2014 of the sensing element 2000. A second coating 2006 is applied to a second conductive portion 2016 of the second planar face 2010 to form a second electrical pole. The first conductive portion 2014 and second conductive portion 2016 are separated by a gap 2018 such that the first conductive portion 2014 and second conductive portion 2016 are not in contact with each other. In one embodiment, the first conductive portion 2014 and second conductive portion 2016 are electrically isolated from one another.

In some embodiments, the first and second conductive portions 2014, 2016 are sometimes referred to as masked portions, or coated portions. The conductive portions 2014, 2016, can be either the portions exposed to, or blocked from, material deposited through a masking, or deposition process. However, in some embodiments, masks aren't used. Either screen printing, or silk screening process techniques can be used to create the first and second conductive portions 2014, 2016.

In another embodiment, the first coating 2004 is applied to the first planar face 2008, an edge portion of the substrate 2002, and a first conductive portion 2014. By applying the

first coating **2004** to an edge portion of the substrate **2002**, through holes **1012** can optionally be omitted.

In one embodiment, the first coating **2004** and second coating **2006** are conductive materials. For example, the coatings **2004**, **2006** can include silver, such as from a silver deposition process. By using a conductive material as a coating **2004**, **2006**, the multi-parameter sensor assembly can function as an electrode as well.

Electrodes are devices well known to those of skill in the art for sensing or detecting the electrical activity, such as the electrical activity of the heart. Changes in heart tissue polarization result in changing voltages across the heart muscle. The changing voltages create an electric field, which induces a corresponding voltage change in an electrode positioned within the electric field. Electrodes are typically used with echo-cardiogram (EKG or ECG) machines, which provide a graphical image of the electrical activity of the heart based upon signal received from electrodes affixed to a patient's skin.

Therefore, in one embodiment, the voltage difference across the first planar face **2008** and second planar face **2010** of the sensing element **2000** can indicate both a piezoelectric response of the sensing element **2000**, such as to physical aberration and strain induced onto the sensing element **2000** from acoustic energy released from within the body, as well as an electrical response, such as to the electrical activity of the heart. Circuitry within the sensor assembly and/or within a physiological monitor (not shown) coupled to the sensor assembly distinguish and separate the two information streams. One such circuitry system is described in U.S. Provisional No. 60/893,853, filed Mar. 8, 2007, titled, "Multi-parameter Physiological Monitor," which is expressly incorporated by reference herein.

Referring still to FIGS. **20A-C**, the sensing element **2000** is flexible and can be wrapped at its edges, as shown in FIG. **20C**. In one embodiment, the sensing element **2000** is the sensing element **1920** wrapped around the frame **1918**, as shown in FIGS. **19D** and **19E**. In addition, by providing both a first conductive portion **2014** and a second conductive portion **2016**, both the first coating **2004** and second coating **2006** and therefore the first electrical pole of and the second electrical pole of the sensing element **2000** can be placed into direct electrical contact with the same surface of the PCB, such as the PCB **1922** as shown FIGS. **5A-B** below. This advantageously provides symmetrical biasing of the sensing element **2000** under tension while avoiding uneven stress distribution through the sensing element **2000**.

Bonding Layer

Referring back to FIGS. **19D-19E**, the bonding layer **1924** (sometimes referred to as an insulator layer) of certain embodiments is an elastomer and has adhesive on both of its faces. In other embodiments, the bonding layer **1924** is a rubber, plastic, tape, such as a cloth tape, foam tape, or adhesive film, or other compressible material that has adhesive on both its faces. For example, in one embodiment, the bonding layer **1924** is a conformable polyethylene film that is double coated with a high tack, high peel acrylic adhesive. The bonding layer **1924** in some embodiments is about 2, 4, 6, 8 or 10 millimeters thick.

The bonding layer **1924** advantageously forms a physical insulation layer or seal between the components of the sensor subassembly **1902** preventing substances entering and/or traveling between certain portions of the sensor subassembly **1902**. In many embodiments, for example, the bonding layer **1924** forms a physical insulation layer that is water resistant or water proof, thereby providing a water-proof or water-resistant seal. The water-resistant properties

of the bonding layer **1924** provides the advantage of preventing moisture from entering the acoustic chamber or lower cavity **1936**. In certain embodiments, the sensing element **1920**, the bonding layer **1924** and/or the shield layers **1926**, **1928** (described below) form a water resistant or water proof seal. The seal can prevent moisture, such as perspiration, or other fluids, from entering portions of the sensor subassembly **1902**, such as the cavity **1936** when worn by a patient. This is particularly advantageous when the patient is wearing the multi-parameter sensor assembly **1900** during physical activity. The water-resistant seal prevents current flow and/or a conductive path from forming from the first surface of the sensing element **1920** to its second surface or vice versa as a result of patient perspiration or some other moisture entering and/or contacting the sensing element **1920** and/or sensor assembly **1915**.

The bonding layer **1924** can also provide electrical insulation between the components of the sensor subassembly **1902**, preventing the flow of current between certain portions of the sensor subassembly **1902**. For example, the bonding layer **1924** also prevents the inside electrical pole from shorting to the outside electrical pole by providing electrical insulation or acting as an electrical insulator between the components. For example, in the illustrated embodiment, the bonding layer **1924** provides electrical insulation between the sensing element **1920** and the inner shield layer **1926**, preventing the inside electrical pole of the sensing element **1920** from shorting to the outside electrical pole. In another embodiment, a bonding layer is placed between the outer surface of the sensing element **1920** and the outer shield layer **1928**.

The elasticity or compressibility of the bonding layer **1924** can act as a spring and provide some variability and control in the pressure and force provided between the sensing element **1920** and PCB **1922**. In some embodiments, the sensor assembly does not include a bonding layer **1924**.
Electrical Noise Shielding Barrier

An electrical noise shielding barrier can electrically shield the electrical poles of the sensing element from external electrical noises. In some embodiments the electrical shielding barrier can include one or more layers which form a Faraday cage around a piezoelectric sensing element, and which distribute external electrical noise substantially equally to the electrical poles of the piezoelectric sensing element. In addition, the shielding barrier flexibly conforms to the surface shape of the piezoelectric element as the surface shape of the piezoelectric element changes, thereby improving the shielding and sensor performance.

Referring still to FIGS. **19D-19E**, the electrical shielding barrier **1927** of the illustrated embodiment includes first and second shield layers **1926**, **1928** (also referred to herein as inner and outer shield layers **1926**, **1928**) which form a Faraday cage (also referred to as a Faraday shield) which encloses the sensing element **1920** and acts to reduce the effect of noise on the sensing element from sources such as external static electrical fields, electromagnetic fields, and the like. As will be described, one or more of the inner and outer shield layers **1926**, **1928** advantageously conform to the contours of the sensing element **1920** during use, allowing for enhanced shielding of the sensing element from external electrical noise.

The inner and outer shield layers **1926**, **1928** include conductive material. For example, the inner and outer shield layers **1926**, **1928** include copper in certain embodiments and are advantageously formed from a thin copper tape such that the layers can conform to the shape, contours and topology of the sensor element **1920** and the frame **1918**. In

some configurations, other materials (e.g., other metals) or other combinations of materials can be used. Moreover, as described herein with respect to FIGS. 19-22, the electrical shielding barrier 1927 or portions thereof, such as one or more of the first and second shield layers 1926, 1928, can be formed from piezoelectric films. In such embodiments, the sensor 1915 can include first and second piezoelectric films arranged in a stack, and the shielding barrier 1927 can be formed from the outer electrode of each film in the stack.

In various embodiments, one or more of the inner and outer shield layers 1926, 1928 are from between about 0.5 micrometer and 10 micrometers thick. For example, the shield layers 1926, 1928, may be from between about 1.5 and about 6 micrometers thick. In one embodiment, the inner and outer shield layers 1926, 1928 include copper tape about 3 micrometers thick. In yet other embodiments, the shield layers 1926, 1928 may be greater than 10 micrometers thick or less than 0.5 micrometers thick. In general, the thickness of the shield layer 1926, 1928 is selected to provide improved electrical shielding while allowing for the shield layers 1926, 1928 to conform to the sensor element 1920 and/or the frame 1918. The inner shield layer 1926 includes an adhesive on the inside surface 1952 such that it can adhere to the frame 1918. The inner shield layer 1926 adheres directly to the frame 1918 and advantageously conforms to the contours of the frame such as the rounded edges 1934 and the lower cavity 1936, adhering to the surface 1950 defining the base of the cavity 1936. The bonding layer 1924 (e.g., a tape adhesive) is wrapped around and generally conforms to the contours of the inner shield layer 1926 and the frame 1918. The sensing element 1920 is wrapped around the bonding layer 1924, the inner shield layer 1924 and the frame 1918. The outer shield layer 1928 is wrapped around and advantageously conforms to the contours of the sensing element 1920 and the frame 1918. In certain embodiments, a bonding or insulating layer is positioned between the sensing element 1920 and the outer shielding layer 1928 as well. As such, the sensing element 1920 is sandwiched between and enclosed within the inner and outer shield layers 1926, 1928 which form a Faraday cage around the sensing element 1920. The configuration of the shield layers 1926, 1928, the sensing element 1920 and the bonding layer 1924 will be described in greater detail below with respect to FIGS. 5A-B.

In certain embodiments, the shield layers 1926, 1928 are coupled to a common potential (e.g., ground) or are otherwise operatively coupled, and each of the shield layers 1926, 1928 are also electrically (e.g., capacitively) coupled to one of the poles of the sensing element 1920. For example, the shielding layer 1926 may be capacitively coupled to the first electrode of the sensing element 1920, and the shielding layer 1928 may be capacitively coupled to the second electrode of the sensing element 1920.

As discussed, the electrical shielding barrier 1927 such as the Faraday cage formed by the inner and outer shield layers 1926, 1928 helps to reduce the effect of noise electrical noise on the sensing element 1920 from sources such as external static electrical fields and electromagnetic fields, thereby lowering the noise floor, providing better noise immunity, or both. For example, the electrical shielding barrier 1927 allows for the removal of electrical interference or noise incident directed towards the sensing element 1920 while allowing the non-noise component of the sensed signal indicative of bodily sounds to be captured by the sensor 1915. For example, in one embodiment the sensing element 1920 is a piezoelectric film such as one of the piezoelectric films described herein having positive and negative electri-

cal poles and configured in a differential mode of operation. The electrical shielding barrier 1927 acts to balance the effect of the noise by distributing at least a portion of the noise substantially equally to the positive and negative electrical poles of the piezoelectric element. In some embodiments, the electrical shielding barrier 1927 distributes the noise equally to both the positive and negative poles. Moreover, the noise signals distributed to the positive and negative electrical poles are substantially in phase or actually in phase with each other. For example, the noise signals distributed to the positive and negative poles are substantially similar frequencies and/or amplitudes with substantially no phase shift between them.

For example, in certain embodiments, noise incident on the shielding barrier 1927 is substantially equally distributed to each of the shielding layers 1926, 1928 because these layers are at a common potential (e.g., ground). The substantially equally distributed noise may then be coupled (e.g., capacitively coupled) to the poles of the sensing element 1920. In certain embodiments, at least some of the external electrical noise is shunted or otherwise directed to ground by the shield layers 1926, 1928 instead of, or in addition to, being distributed to the poles of the sensing element 1920.

Because the noise signal components on the positive and negative poles are substantially in phase, the difference between the noise components on the respective poles is negligible or substantially negligible. On the other hand, the difference between the differential non-noise sensor signal components indicative of bodily sounds on the positive and negative poles will be non-zero because the sensing element is configured in a differential mode. As such, the noise signals can advantageously be removed or substantially removed through a common-mode rejection technique.

For example, a common-mode rejection element may receive a signal including the combined noise and non-noise sensor signal components of the positive and negative poles, respectively. The common-mode rejection element is configured to output a value indicative of the difference between the combined signal on the positive pole and the combined signal on the negative pole. Because the difference between the noise signals is negligible, the output of the common-mode rejection element will be substantially representative of the non-noise component of the sensor signal and not include a significant noise component. The common mode rejection element may include, for example, an operational amplifier. In one embodiment, for example, three operational amplifiers (not shown) are used and they are disposed on the PCB 1922.

Because the shielding layers 1926, 1928 conform to the topology of the frame 1918 and the sensing element 1920, the shielding layers 1926, 1928 are physically closer to the electrical poles of the sensing element 1920 and are more uniformly displaced from the sensing element 1920. Moreover, the outer shield layer 1928 of certain embodiments actively moves with and conforms to the contours of the sensing element 1920 during use, such as when the sensor assembly is placed against the skin or when the sensing element 1920 is moving due to acoustic vibrations. For example, when placed against the skin, the coupling element 1958 pushes against both the outer shielding layer 1928 of the shielding barrier 1927 and the sensing element 1920, causing them to curve along the inside surface of the coupling element 1958 (FIG. 5A). Because the cage is flexible and can conform to the movement of the shielding element 1920, the shielding performance and sensor performance is improved. This arrangement provides advantages

such as for example, for the noise signals to be more accurately and evenly distributed to the positive and negative electrical poles of the sensing element 1920 by the shielding layers 1926, 1928, thereby providing enhanced noise reduction. This arrangement can also provide for improved manufacturability and a more stream-lined design.

Alternative configurations for the electrical shielding barrier 1927 are possible. For example, the inner shield layer may not include an adhesive layer and may, for example, be held in place against the frame 1918 by pressure (e.g., from the locking posts 1932). The outer shield 1928 may also include an adhesive layer in some embodiments. In various other embodiments, the shield layers 1926, 1928 may include other materials such as other types of metals. One or more of the shield layers may be relatively rigid in some configurations. In one embodiment, an insulating layer or bonding layer is disposed between sensing element 1920 and the outer shield layer 1928. In some embodiments, the inner shield layer 1926 actively conforms to the contours of the sensing element 1920 during use in addition to the outer shield layer 1928. In another embodiment, the inner shield layer 1926 actively conforms to the sensing element 1920 during use and the outer shield layer 1928 does not. In yet other embodiments, the sensor assembly 1901 does not include an electrical shielding barrier 1927.

Acoustic Coupler

The sensor may also include an acoustic coupler or biasing element, which advantageously improves the coupling between the source of the signal to be measured by the sensor (e.g., the patient's skin) and the sensing element. The acoustic coupler generally includes a coupling portion positioned to apply pressure to the sensing element so as to bias the sensing element in tension. For example, the acoustic coupler may include one or more bumps, posts or raised portions which provide such tension. The bumps, posts or raised portions may be positioned on the inner surface of the coupler, the outer surface of the coupler, or both and may further act to evenly distribute pressure across the sensing element. In addition, the acoustic coupler can be further configured to transmit bodily sound waves to the sensing element. The acoustic coupler can also be configured to provide electrical isolation between the patient and the electrical components of the sensor.

In the illustrated embodiment, the acoustic coupler 1914 houses the other components of the sensor subassembly including the frame 1918, the PCB 1922, the shield layers 1926, 1928, the bonding layers 1924 and the sensing element 1920. The acoustic coupler 1914 includes a non-conductive material or dielectric. As shown, the acoustic coupler 1914 generally forms a dielectric barrier between the patient and the electrical components of the sensor assembly 1901. As such, the acoustic coupler 1914 provides electrical isolation between the patient and the electrical components of the sensor subassembly 1902. This is advantageous in avoiding potential harmful electrical pathways or ground loops forming between the patient and the sensor.

As shown in FIGS. 19D-19E, the acoustic coupler 1914 is formed in a hollow shell capable of housing the components of the other sensor subassembly 1902. Referring to FIG. 19D, the acoustic coupler 1914 of the illustrated embodiment also includes recesses 1956 and holes 1952 capable of receiving and securing the button 1912 (FIG. 19B) and portions of the elongate member 1910 (FIG. 19B) of the attachment subassembly 1904.

FIG. 21 is a cross-sectional view of the acoustic coupler 1914 taken along the line 21-21. In certain embodiments, the acoustic coupler includes a bump or protrusion on the inner

surface of the coupler 1914 and configured to advantageously bias the sensing membrane in tension. For example, a coupling element 1958 is disposed on the on the interior bottom portion of the acoustic coupler 1914 and which biases the sensing element 1920 in tension. The coupling element 1958 of the illustrated embodiment is a generally rectangular bump which extends by a height h above the cavity 1960 which is formed on the interior bottom of the acoustic coupler 1914. The coupling element 1958 is centered about and extends along the longitudinal axis 1940 (FIGS. 19D and 19E) from near the front of the acoustic coupler 1914 to near the back of the acoustic coupler 1914. In the illustrated embodiment, the coupling element 1958 is about $\frac{1}{4}$ of the width of the acoustic coupler 1914 along the transverse axis 1938. As will be discussed in greater detail below with respect to FIG. 22A-B, the coupling element 1958 can advantageously bias the sensing element 1920 in tension by applying pressure to the sensing element 1920. Because the sensing element 1920 may be generally taut in tension under the pressure of the coupling bump 1958, the sensing element 1920 will be mechanically coupled to the coupling bump 1958 and responsive to acoustic vibrations travelling through the coupler 1914 to the sensing element 1920, thereby providing improved coupling between the patient's skin and the sensing element 1920. As such, the acoustic coupler 1914 provides for improved measurement sensitivity, accuracy, or both, among other advantages.

The acoustic coupler 1914 is further configured to transmit bodily sound waves to the sensing element 1920. The coupler 1914 can further include a portion disposed on the outer surface of the coupler 1914 and which is configured to contact the skin during use. For example, the acoustic coupler 1914 can include an outer protrusion, bump or raised portion on the outer surface. Referring to FIGS. 19E and 4, the underside of the acoustic coupler 1914 includes portion 1916 which is configured to contact the skin of the patient and can provides contact between the skin and the acoustic coupler 1914. Acoustic vibrations from the skin will be incident on the portion 1916, travel through the acoustic coupler to the coupling bump 1958 and eventually be incident on the sensing element 1920 held in tension by the bump 1958. In addition, the contact portion 1916 may, in conjunction with the coupling element 1958 or on its own, also help to improve the coupling between the skin and the sensing element 1920. For example, when pressed against the skin, the contact portion 1916 may push a portion of the inner surface of the coupler 1914, such as the coupling element 1958, into the sensing element 1920, advantageously holding the sensing element 1920 in tension. As shown, the contact portion 1916 of the illustrated embodiment includes a semi-cylindrical bump mounted generally underneath the coupling element 1958. Similar to the coupling element 1958, the contact portion 1916 is centered about and extends along the longitudinal axis 1940 from near the front of the acoustic coupler 1914 to near the back of the acoustic coupler 1914. Moreover, the acoustic coupler 1914 acts to evenly distribute pressure to the sensing element 1920 during use. For example, because the coupling element 1958 and the portion 1916 are generally positioned such that they are centered with respect to surface of the sensing element 1920, pressure will be distributed symmetrically and/or evenly across the sensing element 1920.

Referring to FIG. 19E, a pair of slots 1964 are disposed on either end of the contact portion 1916 and each run generally along the transverse axis from near the left side of the acoustic coupler 1914 to the right side of the acoustic coupler 1914. The slots serve to decouple a segment 1966 of

the bottom of the acoustic coupler 1914 including the coupling element 1958 and the contact portion 1916 from the remainder of the acoustic coupler 1914. As such, the segment 1966 can move at least partially independent from the rest of the acoustic coupler 1914 in response to acoustic vibrations on the skin of the patient, thereby efficiently transmitting acoustic vibrations to the sensing element 1920. The acoustic coupler 1914 of certain embodiments includes an elastomer such as, for example, rubber or plastic material.

In an alternative embodiment of the acoustic coupler 1914, for example, the acoustic coupler 1914 does not include a hollow shell and does not house the other components of the sensor subassembly. For example, the coupler 1914 may include a single planar portion such as, for example, a board which couples to the underside of the frame 1918 such that the shielding layers 1926, 1928, the sensing element 1920 and the bonding layer 1924 are positioned between the coupler 1914 and the frame 1918. In some configurations, the coupler 1914 is positioned between the frame 1918 and one or more of the shielding layers 1926, 1928, the sensing element 1920 and the bonding layer 1924. Moreover, the acoustic coupler 1914 may include a dielectric material, which advantageously electrically isolates the electrical components of the sensor subassembly 1902 from the patient. For example, the dielectric layer may ensure that there is no electrical connection or continuity between the sensor assembly and the patient.

In certain embodiments, portions of the sensor assembly such as, for example, the acoustic coupler 1914 may include a gel or gel-like material. The gel may provide beneficial acoustic transmission, for example, serving to enhance the coupling between the acoustic vibrations from the patient's skin and the sensing element 1920. The gel may provide acoustic impedance matching, for example, between the skin and the sensor. For example, the gel may serve to reduce the impedance mismatch from potential skin-to-air and air-to-sensing element discontinuity, thereby reducing potential reflections and signal loss. The gel may be embedded in a portion of the acoustic coupler 1914. For example, one or more of the coupling element 1958 and the contact portion 1916 may include a gel or gel-like material. The acoustic coupler 1914 may include an embedded gel in certain embodiments where one or more of the coupling element 1958 and the contact portion 1916 are not included. For example, the entire patient contact portion of the acoustic coupler 1914 may include gel material extending substantially from the patient contact surface to the interior of the coupler 1914 across the contact portion. One or more columns of gel material may extend from the patient contact surface of the coupler 1914 to the interior of the coupler 1914 in other embodiments. In yet further embodiments, the gel is not embedded in the acoustic coupler 1914 but is added to the skin directly. In one embodiment, the gel is embedded in the acoustic coupler 1914 and is configured to be released from the coupler 1914 when the sensor assembly is applied to the patient. For example, gel can be filled in one or more cavities of the acoustic coupler 1914 prior to use wherein the cavities are configured to open and release the gel when the coupler is pressed against the skin.

FIGS. 22A-B are cross-sectional views of the sensor subassembly 1902 of FIG. 19 along the lines 22A-22A and 22B-22B, respectively. As shown, the inner copper shield 1926 is positioned as the inner most of the shield layers 1926, 1928, the bonding layer 1924 and the sensing element 1920. Referring to FIGS. 19D-E and FIGS. 22A-B, the four tabs 1968 of the inner copper shield 1926 are flat and extend across the top of the frame recess 1930 and the four corners

of the top surface of the PCB (not shown in FIGS. 22A-B) which sits in the frame recess 1930. The bonding layer 1924 is wrapped around the inner copper shield 1926. The upper portions 1970 of the bonding layer 1924 bend downward to conform to the shape of the frame 1918 such that they extend across and contact the bottom of the frame cavity 1930. The sensing element 1920 is wrapped around the bonding layer 1924 and the upper portions 1972 of the sensing element 1920 also bend downward to conform to the shape of the frame 1918. As such, the upper portions 1972 of the sensing element 1920 extend across the bottom of the frame cavity 1930 and are in contact with the bottom of the PCB 1922 and the top surface of the bonding layer 1924. The outer copper layer 1928 is wrapped around the sensing element 1920 and the upper planar portions 1973 of the outer copper shield 1928 are flat, extend across the top of the frame recess 1930, and are in contact with the top surface of the PCB (not shown).

The shield layers 1926, 1928, the bonding layer 1924 and the sensing element 1920 wrap around the rounded edges 1934 of the frame 1918. The lower planar portions 1974, 1976 of the inner shield layer 1926 and the bonding layer 1924 bend upwards so as to extend across the bottom surface 1950 of the frame 1918. The lower planar portions 1962, 1980 of the sensing element 1920 and the outer shield layer 1928, on the other hand, extend between the lower frame cavity 1936 and the coupler cavity 1960. Moreover, the lower planar portions 1962, 1980 of the sensing element 1920 and the outer shield layer 1928 extend across the top of the coupling portion 1958. Because the coupler portion 1958 extends slightly above the coupler cavity 1960 into the lower frame cavity 1936 by the distance h , the sensing element 1920 is advantageously biased in tension improving the sensitivity of the sensing element 1920, the coupling of the sensing element 1920 to acoustic vibrations in the skin of the patient (not shown), or both.

In various embodiments, the components of the sensor subassembly 1902 may be arranged differently. For example, the components may be combined such that the overall assembly include fewer discrete components, simplifying manufacturability. In one embodiment, one or more of the shielding layers 1926, 1928, the bonding layer 1924 and the sensing element 1920 may include an integral portion (e.g., a multi-layered film). In some embodiments, more than one bonding layer 1924 is used. In one embodiment, adhesive layers are formed on one or more of the shielding layers 1926, 1928 and the sensing element 1920, and no separate bonding layer 1924 is present. In another embodiment, the various layers are held together by pressure (e.g., from the contact posts 1932 and/or PCB) instead of through the use of adhesives.

Referring still to FIGS. 19D-E and 22A-B, a method for attaching the shielding layers 1926, 1928, the bonding layer 1924, the sensing element 1920 and the PCB 1922 to the frame 1918 includes providing the inner shield 1926 and attaching it to the frame 1918. The sensing element 1920 and bonding layer 1924 are provided and also attached to the frame 1918. A printed circuit board 1922 is then provided. The printed circuit board 1922 is placed on top of the sensing element 1920 such that a first edge 1980 of the printed circuit board 1922 is placed over a first conductive portion of the sensing element 1920, and a second edge 1982 of the printed circuit board 1922 is placed over a second conductive portion of the sensing element 1920.

The printed circuit board 1922 is pressed down into the sensing element 1920 in the direction of the frame 1918. As the printed circuit board 1922 is pressed downward, the

contact bumps (not shown) of the frame 1918 push the bonding layer 1924 and sensing element 1920 into contact strips located along the first and second sides or edges 1980, 1982 of the printed circuit board 1922. The contact strips of the printed circuit board 1922 are made from conductive material, such as gold. Other materials having a good electro negativity matching characteristic to the conductive portions of the sensing element 1920, may be used instead. The elasticity or compressibility of the bonding layer 1924 acts as a spring, and provides some variability and control in the pressure and force provided between the sensing element 1920 and printed circuit board 1922.

Once the outer shield 1928 is provided and attached to the frame 1918, a desired amount of force is applied between the PCB 1922 and the frame 1918 and the locking posts 1932 are vibrated or ultrasonically or heated until the material of the locking posts 1932 flows over the PCB 1922. The locking posts 1932 can be welded using any of a variety of techniques, including heat staking, or placing ultrasonic welding horns in contact with a surface of the locking posts 1932, and applying ultrasonic energy. Once welded, the material of the locking posts 1932 flows to a mushroom-like shape, hardens, and provides a mechanical restraint against movement of the PCB 1922 away from the frame 1918 and sensing element 1920. By mechanically securing the PCB 1922 with respect to the sensing element 1920, the various components of the sensor sub-assembly 1902 are locked in place and do not move with respect to each other when the multi-parameter sensor assembly is placed into clinical use. This prevents the undesirable effect of inducing electrical noise from moving assembly components or inducing instable electrical contact resistance between the PCB 1922 and the sensing element 1920. In certain embodiments, the locking posts 1932 provide these advantages substantially uniformly across multiple sensors.

Therefore, the PCB 1922 can be electrically coupled to the sensing element 1920 without using additional mechanical devices, such as rivets or crimps, conductive adhesives, such as conductive tapes or glues, like cyanoacrylate, or others. In addition, the mechanical weld of the locking posts 1932 helps assure a stable contact resistance between the PCB 1922 and the sensing element 1920 by holding the PCB 1922 against the sensing element 1920 with a constant pressure, for example, and/or preventing movement between the PCB 1922 and the sensing element 1920 with respect to each other.

The contact resistance between the sensing element 1920 and PCB 1922 can be measured and tested by accessing test pads on the PCB 1922. For example, in one embodiment, the PCB 1922 includes three discontinuous, aligned test pads that overlap two contact portions between the PCB 1922 and sensing element 1920. A drive current is applied, and the voltage drop across the test pads is measured. For example, in one embodiment, a drive current of about 100 mA is provided. By measuring the voltage drop across the test pads the contact resistance can be determined by using Ohm's law, namely, voltage drop (V) is equal to the current (I) through a resistor multiplied by the magnitude of the resistance (R), or $V=IR$. While one method for attaching the shield layers 1926, 1928, the bonding layer 1924, the sensing element and the PCB 1922 to the frame 1918 has been described, other methods are possible. For example, as discussed, in some embodiments, one or more of the various separate layers are combined in an integral layer which is attached to the frame 1918 in one step.

Printed Circuit Board

The PCB 1922 includes various electronic components mounted to either or both faces of the PCB 1922. When sensor assembly is assembled and the PCB 1922 is disposed in the upper frame cavity 1930, some of the electronic components of the PCB 1922 may extend above the upper frame cavity 1930. To reduce space requirements and to prevent the electronic components from adversely affecting operation of the sensor assembly, the electronic components can be low-profile, surface mounted devices. The electronic components are often connected to the PCB 1922 using conventional soldering techniques, for example the flip-chip soldering technique. Flip-chip soldering uses small solder bumps such of predictable depth to control the profile of the soldered electronic components. The four tabs 1968 of the inner copper shield 1926 and the upper planar portions 1973 of the outer copper shield 1928 are soldered to the PCB 1922 in one embodiment, electrically coupling the electrical shielding barrier to the PCB 1922.

In some embodiments, the electronic components include filters, amplifiers, etc. for pre-processing or processing a low amplitude electric signal received from the sensing element 1920 (e.g., the operational amplifiers discussed above with respect to the Faraday cage) prior to transmission through a cable to a physiological monitor. In other embodiments, the electronic components include a processor or pre-processor to process electric signals. Such electronic components may include, for example, analog-to-digital converters for converting the electric signal to a digital signal and a central processing unit for analyzing the resulting digital signal.

In other embodiments, the PCB 1922 includes a frequency modulation circuit having an inductor, capacitor and oscillator, such as that disclosed in U.S. Pat. No. 6,661,161, which is incorporated by reference herein. In another embodiment, the PCB 1922 includes an FET transistor and a DC-DC converter or isolation transformer and phototransistor. Diodes and capacitors may also be provided. In yet another embodiment, the PCB 3114 includes a pulse width modulation circuit.

In one embodiment, the PCB 1922 also includes a wireless transmitter, thereby eliminating mechanical connectors and cables. For example, optical transmission via at least one optic fiber or radio frequency (RF) transmission is implemented in other embodiments. In other embodiments, the sensor assembly includes an information element which can determine compatibility between the sensor assembly and the physiological monitor to which it is attached and provide other functions, as described below.

Additional Example Sensor

FIG. 23A is a top perspective view illustrating portions of another embodiment of a sensor system 2300 including a sensor assembly 2301 suitable for use with any of the physiological monitors shown in FIGS. 1A-C. The sensor assembly 2301 includes a sensor 2315, a cable assembly 2317 and a connector 2305. The sensor 2315, in one embodiment, includes a sensor subassembly 2302 and an attachment subassembly 2304. The cable assembly 2317 of one embodiment includes a cable 2307 and a patient anchor 2303. The various components are connected to one another via the sensor cable 2307. The sensor connector 2305 can be removably attached to a physiological monitor (not shown), such as through a monitor cable, or some other mechanism. In one embodiment, the sensor assembly 2301 communicates with a physiological monitor via a wireless connection.

The sensor system 2300 and certain components thereof may be generally similar in structure and function or identical to other sensor systems described herein, such as, for

example, the sensor systems **100**, **1900** described herein with respect to FIGS. **1** and **19-22**, respectively.

For example, the sensor system **2300** may include an electrical shielding barrier (FIGS. **23D-E**) including one or more layers which form a Faraday cage around an piezo-electric sensing element (FIGS. **23D-E**), and which distribute external electrical noise substantially equally to electrical poles of the piezoelectric sensing element. The shielding barrier or portions thereof of some embodiments can flexibly conform to the surface shape of the piezoelectric element as the surface shape of the piezoelectric element changes, thereby improving the shielding and sensor performance.

The sensor system **2300** may further include an acoustic coupler **2314** which can including a bump positioned to apply pressure to the sensing element so as to bias the sensing element in tension. The acoustic coupler can also provide electrical isolation between the patient and the electrical components of the sensor, beneficially preventing potentially harmful electrical pathways or ground loops from forming and affecting the patient or the sensor.

The sensor system **2309** may also include an attachment subassembly **2304**. In one embodiment, the attachment subassembly **2304** is configured to press the sensor against the patient's skin with a pre-determined amount of force. The attachment subassembly **2304** can be configured act in a spring-like manner to press the sensor **2300** against the patient. The attachment subassembly **2304** can also be configured such that movement of the sensor **2300** with respect to the attachment subassembly **2304** does not cause the attachment subassembly **2304** to peel off or otherwise detach from the patient during use.

Additionally, in some embodiments, a patient anchor **2303** is provided which advantageously secures the sensor **2315** to the patient at a point between the ends of the cable **2307**. Securing the cable **2307** to the patient can decouple the sensor assembly **2300** from cable **2307** movement due to various movements such as accidental yanking or jerking on the cable **2307**, movement of the patient, etc. Decoupling the sensor assembly **2300** from cable **2307** movement can significantly improve performance by eliminating or reducing acoustical noise associated with cable **2307** movement. For example, by decoupling the sensor **2300** from cable movement, cable movement will not register or otherwise be introduced as noise in the acoustical signal generated by the sensor **2300**.

The shielding barrier, acoustic coupler **2314**, attachment subassembly **2304**, and patient anchor **2303** may be generally similar in certain structural and functional aspects to the shielding barrier, acoustic coupler **1914**, attachment subassembly **1904**, and patient anchor **1903** of other sensor systems described herein, such as the sensor system **1900** described with respect to FIGS. **19A-22B**, for example.

FIGS. **23B-C** are top and bottom perspective views of a sensor including subassembly **2302** and an attachment subassembly **2304** in accordance with another embodiment of the present disclosure. The attachment subassembly **2304** generally includes lateral extensions symmetrically placed about the sensor subassembly **2302**. An embodiment of a similar attachment subassembly is described in detail with respect to FIG. **10**.

FIG. **23D-E** are top and bottom exploded, perspective views, respectively, of the sensor subassembly of FIGS. **23A-C**. The frame **2318** generally supports the various components of the sensor such as the piezoelectric element, electrical shielding barrier, attachment element and other components. The sensor subassembly **2302** includes an acoustic coupler **2314**, sensing element **2320**, adhesive layer

2324, and first and second electrical shielding layers **2326**, **2328** which may, in certain aspects, be generally similar in structure and function to the acoustic coupler **1914**, sensing element **1920**, adhesive layer **1924**, and first and second electrical shielding layers **1926**, **1928** of FIGS. **19A-19E**, for example.

As shown, and unlike the embodiment shown in FIGS. **19A-E**, the adhesive layer **2324** of FIG. **23D-E** stretches straight across the frame **2328** without conforming to the surface **2350** on the underside of the frame **2318**. Thus, the sensing element **2320** is sandwiched between the adhesive layer **2324** and the outer shielding layer **2328**. The adhesive layer **2324** includes adhesive over its entire outer surface which is in contact with the sensing element **2320**. Moreover, the copper layer **2328** may also include an adhesive on its interior surface which contacts the other side of the sensing element **2320**. As such, the adhesive layer **2324** and the shielding layer **2328** bond to opposite sides of the sensing element **2320**, sandwiching and creating a seal around it. This sandwiching and sealing of the sensing element **2320** improves the liquid resistivity of the sensor subassembly **2302** by impeding water or water vapors (e.g., from sweat or other sources) from ingressing and contacting the sensing element **2320**. Thus, the sandwiching of the sensing element **2320** protects the sensor **2302** from undesired effects such as electrical shorting due to liquid ingress. In one embodiment, the sensor **2302** is IPX1 compliant.

The planar portion **2325** of the adhesive layer **2324**, along with the corresponding planar portions **2321**, **2329** of the sensing element **2320** and outer shielding layer **2328**, are configured to move with respect to the cavity defined by the underside of the frame **2318** in response to vibrations. The adhesive layer **2324** generally includes adhesive on all of its surface area except for the interior surface of the planar portion **2325**. As such, the adhesive layer **2324** is securely bonded in place while the planar portion **2325** can move freely with respect to the cavity during operation without sticking. Moreover, because the interior portion of the planar portion **2325** is non-adhesive, foreign material such as dust particles will generally not stick to the non-adhesive planar portion **2325**, improving sensor operation.

Similar to the frame **1918** of FIG. **19D**, the frame **2318** includes four locking posts **2332**. However, the posts **2332** of FIG. **23D** are shown in a locked or liquefied configuration, unlike the posts **1932** illustrated in FIG. **19D**.

As shown in FIG. **23D**, the shielding layers **2326**, **2328** include flap portions **2368**, **2373** which conform to the frame **2318** and sit underneath the PCB **2322** in an assembled configuration. Similarly, the sensing element **2320** of the sensor subassembly **2302** includes a flap portion **2372** which conforms to the frame **2318** and sits underneath the PCB **1922**. Upon welding of the locking posts **2332**, the PCB **2322** is pressed downwards into physical and electrical contact with the flap portions **2368**, **2373**, **2372** of the shielding layers **2326**, **2328** and sensing element **2320**. As such, because the flaps **2368**, **2373**, **2372** are configured to sit underneath the PCB **2322**, they are held in place in a pressure fit without soldering, improving manufacturability. Information Element

In addition, the sensor assembly can include any of a variety of information elements, such as readable and/or writable memories. Information elements can be used to keep track of device usage, manufacturing information, duration of sensor usage, compatibility information, calibration information, identification information, other sensor, physiological monitor, and/or patient statistics, etc. The information element can communicate such information to a

physiological monitor. For example, in one embodiment, the information element identifies the manufacturer, lot number, expiration date, and/or other manufacturing information. In another embodiment, the information element includes calibration information regarding the multi-parameter sensor. Information from the information element is provided to the physiological monitor according to any communication protocol known to those of skill in the art. For example, in one embodiment, information is communicated according to an I²C protocol. The information element may be provided on or be in electrical communication with the PCB 1922. In various embodiments, the information element can be located in another portion of the sensor assembly. For example, in one embodiment, the information element is provided on a cable connected to the PCB 1922. The information element may further be located on the sensor connector 1905, the attachment subassembly 1904, or some other part of the sensor assembly.

The information element can include one or more of a wide variety of memory devices known to an artisan from the disclosure herein, including an EPROM, an EEPROM, a flash memory, a combination of the same or the like. The information element can include a read-only device such as a ROM, a read and write device such as a RAM, combinations of the same, or the like. The remainder of the present disclosure will refer to such combination as simply EPROM for ease of disclosure; however, an artisan will recognize from the disclosure herein that the information element can include the ROM, the RAM, single wire memories, combinations, or the like.

The information element can advantageously store some or all of a wide variety data and information, including, for example, information on the type or operation of the sensor, type of patient or body tissue, buyer or manufacturer information, sensor characteristics including calculation mode data, calibration data, software such as scripts, executable code, or the like, sensor electronic elements, sensor life data indicating whether some or all sensor components have expired and should be replaced, encryption information, monitor or algorithm upgrade instructions or data, or the like. In some embodiments, the information element can be used to provide a quality control function. For example, the information element may provide sensor identification information to the system which the system uses to determine whether the sensor is compatible with the system.

In an advantageous embodiment, the monitor reads the information element on the sensor to determine one, some or all of a wide variety of data and information, including, for example, information on the type or operation of the sensor, a type of patient, type or identification of sensor buyer, sensor manufacturer information, sensor characteristics including history of the sensor temperature, the parameters it is intended to measure, calibration data, software such as scripts, executable code, or the like, sensor electronic elements, whether it is a disposable, reusable, or multi-site partially reusable, partially disposable sensor, whether it is an adhesive or non-adhesive sensor, sensor life data indicating whether some or all sensor components have expired and should be replaced, encryption information, keys, indexes to keys or has functions, or the like monitor or algorithm upgrade instructions or data, some or all of parameter equations, information about the patient, age, sex, medications, and other information that can be useful for the accuracy or alarm settings and sensitivities, trend history, alarm history, sensor life, or the like.

Terminology/Additional Embodiments

Embodiments have been described in connection with the accompanying drawings. However, it should be understood that the figures are not drawn to scale. Distances, angles, etc. are merely illustrative and do not necessarily bear an exact relationship to actual dimensions and layout of the devices illustrated. In addition, the foregoing embodiments have been described at a level of detail to allow one of ordinary skill in the art to make and use the devices, systems, etc. described herein. A wide variety of variation is possible. Components, elements, and/or steps can be altered, added, removed, or rearranged. While certain embodiments have been explicitly described, other embodiments will become apparent to those of ordinary skill in the art based on this disclosure.

Conditional language used herein, such as, among others, “can,” “could,” “might,” “may,” “e.g.,” and the like, unless specifically stated otherwise, or otherwise understood within the context as used, is generally intended to convey that certain embodiments include, while other embodiments do not include, certain features, elements and/or states. Thus, such conditional language is not generally intended to imply that features, elements and/or states are in any way required for one or more embodiments or that one or more embodiments necessarily include logic for deciding, with or without author input or prompting, whether these features, elements and/or states are included or are to be performed in any particular embodiment.

Depending on the embodiment, certain acts, events, or functions of any of the methods described herein can be performed in a different sequence, can be added, merged, or left out all together (e.g., not all described acts or events are necessary for the practice of the method). Moreover, in certain embodiments, acts or events can be performed concurrently, e.g., through multi-threaded processing, interrupt processing, or multiple processors or processor cores, rather than sequentially.

The various illustrative logical blocks, modules, circuits, and algorithm steps described in connection with the embodiments disclosed herein can be implemented as electronic hardware, computer software, or combinations of both. To clearly illustrate this interchangeability of hardware and software, various illustrative components, blocks, modules, circuits, and steps have been described above generally in terms of their functionality. Whether such functionality is implemented as hardware or software depends upon the particular application and design constraints imposed on the overall system. The described functionality can be implemented in varying ways for each particular application, but such implementation decisions should not be interpreted as causing a departure from the scope of the disclosure.

The various illustrative logical blocks, modules, and circuits described in connection with the embodiments disclosed herein can be implemented or performed with a general purpose processor, a digital signal processor (DSP), an application specific integrated circuit (ASIC), a field programmable gate array (FPGA) or other programmable logic device, discrete gate or transistor logic, discrete hardware components, or any combination thereof designed to perform the functions described herein. A general purpose processor can be a microprocessor, but in the alternative, the processor can be any conventional processor, controller, microcontroller, or state machine. A processor can also be implemented as a combination of computing devices, e.g., a combination of a DSP and a microprocessor, a plurality of microprocessors, one or more microprocessors in conjunction with a DSP core, or any other such configuration.

The blocks of the methods and algorithms described in connection with the embodiments disclosed herein can be embodied directly in hardware, in a software module executed by a processor, or in a combination of the two. A software module can reside in RAM memory, flash memory, ROM memory, EPROM memory, EEPROM memory, registers, a hard disk, a removable disk, a CD-ROM, or any other form of computer-readable storage medium known in the art. An exemplary storage medium is coupled to a processor such that the processor can read information from, and write information to, the storage medium. In the alternative, the storage medium can be integral to the processor. The processor and the storage medium can reside in an ASIC. The ASIC can reside in a user terminal. In the alternative, the processor and the storage medium can reside as discrete components in a user terminal.

While the above detailed description has shown, described, and pointed out novel features as applied to various embodiments, it will be understood that various omissions, substitutions, and changes in the form and details of the devices or algorithms illustrated can be made without departing from the spirit of the disclosure. As will be recognized, certain embodiments of the inventions described herein can be embodied within a form that does not provide all of the features and benefits set forth herein, as some features can be used or practiced separately from others. The scope of certain inventions disclosed herein is indicated by the appended claims rather than by the foregoing description. All changes which come within the meaning and range of equivalency of the claims are to be embraced within their scope.

What is claimed is:

1. An acoustic sensor comprising:
first and second piezoelectric elements each including respective first and second electrodes; and
a noise attenuator coupled to the first electrode of the first piezoelectric element and the first electrode of the second piezoelectric element, the noise attenuator configured to:
at least partially constructively combine a physiological signal component of a first signal output by the first piezoelectric element and a physiological signal component of a second signal output by the second piezoelectric element; and
at least partially destructively combine a noise component of the first signal output by the first piezoelectric element and a noise component of the second signal output by the second piezoelectric element.
2. The acoustic sensor of claim 1, wherein the first piezoelectric element and the second piezoelectric element are arranged in a stack, and wherein the second electrode of the first piezoelectric element and the second electrode of the second piezoelectric element are coupled to a common potential.
3. The acoustic sensor of claim 2, wherein the first and second piezoelectric elements each comprise:
first electrode coatings disposed on surfaces of the respective piezoelectric elements corresponding to an outer portion of the stack; and
second electrode coatings disposed on surfaces of the respective piezoelectric elements corresponding to an inner portion of the stack,
wherein the first electrode coatings are configured to shield the second electrode coatings from electromagnetic noise.

4. The acoustic sensor of claim 1, wherein the noise attenuator comprises at least one of: circuitry including an amplifier, a signal processor, or a general-purpose processor.

5. The acoustic sensor of claim 1, wherein the noise attenuator is further configured to generate a reduced noise signal based on constructively combining the physiological signal components and destructively combining the noise components.

6. The acoustic sensor of claim 5, wherein the reduced noise signal has a lower noise component than one or more of the first and second signals.

7. The acoustic sensor of claim 5, wherein the noise attenuator generates the reduced noise signal using common-mode rejection.

8. The acoustic sensor of claim 1 further comprising:

a coupling bump configured to apply pressure to at least one of the first and second piezoelectric elements to push at least a portion of the one of the first and second piezoelectric elements into a cavity of the acoustic sensor.

9. The acoustic sensor of claim 8, wherein the coupling bump is configured to transmit acoustic vibrations to the one of the first and second piezoelectric elements through the acoustic coupling bump when the acoustic sensor is attached to the medical patient.

10. A method comprising:

receiving signals from an acoustic sensor that is attachable to a medical patient and configured to provide the signals responsive to acoustic vibrations indicative of one or more physiological parameters of the medical patient, the acoustic sensor including first and second piezoelectric elements each including respective first and second electrodes; and
by a noise attenuator:

at least partially constructively combine a physiological signal component of a first signal output by the first piezoelectric element and a physiological signal component of a second signal output by the second piezoelectric element; and

at least partially destructively combine a noise component of the first signal output by the first piezoelectric element and a noise component of the second signal output by the second piezoelectric element,

wherein the noise attenuator is coupled to the first electrode of the first piezoelectric element and the first electrode of the second piezoelectric element.

11. The method of claim 10, wherein the first piezoelectric element and the second piezoelectric element are arranged in a stack, and wherein the second electrode of the first piezoelectric element and the second electrode of the second piezoelectric element are coupled to a common potential.

12. The method of claim 11, wherein the first and second piezoelectric elements each comprise:

first electrode coatings disposed on surfaces of the respective piezoelectric elements corresponding to an outer portion of the stack; and

second electrode coatings disposed on surfaces of the respective piezoelectric elements corresponding to an inner portion of the stack,

wherein the first electrode coatings are configured to shield the second electrode coatings from electromagnetic noise.

13. The method of claim 10, wherein the noise attenuator comprises at least one of: circuitry including an amplifier, a signal processor, or a general-purpose processor.

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14. The method of claim 10 further comprising:

by the noise attenuator, generating a reduced noise signal
based on constructively combining the physiological
signal components and destructively combining the
noise components.

15. The method of claim 14, wherein the reduced noise
signal has a lower noise component than one or more of the
first and second signals.

16. The method of claim 14, wherein the noise attenuator
generates the reduced noise signal using common-mode
rejection.

17. The method of claim 10, wherein the acoustic sensor
further includes a coupling bump configured to apply pres-
sure to at least one of the first and second piezoelectric
elements to push at least a portion of the one of the first and
second piezoelectric elements into a cavity of the acoustic
sensor.

18. The method of claim 17, wherein the coupling bump
is configured to transmit acoustic vibrations to the one of the
first and second piezoelectric elements through the acoustic
coupling bump when the acoustic sensor is attached to the
medical patient.

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19. A method comprising:

at least partially constructively combining, by a noise
attenuator, a physiological signal component of a first
signal received from a first piezoelectric element of an
acoustic sensor and a physiological signal component
of a second signal received from a second piezoelectric
element of the acoustic sensor; and

at least partially destructively combining, by the noise
attenuator, a noise component of the first signal
received from the first piezoelectric element and a noise
component of the second signal received from the
second piezoelectric element,

wherein the noise attenuator is coupled to a first electrode
of the first piezoelectric element and a first electrode of
the second piezoelectric element.

20. The method of claim 19, wherein a second electrode
of the first piezoelectric element and a second electrode of
the second piezoelectric element are coupled to a common
potential.

21. The method of claim 20, wherein the first and second
piezoelectric elements are each stretched from a first side of
a cavity of the acoustic sensor to a second side of the cavity
of the acoustic sensor.

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专利名称(译)	具有多个传感元件的声学呼吸监测传感器		
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摘要(译)

根据某些描述的方面，多种声学传感元件以各种有益的方式被采用以提供改进的生理监测，以及其他优点。在各种实施例中，传感元件可有利地用于单个传感器封装中，多个传感器封装中以及监控环境中的各种其他策略位置。根据其他方面，为了补偿皮肤弹性和附着可变性，提供了包括一个或多个压力平衡路径的声学传感器支撑件。通路可以提供从由传感元件和框架限定的空腔到环境空气压力的空气流动通道。

