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(54) **FUNCTIONAL SKIN PATCH**

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(57) **ABSTRACT**

A functional skin patch having a first surface and a second surface opposite the first surface is provided. The functional skin patch includes a functional unit having a thermo harvester and an antenna unit. The thermo harvester has a first terminal thermally connected to the first surface and a second terminal. The antenna unit has a first terminal thermally connected to the second terminal of the thermo harvester and a second terminal thermally connected to the second surface. The antenna unit has a stacked layer structure including, in this sequence, a metal layer thermally connected to the second terminal of the thermo harvester, a ferrite layer thermally connected to the metal layer, and an antenna layer thermally connected to the ferrite layer.

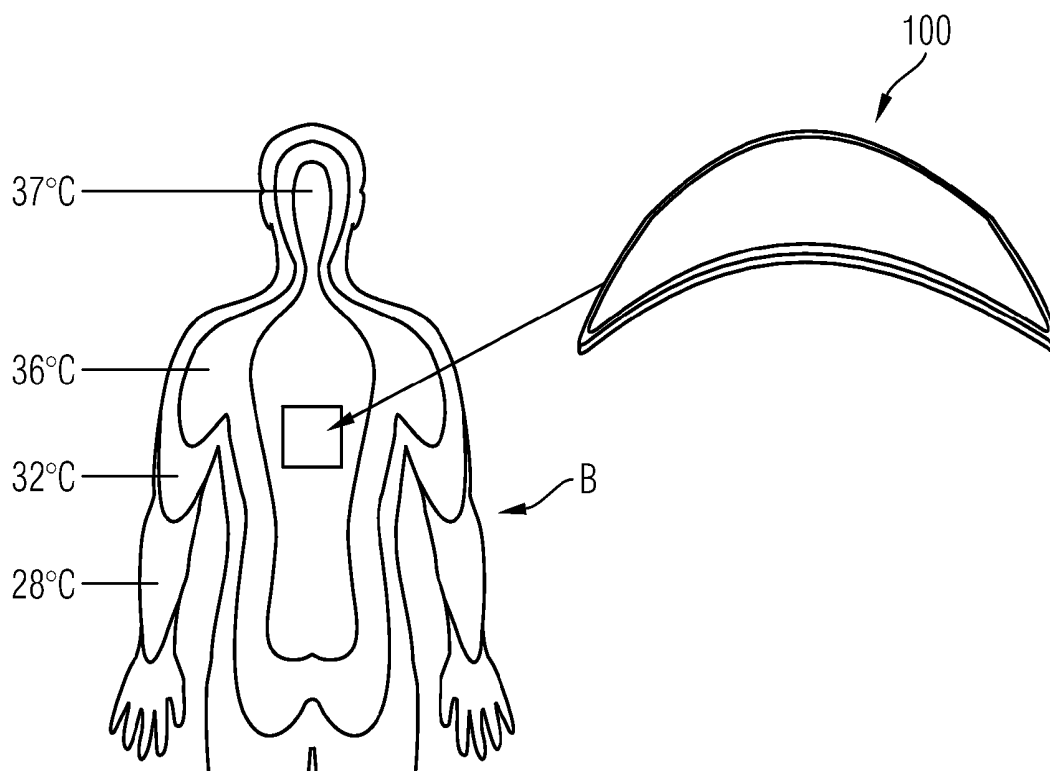


FIG 1A

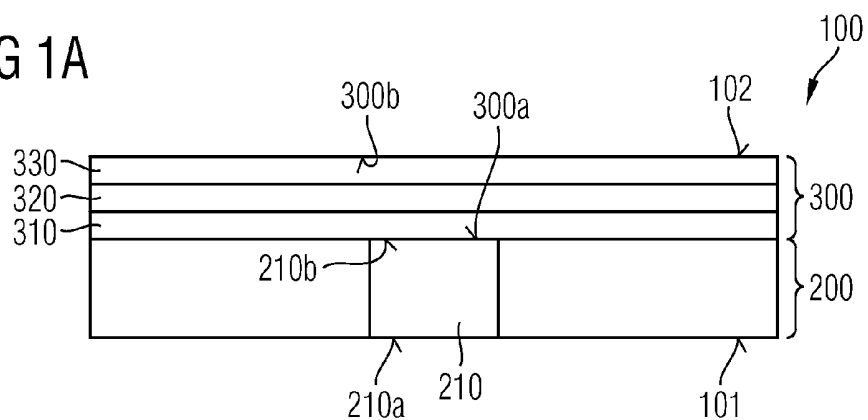


FIG 1B

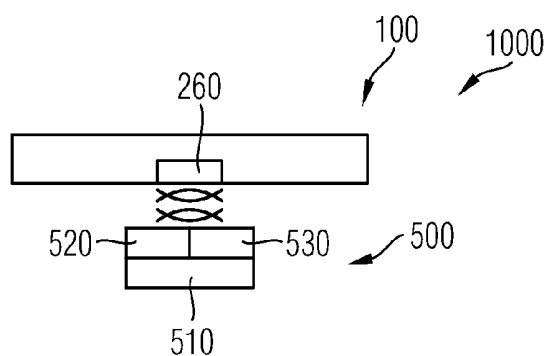


FIG 2

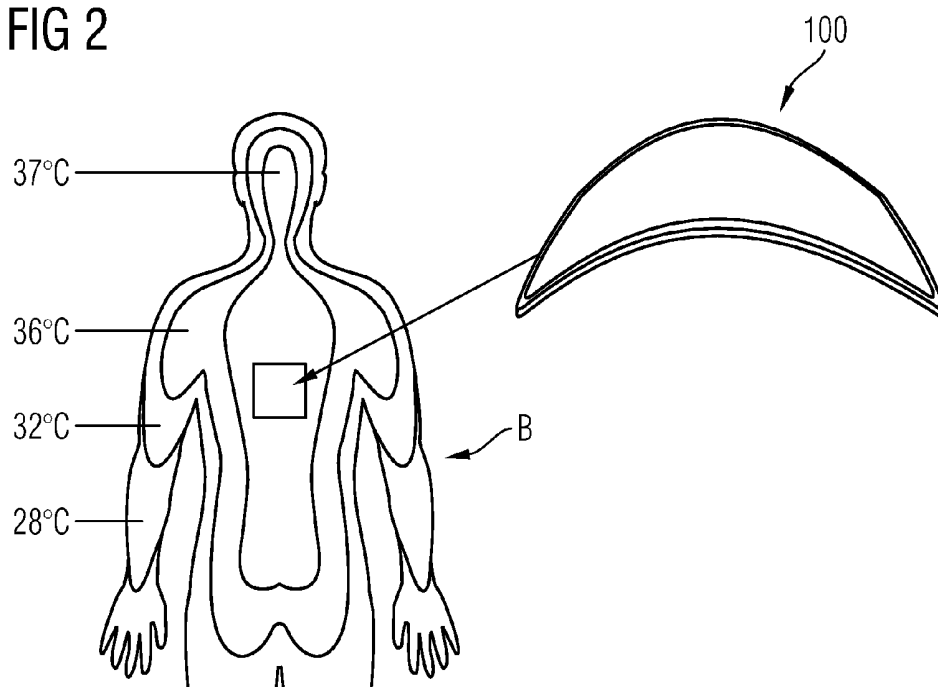


FIG 5A

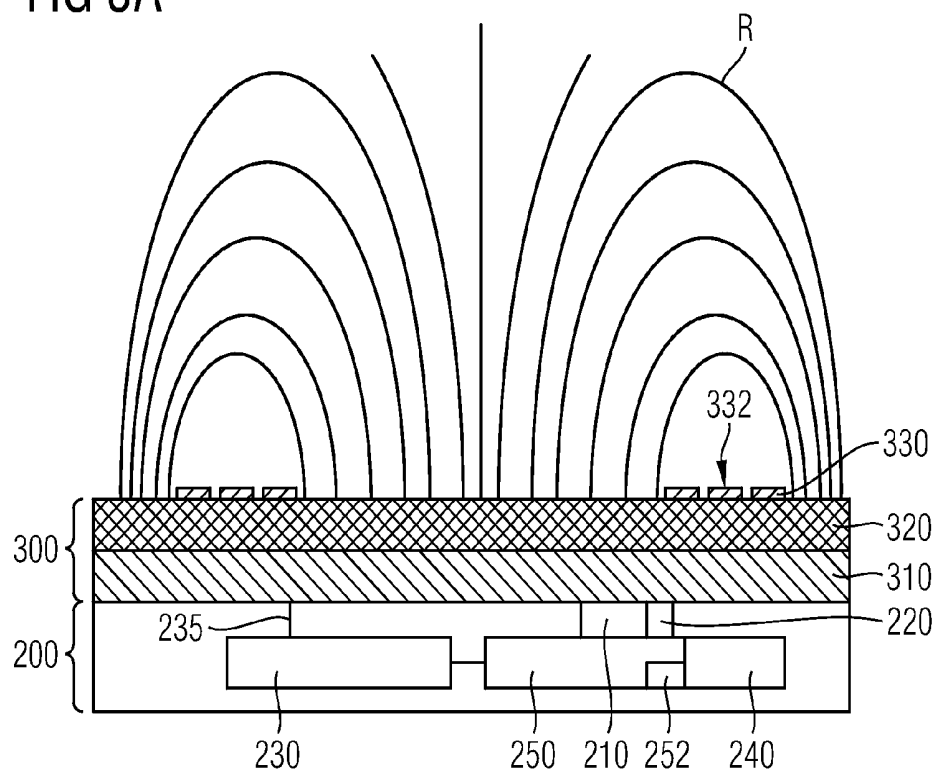


FIG 5B

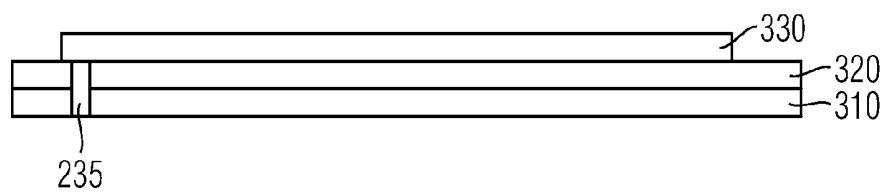


FIG 6

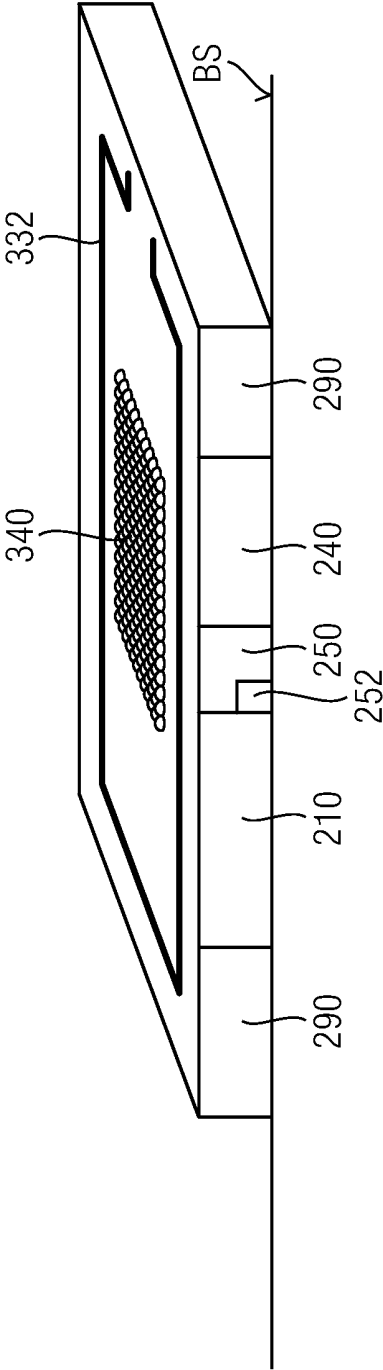


FIG 7A

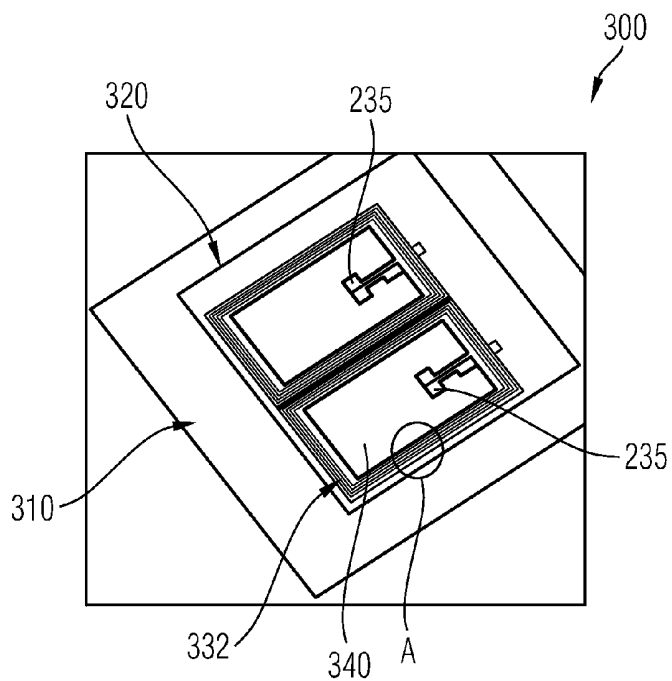


FIG 7B

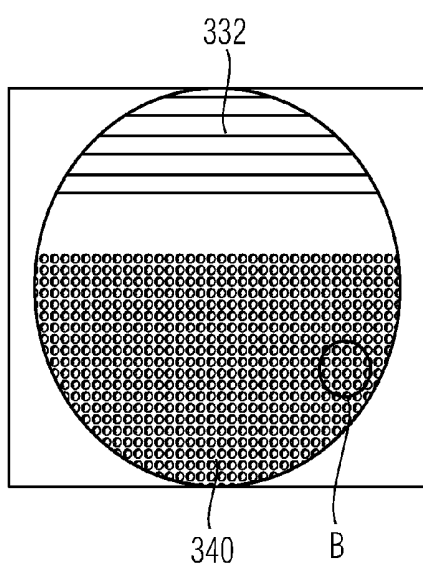


FIG 7C

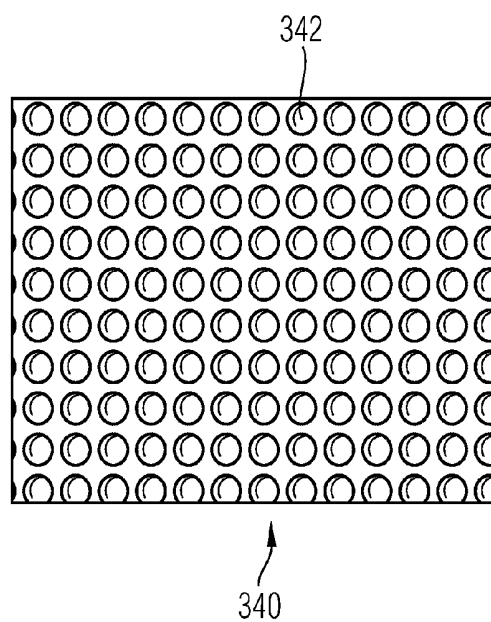


FIG 8

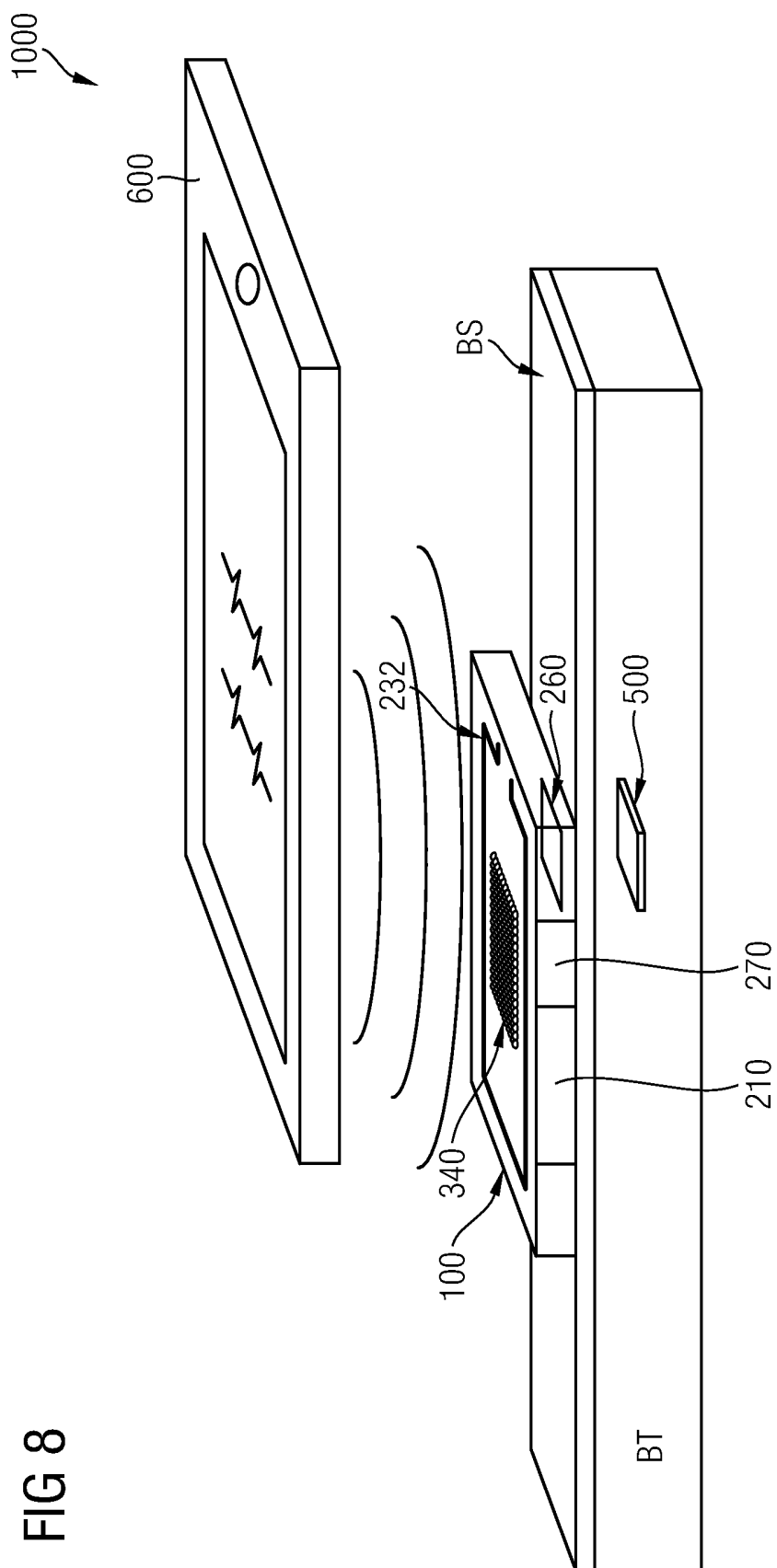


FIG 9

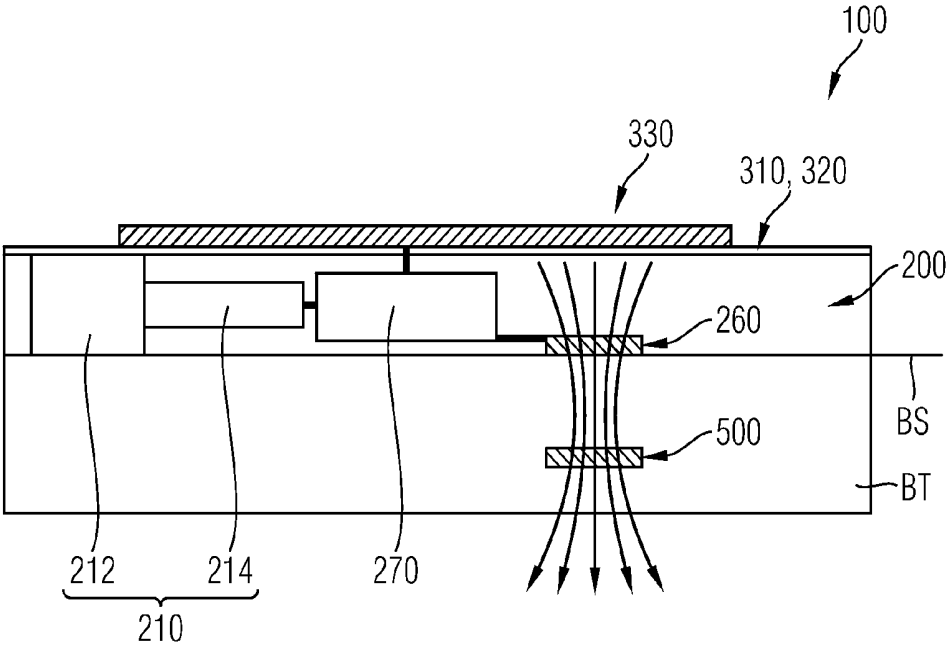


FIG 10A

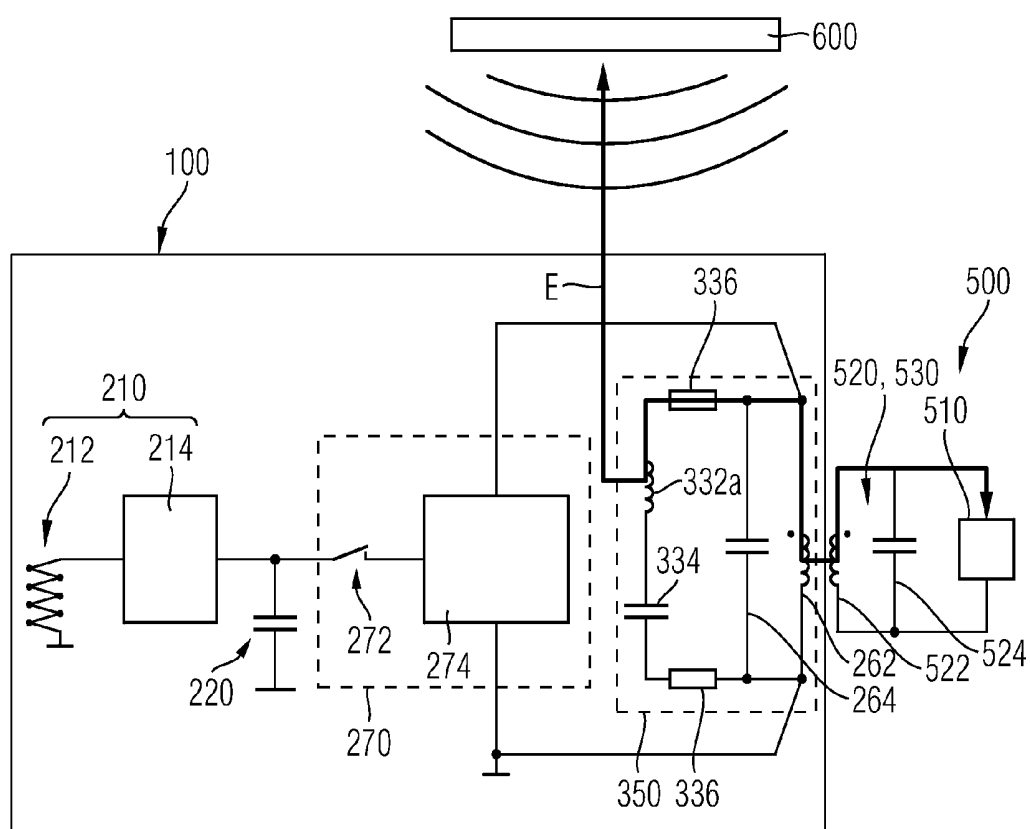
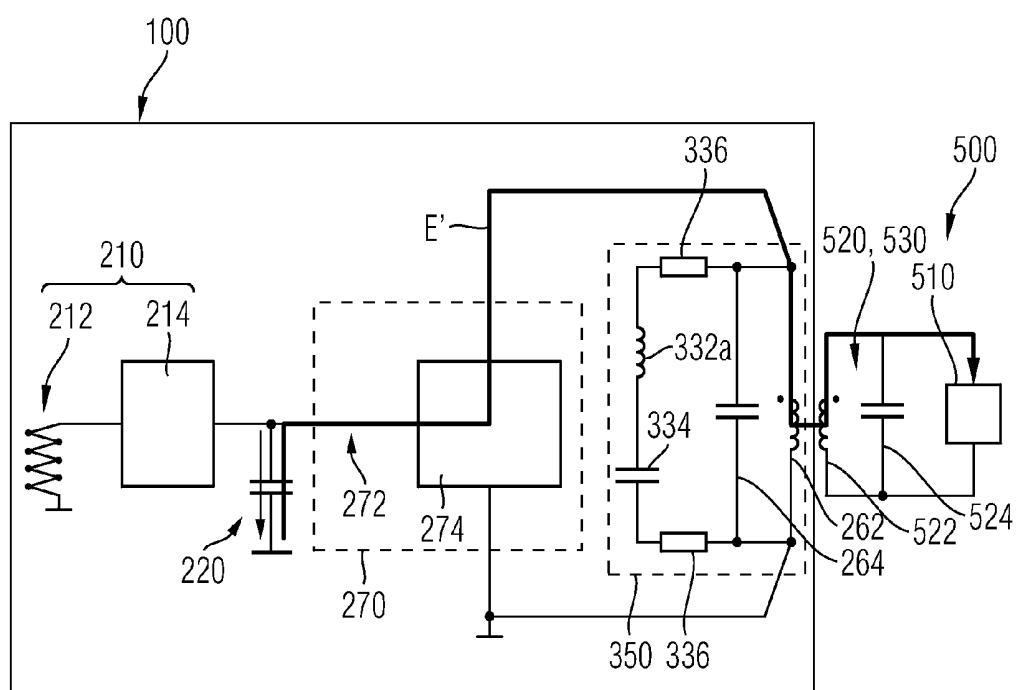


FIG 10B



FUNCTIONAL SKIN PATCH

PRIORITY CLAIM

[0001] This application claims priority to German Patent Application No. 10 2014 116 537.3 filed on 12 Nov. 2014, the content of said application incorporated herein by reference in its entirety.

BACKGROUND

[0002] Functional skin patches or sensor plasters for medical or industrial monitoring networks provide limited space in a thickness direction and further require flexibility to fit to the underlying body, e.g. a human body. In case a thermo harvester is integrated in a functional skin patch, a radiating surface of maximized area is desirable to enhance the thermal conductivity between the functional skin patch and the surrounding air. To provide a low thermal transfer resistance of the outer surface of the functional skin patch, a metal layer may be provided. However, in case the functional skin patch is equipped with an antenna unit, the radiating outer surface and the antenna part compete for the surface area of the outer surface of the functional skin patch.

[0003] It is an object to provide a functional skin patch having an antenna and improved thermo harvesting properties.

SUMMARY

[0004] According to an embodiment of a functional skin patch having a first surface and a second surface opposite the first surface, the functional skin patch comprises a functional unit comprising a thermo harvester, the thermo harvester having a first terminal thermally connected to the first surface and a second terminal, and an antenna unit having a first terminal thermally connected to the second terminal of the thermo harvester and a second terminal thermally connected to the second surface, wherein the antenna unit has a stacked layer structure comprising, in this sequence, a metal layer thermally connected to the second terminal of the thermo harvester, a ferrite layer thermally connected to the metal layer, and an antenna layer thermally connected to the ferrite layer.

[0005] According to an embodiment of a system for monitoring a body health parameter, the system comprises a functional skin patch, and an implantable device having a sensor unit for measuring at least one body health parameter, a data transceiver unit for transmitting measurement data containing the at least one body health parameter to the functional skin patch, and an energy receiving unit for receiving electromagnetic energy from the coupling antenna of the functional skin patch.

[0006] Those skilled in the art will recognize additional features and advantages upon reading the following detailed description and on viewing the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

[0007] The accompanying drawings are included to provide a further understanding of the invention and are incorporated in and constitute a part of this specification. The drawings illustrate the embodiments of the present invention and together with the description serve to explain principles of the invention. Other embodiments of the invention and

intended advantages will be readily appreciated as they become better understood by reference to the following detailed description.

[0008] FIG. 1A is a schematic block diagram of a functional skin patch according to an embodiment.

[0009] FIG. 1B is a schematic block diagram of a system for monitoring a body health parameter according to an embodiment.

[0010] FIG. 2 illustrates an arrangement position on a human body of a functional skin patch according to an embodiment.

[0011] FIG. 3 is a schematic diagram illustrating heat flow through the functional skin patch according to an embodiment.

[0012] FIG. 4 is a thermal circuit diagram illustrating the heat flux through the functional skin patch according to an embodiment.

[0013] FIG. 5A is a schematic cross-sectional view of a portion of a functional skin patch according to an embodiment.

[0014] FIG. 5B is a schematic cross-sectional view of a portion of the antenna unit of the functional skin patch according to an embodiment.

[0015] FIG. 6 is a schematic perspective view of a functional skin patch comprising a metal dot layer printed on a ferrite layer for enhancing the surface area of the antenna layer according to an embodiment.

[0016] FIG. 7A is a schematic perspective view of the antenna unit according to an embodiment.

[0017] FIG. 7B is a detailed view of the part A of FIG. 7A showing an antenna pattern and a metal dot layer printed on the ferrite layer of the functional skin patch according to an embodiment.

[0018] FIG. 7C is a detailed view of the part B of FIG. 7B showing the metal dot layer printed on the ferrite layer.

[0019] FIG. 8 is a schematic perspective view of a system for monitoring a body health parameter according to an embodiment.

[0020] FIG. 9 is a schematic cross-sectional view of a functional skin patch of the system for monitoring a body health parameter according to an embodiment.

[0021] FIG. 10A is a schematic circuit diagram of the system for monitoring a body health parameter in a first modus.

[0022] FIG. 10B is a schematic circuit diagram of a system for monitoring a body health parameter in a second modus.

DETAILED DESCRIPTION

[0023] In the following detailed description, reference is made to the accompanying drawings, which form a part hereof, and in which are shown by way of illustrations specific embodiments in which the invention may be practiced. It is to be understood that other embodiments may be utilized and structural or logical changes may be made without departing from the scope of the present invention. For example, features illustrated or described for one embodiment can be used on or in conjunction with other embodiments to yield yet a further embodiment. It is intended that the present invention includes such modifications and variations. The examples are described using specific language which should not be construed as limiting the scope of the appending claims. The drawings are not scaled and are for illustrative purposes only. For clarity, the same elements have been designated by corresponding references in the different drawings if not stated otherwise.

[0024] The terms “having”, “containing”, “including”, “comprising” and the like are open and the terms indicate the presence of stated structures, elements or features but not preclude additional elements or features. The articles “a”, “an” and “the” are intended to include the plural as well as the singular, unless the context clearly indicates otherwise.

[0025] The term “electrically connected” describes a permanent low-ohmic connection between electrically connected elements, for example a direct contact between the concerned elements or a low-ohmic connection via a metal and/or highly doped semiconductor. The term “electrically coupled” includes that one or more intervening element(s) configured for signal transmission may be provided between the electrically coupled elements, for example resistors, resistive elements or elements that are controllable to temporarily provide a low-ohmic connection in a first state and a high-ohmic electric decoupling in a second state.

[0026] FIG. 1A is a schematic block diagram of a functional skin patch 100 according to an embodiment. As can be seen from FIG. 1A, the functional skin patch 100 has a first surface 101 and a second surface 102, which is opposite to the first surface 101. The functional skin patch 100 comprises a functional unit 200 and an antenna unit 300. The functional unit 200 comprises a thermo harvester 210, wherein the thermo harvester 210 has a first terminal 210a thermally connected to the first surface 101 and a second terminal 210b. The second terminal 210b of the thermo harvester 210 is thermally connected to a first terminal 300a of the antenna unit 300. A second terminal 300b of the antenna unit 300 is thermally connected to the second surface 102. The antenna unit 300 has a stacked layer structure comprising, in this sequence, a metal layer 310 thermally connected to the second terminal 210b of the thermo harvester 210, a ferrite layer 320 thermally connected to the metal layer 310, and an antenna layer 330 thermally connected to the ferrite layer 320.

[0027] By providing the structure of the functional skin patch 100, an electromagnetic field of the antenna layer 330 is reflected by the ferrite layer 320 while at the same time the antenna layer 330 is electrically isolated from the metal layer 310. As a consequence, by providing the antenna unit 300 having the stacked layer structure of the metal layer 310, the ferrite layer 320 and the antenna layer 330, an excellent heat flux from the second terminal 210b of the thermo harvester 210 to the second surface 102 of the functional skin patch 100 may be provided while the functionality of the antenna layer 330 is not negatively affected.

[0028] FIG. 1B is a schematic block diagram of a system 1000 for monitoring a body health parameter according to an embodiment. The system 1000 comprises a functional skin patch 100 and an implantable device 500. The implantable device 500 has a sensor unit 510 for measuring at least one body health parameter, a data transceiver unit 520 for transmitting measurement data containing the at least one body health parameter to the functional skin patch 100, and an energy receiving unit 530 for receiving electromagnetic energy from the coupling antenna 260 of the functional skin patch 100.

[0029] By providing the system 1000 as shown in FIG. 1B, an implantable device may be energized by the functional skin patch 100, which in turn is configured to generate autonomously energy by means of the thermo harvester 210. Thus, a long term monitoring of at least one body health

parameter may be achieved, wherein the energy for the monitoring is at least partly generated by harvesting the body heat.

[0030] FIG. 2 illustrates and arrangement position of a functional skin patch 100 on a human body B. The functional skin patch 100 according to an embodiment is configured to harvest the body heat by conducting heat from a body skin through the thermo harvester 210 to an outer surface, i.e. the second surface 102, which is in contact with the air of the environment. The application of the functional skin patch 100 is not restricted to the human body B, but it is also possible to apply the functional skin patch 100 to a body surface of an animal, which is preferably an endotherm. As can be seen from FIG. 2, the extremities of the human body B have a lower temperature, thus an application at the torso of the human body B is preferred. The temperature of the human body B reaches from a temperature range of 28° C. at a forearm region to 37° C. at a torso region of the human body B.

[0031] The area of the first and second surface 101, 102 of the functional skin patch 100 may be in a range of 20 cm² to 500 cm², or in a range of 50 cm² to 100 cm², or in a range of 50 cm² to 80 cm². The size of the functional skin patch 100 is a trade-off between the amount of heat which can be harvested, and the convenience for a person wearing the functional skin patch 100.

[0032] FIG. 3 illustrates the heat flux within the functional skin patch 100 according to an embodiment, wherein FIG. 4 is the corresponding thermal circuit diagram of the functional skin patch 100. As can be seen from FIG. 3, the functional skin patch 100 may further comprise a heat collector unit 400 having a first terminal 400a thermally connected to the first surface 101 and a second terminal 400b thermally connected to the first terminal 210a of the thermo harvester 210. As further illustrated in FIG. 3, the thermo harvester 210 may be embedded in a thermally isolating layer 290, to ensure that the heat flux is guided only through the thermo harvester 210 and is not bypassed or shunted from the heat collector unit 400 to the antenna unit 300. The thermally isolating layer 290 may comprise at least one of wool, cellulose, foamed plastics such as expanded polyethylene or a material which fulfils the requirements of being flexible and at the same time having a low heat conductance. The thermal resistance of the thermally isolating layer 290 may be in a range of 20 to 50 K/W.

[0033] The heat flux Q flows, as shown in FIG. 4, from the skin of a body, which has a temperature T_{source}, via the first surface 101, the first terminal 400a of the heat collector unit 400, and the second terminal 400b to the heat collector unit 400 having a thermal resistance R_{θ_source}. From the second terminal 400b of the heat collector unit 400, the heat flux Q flows through the thermal harvester 210 from the first terminal 210a to the second terminal 210b, wherein the inner thermal resistance of the thermo harvester 210 is R_{θ_TEG}. The heat is then guided from the second terminal 210b of the thermo harvester 210 through the antenna unit 300 having a thermal resistance of R_{θ_sink} and from the first terminal 300a to the second terminal 300b of the antenna unit 300. At least, the heat is then radiated from the second surface 102 being in contact with air having the temperature T_{Air}, wherein the second surface 102 is in thermal contact with the second terminal 300b of the antenna unit 300.

[0034] Thermoelectric energy harvesting of the thermo harvester 210 makes use of the thermo electric effect to gain electric energy from a temperature difference ΔT_{TEG}. In an operating state of the thermo harvester 210, a continuous heat flux occurs from the heat source having the temperature

T_{source} through the thermo harvester **210** via the radiating second surface **102** to the surrounding air having the temperature T_{Air}. A crucial parameter in the described system is the thermal transfer resistance of the second terminal **300b** of the antenna unit **300** or the second surface **102** to the surrounding air. In case no sufficient heat radiation occurs, the temperature at the second terminal **210b** of the thermo harvester **210** rises, thus the temperature gradient ΔT_{TEG} will be diminished, resulting in a lower output power of the thermo harvester **210**. As a consequence, the thermal resistance of the heat collector unit **400** R₀_{source} and the thermal resistance of the antenna unit **300** R₀_{sink} is preferably low to reduce the thermal resistive impedance drop at the respective thermal resistors of the antenna unit **300** and the heat collector unit **400**.

[0035] Thus, the heat collector unit **400** is preferably made of a material having a high thermal conductivity such as a metal or a material having a sufficient flexibility and at the same time a high thermal conductivity. In an analogous way, the antenna unit **300** being configured to spread the heat flux from the second terminal **210b** of the thermo harvester **210** to the second surface **102** is made of a material or a material composition having a low thermal resistance. From a heat conductance side of view, an antenna unit **300** consisting only of a material having a high thermal conductivity may be preferred. However, most of the materials with a sufficient flexibility and a high thermal conductivity show at the same time a high electric conductivity.

[0036] Thus, for providing an antenna structure, which is not shunted by the antenna unit **300** and which may be selectively contacted from the side of the functional unit **200**, a design of the antenna unit **300** is necessary, which provides both the possibility of having an antenna structure and improved thermal conductance properties. In other words, a co-integration of an antenna and a heat sink has to be provided, which has a small size and a flexible design. Herein, the antenna unit **300** should combine the properties of an ideal heat sink being a good heat conductor, having a large surface area and being flexible, and of an ideal antenna substrate being an electrical insulator.

[0037] The temperature T_{source} of the skin is lowered by the thermal resistance of the skin, thus a region, in which the body temperature is about 37° C., is lowered to a temperature of about 28° C. to 30° C. In case the temperature of the environment T_{air} is about 10° C. to 15° C., a total temperature difference between T_{source} and T_{air} is in a range of 10° C. Taking into account the thermal resistances R₀_{source} and R₀_{sink}, a temperature difference ΔT_{TEG} over R₀_{TEG} is in a range of 1 K to 3 K. The power density of the human body B in the torso region is about 3.5 mW/cm². R₀_{source} may be in a range of 10 K/W-300 K/W. (R₀_{source} includes the complete thermal resistance from the inner part of the body to the thermo harvester). R₀_{TEG} may be in a range between 10 K/W and 20 K/W. R₀_{sink} may be in a range of 100 K/W to 300 K/W, or in a range of 100 K/W to 120 K/W, as will be discussed below.

[0038] FIG. 5A is a schematic cross-sectional view of a portion of a functional skin patch **100** of an embodiment.

[0039] As can be seen from FIG. 5A, the functional unit **200** comprises, next to the thermo harvester **210**, further functional elements. The functional unit **200** may further comprise a radio frequency (RF) circuit **230**, which is connected to the antenna layer **330** via a connection plug **235**. The connection plug **235** is, as can be seen from FIG. 5B, extended through the metal layer **310** and the ferrite layer **320** and

connected to the antenna layer **330**. FIG. 5B is a detailed view of the antenna unit **300**. The transmission frequency of the RF-circuit **230** and of the antenna layer **330** is in a range, which is configured to the size of the functional skin patch **100**. Preferably, the transmission band is in a range of 10 MHz to 100 MHz, or in a range of 10 MHz to 50 MHz, or in a range of 10 MHz to 20 MHz, or in a range of 13 MHz to 14 MHz.

[0040] The functional unit **200** may further comprise a sensor unit **240**, which is configured to sense a body health parameter including at least one of a body temperature, a body pulse frequency, an electrocardiogram recording, an electro-encephalogram recording, a body function, a blood sugar value, a blood pressure, or a blood heparin value. The body temperature may be measured by an integrated thermometer. The body pulse frequency, the electrocardiogram recording, and the electroencephalogram recording may be measured by electrodes integrated in the first surface **101** of the functional skin patch **100**, wherein the measured electrode potential recording is analysed in a well-known manner. Furthermore, a blood sugar value may be measured invasively by a sensor chip analysing blood or interstitial fluid composition or non-invasively by near infrared or infrared recording or by photoacoustic measurements of the interstitial fluid in the subcutaneous tissue. In addition, a blood pressure may be measured directly by the functional skin patch **100** or by use of an implanted device, as will be discussed below. The blood heparin value may be measured invasively or non-invasively by the functional skin patch **100** in an analogous way as the blood sugar value.

[0041] The thermo harvester **210** may comprise an energy storage unit **220** for storing the harvested body energy. The energy storage unit **220** may be a rechargeable battery or a capacitor being configured to store sufficient energy for providing a long term monitoring of the body health parameters. The size of the energy storage unit **220** is only limited by the thickness of the functional unit **200**. To provide an energy storage unit **220** having a low thickness, printed energy storage devices or printed supercapacitors may be used.

[0042] Further, the functional unit **200** may comprise a processing unit **250** for processing measurement data of the sensor unit **240** and for transmitting the measurement data to the RF-circuit **230**. The processing unit **250** may be integrated in a monolithic circuit. Thus, at least one body health parameter may be measured by the sensor unit **240** and transmitted to the processing unit **250**, which processes or analyses the measurement data of the sensor unit **240**. The processed measurement data is then transmitted from the processing unit **250** to the RF-circuit **230**. The RF-circuit **230** generates a radio frequency (RF) signal modulated by the measurement data information and transmits the RF-signal via the connection plug **235** to the antenna layer **330**. As can be seen from FIG. 5A, the RF-signal is then radiated from the antenna layer **330** to be received by an external receiver to receive the measurement data from the sensor unit **240**. The RF-circuit **230** may also be configured to receive RF-signals from an external transceiver to receive instructions for operating the functional unit **200**.

[0043] As can be seen from FIGS. 5A and 5B, the metal layer **310** may be a flexible metal foil having a thickness in a range between 5 μ m and 1000 μ m. The thickness of the metal layer **310** may be also in a range between 5 μ m to 300 μ m, or in a range of 50 μ m to 100 μ m. The flexible metal foil may comprise copper to optimally spread the heat energy over the complete surface of the functional skin patch **100**.

[0044] The ferrite layer 320 may be a flexible ferrite foil having a thickness in a range between 5 μm and 1000 μm . The thickness of the ferrite layer 320 may also have, comparable to the metal layer 310, a thickness in a range between 5 μm to 300 μm or in a range between 50 μm to 100 μm . The flexible ferrite foil of the ferrite layer 320 is configured to shield the RF-field of the antenna 332, as can be seen from FIG. 5A. Ferrite foils are electrical isolators and have a relatively high heat conductivity. In particular, in case of a small thickness of lower than 100 μm a good heat transfer may be achieved to the environment of air. The ferrite layer 320 may include a ferrite material such as Fe_2O_3 or Fe_3O_4 , and may further include, for adapting the magnetic properties, MnZn-ferrite such as $\text{Mn}_x\text{Zn}_{(1-x)}\text{Fe}_2\text{O}_4$, or NiZn-ferrite such as $\text{Ni}_x\text{Zn}_{(1-x)}\text{Fe}_2\text{O}_4$. The antenna layer 330 includes an antenna pattern 332, which is printed on the ferrite layer 320. The printed antenna patterned may be realized by a silver printing in an inkjet process. Thus, the antenna layer 330 is not a continuous layer but a patterned layer being configured to form an antenna structure, as can be seen, for example in FIG. 7A. The antenna pattern 332 may thus have a form of a loop antenna as used, for example for RF-ID antennas. As can be seen from FIG. 5A, the metal layer 310, the ferrite layer 320 and the antenna layer 330 may be in direct contact with each other to maximize the heat conductance between these three layers.

[0045] It has been found that the specific thermal resistance of the stacked layer structure of the metal layer 310 and the ferrite layer 320 is lower than the thermal resistance of the metal layer 310 and the ferrite layer 320 taken alone. This results from the transfer thermal resistance of the metal layer 310 or 320 to the surrounding air. In case only the ferrite layer 320 or the ferrite foil is used, a high thermal transfer resistance results from the low specific heat conductance of ferrite and thus for the lack of sufficient spreading of the heat to the complete second surface 102. In case only a metal layer 310 such as a copper foil is used, the thermal resistance is reduced resulting from the high specific heat conductance of metal and the good spreading properties of the heat over the complete second surface 102. Nonetheless, the surface of the metal foil of the metal layer 310 is very smooth.

[0046] The combination of the metal layer 310 and the ferrite layer 320 leads to overall higher heat conductance properties. The metal in the metal foil of the metal layer 310 leads to a good spreading of the heat over the complete second surface 102, wherein the ferrite layer 320 having a thickness of only 50 μm to 300 μm achieves a good radiation of the heat due to its intrinsic surface roughness. The surface roughness of the ferrite layer 320 results in a reduced thermal transfer resistance to the surrounding air.

[0047] Taking the example of measuring a thermal resistance of a plaster having a size of 60 mm $\times$ 90 mm, the thermal resistance of the ferrite layer 320 has been determined to 313.10 K/W and the thermal resistance of the metal foil of the metal layer 310 has been determined to 14.52 K/W. This results in a specific surface thermal resistance of the metal foil of the metal layer 310 of 2.60 K/(W cm^2) and of the ferrite layer 320 of 5.79 K/(W cm^2). A combination of the metal layer 310 and the ferrite layer 320 having an overall thickness of 300 μm results in a thermal resistance of 108.00 $\mu\text{K}/\text{W}$ and a specific surface thermal resistance of 2.00 $\mu\text{K}/(\text{W } \text{cm}^2)$. Thus, a combination of the metal layer 310 and the ferrite layer 320 leads to a better heat conductance than the metal layer 310 or the ferrite layer 320 taken alone. Reducing the thickness of the stacked layer of the ferrite layer 320 and the

metal layer 310 to an overall thickness of 100 μm leads to thermal resistance values of 109.72 K/W and 2.03 K/(W cm^2) and the reduction of the thickness of the ferrite/metal layer to 50 μm leads to values of 118.63 K/W and 2.20 K/(W cm^2). Thus, the reduction of the overall thickness of the stacked layer structure of the metal layer 310 and the ferrite layer 320 down to even 50 μm still leads to better heat conductance values as the metal layer 310 or the ferrite layer 320 taken alone.

[0048] As can be seen from FIG. 6 and FIG. 7A to 7C, the antenna layer 330 may further comprise a metal dot layer 340 printed on the ferrite layer 320 for enhancing the surface area of the antenna layer 330. As can be seen from FIG. 7B and FIG. 7C, the metal dot layer 340 may be printed next to the antenna pattern 332 on the ferrite layer 320, to enhance the surface area of the second surface 102. Therefore, metal dots 342 having a thickness in a range of 1 μm to 10 μm may be printed on the ferrite layer 320. The diameter of the metal dots 342 may also be enhanced to a diameter in a range of 50 μm to 200 μm . However, due to the intrinsic surface roughness of the ferrite layer 320, the application of a metal dot layer 340 may further improve the heat transfer in case the metal dot layer 340 still leaves a sufficient surface area for the ferrite layer 320 being in contact with air. The metal dot layer 340 and the metal dots 342 are produced in a silver inkjet process or may be also generated in a screen printing.

[0049] FIG. 8 is a schematic perspective view of a system 1000 for monitoring a body health parameter. The system 1000 comprises the functional skin patch 100 as already described in detail above, but having a further functionality to communicate with an implantable device 500. Therefore, the functional skin patch 100 comprises the coupling antenna 260 for communicating with or energizing the implantable device 500, as will be discussed in detail below. As can be seen from FIGS. 8 and 9, the implantable device 500 may be embedded in the body tissue BT or in an subcutaneous area near to the body skin BS, to achieve communication between the implantable device 500 and the functional skin patch 100. The functional skin patch 100 may have in this embodiment the functionality of a so-called booster-plaster, which receives an external RF-signal from an external transceiver 600 by means of the antenna pattern 332, wherein the external RF-field is amplified or boosted to be sent to the implantable device 500 via the coupling antenna 260. Therefore, the antenna layer 330 may be connected to the coupling antenna 260 to boost transmission from the external transceiver 600 to the implantable device 500.

[0050] As can be seen from FIG. 9, the functional skin patch 100 comprises, comparable to the functional skin patch 100 as shown in FIG. 5A, an antenna layer 330, the ferrite layer 320 and the metal layer 310 as well as the thermo harvester 210 comprising a Peltier element 212, which may include Bi_2Te_3 , and a harvester circuit 214, which is configured to harvest the thermoelectric energy from the Peltier element 212. Thermoelectric power generation of the thermo harvester 210 may be based on the transfer of thermal energy through multiple couples of p-type and n-type thermoelectric legs. The thermo harvester 210 may use compounds of Bismuth (Bi), Antimony (Sb), Tellurium (Te) and Selenium (Se) providing optimal efficacy at operating temperatures around ambient and up to 85° C. The generated output voltage is proportional to the number of leg pairs and the actual temperature difference ΔT_{TEG} across the thermo harvester 210. The thermo harvester 210 may have a packing density of up to

100 thermoelectric leg pairs per mm^2 . As per Seebeck's law this translates into 1.4 V at as little as 10°C . of temperature difference ΔT_{TEG} . The thermo harvester **210** may have a thickness in a range between 0.2 mm to 5 mm, or 0.5 mm to 2 mm, or 0.5 mm to 1.5 mm. The surface area of the thermo harvester **210** may be in a range of 5 mm^2 to 20 mm^2 , or 5 mm^2 to 15 mm^2 , or 10 mm^2 to 15 mm^2 . The total number of leg pairs may be in a range between 200 and 1000, or between 300 and 600. The output voltage may be in a range between 100 mV/K to 200 mV/K. In addition, the functional unit **200** may further comprise an energizing unit **270**, which is configured to energize the implantable device **500** via the coupling antenna **260**.

[0051] The implantable device **500** may have the sensor unit **510** for measuring at least one body health parameter, the data transceiver unit **520** for transmitting measurement data containing the at least body health parameter to the functional skin patch **100**, and the energy receiving unit **530** for receiving electromagnetic energy from the coupling antenna **260** of the functional skin patch **100**, as already discussed with regard to FIG. 1B. In detail, the energy receiving unit **530** and the data transceiver unit **520** may use in common a coupling coil **522**, as shown in FIGS. 10A and 10B. Furthermore, the implantable device **500** may comprise an energy storage unit **524**, which may be a chargeable storage device. Herein, a silicon-based rechargeable lithium battery may be used. As silicon has highest lithium ion storage capacity/volume, even a very tiny-sized battery ($A < 1\text{ mm}^2$) may provide storage capacity in the order to up to 250 to 500 μAh , which is sufficient for various applications. The energy storage unit **524** may further comprise a capacitor. Herein, printed energy storage devices or printed supercapacitors may be used.

[0052] A coupling coil **262** (FIGS. 10A and 10B) of the coupling antenna **260** and the coupling coil **522** of the implantable device **500** may comprise at least one of a radio frequency identification (RFID/nearfield communication (NFC) antenna). The diameter of the coupling coil **262** of the coupling antenna **260** may be in the range of 1 mm to 10 mm and the diameter of the antenna pattern **332** of the antenna layer **330** may be in a range of 1 cm to 10 cm. RFID devices operate at different radio frequency ranges, e.g. low frequency (LF) at about 28 to 136 kHz, high frequency (HF) at about 13.56 MHz, and ultra-high frequency (UHF) at 860 to 960 MHz. Each frequency range has unique characteristic in terms of RFID performance.

[0053] NFC is a short range technology that enables two devices to communicate when they are brought into actual touching distance. NFC enables sharing power and data using magnetic field induction at 13.56 MHz (HF) band, at short range, supporting varying data rates from 106 kbps, 212 kbps to 424 kbps. A key feature of NFC is that it allows two devices to interconnect. In reader/writer mode, an NFC tag is a passive device that stores data that can be read by an NFC enable device. In peer-to-peer mode, two NFC devices can exchange data. Bluetooth or WiFi link set up parameters can be shared using NFC and data such as virtual business cards or digital photos can be exchanged. In card emulation mode, the NFC device itself acts as an NFC tag, appearing to an external interrogator as a traditional contact less smart card. These NFC standards are acknowledged by major standardisation bodies and based on ISO/IEC 18092.

[0054] Passive UHF systems use propagation coupling, where an interrogator antenna emits electromagnetic energy radio frequency waves and the RFID tag receives the energy

from the interrogator antenna, and the integrated circuit uses the energy to change the load on the antenna and reflect back an altered signal that is then demodulated. For the LF and HF RFID systems using interactive coupling, the range of the interrogator field is small (0.2 to 80 cm) and can be relatively easily controlled. UHF systems that use propagation coupling are harder to control, because energy is sent over long distances. The radio waves can reflect on hard surfaces and reach tags that are not in the normal range. LF and HF systems perform better than UHF systems around metal and water. The radio waves do reflect off metal and cause false reads, and they are better able to penetrate water. UHF radio waves are attenuated by water.

[0055] In addition, communication may be performed via any one of an Industrial, Scientific and Medical (ISM) Band, which operates in a frequency range between 6.765 MHz to 246 GHz and has bandwidths of up to 2 GHz.

[0056] The energy storage unit **524** is then configured to harvest energy from the coupling antenna **260** for charging the energy storage unit **524**. The energy harvesting may be controlled by a processor unit.

[0057] The sensor unit **510** may be also configured to measure at least one body health parameter as already discussed above with regard to the sensor unit **240** of the functional skin patch **100**. Furthermore, since the implantable device **500** is implanted in the body tissue, also invasive measurements like chemically analysing the interstitial fluid in the subcutaneous tissue may be performed. In addition, in case of implanting the implantable device **500** into a blood vessel, also blood pressure or blood flow may be measured by the implantable device **500**, wherein the measured data is transmitted to the coupling antenna **260** and then via the antenna layer **330** to the external transceiver **600**. The external transceiver **600** may be a mobile phone or a tablet PC being configured to communicate with the RF-circuit **230** of the functional skin patch **100** via the antenna pattern **332**.

[0058] In the following, an employment of the functional skin patch **100** operating as a booster plaster in two different modes A and B will be described.

[0059] As shown in FIG. 10A, in a first mode A, at least one body health parameter is measured by the sensor unit **510** of the implantable device **500** only in a case, if an external RF-field of the external transceiver **600** is applied, which leads to a punctual measurement process. A continuous measurement over a predetermined time range (long term monitoring) requires a repeated application of the external RF-field from the external transceiver **600**. Due to the provision of the thermo harvester **210** in the functional skin patch **100** according to an embodiment, the interface functionality of the functional skin patch **100** working as a booster plaster is enhanced by providing a local energy source within the functional skin patch **100**. The temperature difference between the skin and the environment is converted into electric energy via the thermoelectric energy harvesting of the thermo harvester **210**.

[0060] The locally generated energy is converted into an RF signal by a DC/AC transformer **274** and then applied to the coupling coil **262** of the coupling antenna **260** to be transferred to the implantable device **500**. Therefore, the energizing unit **270** comprises the DC/AC-transformer **274**, which is connected with the DC-terminal to the thermo harvester **210** and with the AC-terminal to the coupling antenna **260**. The RF-signal triggers a measurement process of the implantable device **500**. Thus, the functional unit **200** may further com-

prise a data storage unit **252** (cf. FIG. 5A and FIG. 6), wherein the functional unit **200** is configured to temporarily energize the implantable device **500**, to receive measurement data transmitted from the implantable device **500**, and to store the transmitted measurement data from the implantable device **500** in the data storage unit **252**. The stored data in the data storage unit **252** may be stored for a predetermined time until the data storage unit **252** is read out by the external transceiver **600** on demand.

[0061] In the first modus A, which is illustrated in FIG. 10A, an external field is applied by the external transceiver **600**, wherein the booster circuit of the functional skin patch **100** concentrates the field energy and transmits the concentrated field energy to the implantable device **500**. The booster circuit **350** of the functional skin patch **100** comprises a coupling coil **332a** of the antenna pattern **332**, the coupling coil **262** of the coupling antenna **260**, a first capacitor **334** and a second capacitor **264** for frequency tuning and intrinsic output resistances **336** mainly of the antenna unit **300**. The power transmission from the external transceiver **600** through the booster circuit **350** to the implantable device **500** is illustrated by the arrow E in FIG. 10A.

[0062] The energizing field from the external transceiver **600** is further used for communication. Thus, the implantable device **500** is energized and at the same time the measurement data can be read out. Further, the implantable device **500** may be configured or a continuous measurement may be performed in case the external transceiver **600** is in constant reach of the functional skin patch **100**, which may be the case for a smartphone constantly worn by a user wearing the functional skin patch **100** and the implantable device **500**. In the first modus A, the local energy storage unit **220** is deactivated. Thus, in the first modus A, power transmission and data communication with extend range using the booster antenna of the interface plaster or functional skin patch **100** from an RF-reader is performed to achieve continuous measurement operation and data read-out from the sensors memory.

[0063] In the second modus B, as shown in FIG. 10B, the thermo harvester **210** generates local electric energy. The energy is temporarily stored and may be used on demand for energizing the implantable device **500**. Therefore, an AC-signal is generated by the DC/AC-transformer **274** in predetermined repeated time ranges and directly applied to the coupling coil **262**, as can be seen from the arrow E' in FIG. 10B. Since the larger coupling coil **332a** of the antenna pattern **332** has higher intrinsic output resistances **336**, the current is mainly flowing through the coupling coil **262** of the coupling antenna **260**. A part of the energy is lost via the coupling coil **332a** of the antenna pattern **332**. The RF-field coupled into the implantable device **500** via the coupling coil **522** wakes the implantable device **500** up and triggers a measurement. The measurement result will be temporarily stored in the data storage unit **252**, as described above. Thus, in the second modus B, a continuous power generation by the energy harvesting circuit to the energy storage is performed. Duty cycled activation of the DC/AC-transformer **274** is performed to transmit power to the implantable device **500** and to activate measurement operation. The result is stored internally in a non-volatile memory unit or data storage unit **252** until read-out using an RF-reader of the external transceiver **600**. To perform the selective duty cycled activation of the implantable device **500**, the energizing unit **270** further com-

prises a switch **272** to selectively connect the energizing unit **270** with the thermo harvester **210**.

[0064] Thus, according to the embodiment of the functional skin patch **100** and the system for monitoring a body health parameter, continuous data logging of conventional implanted passive sensor grains using a smart booster antenna plaster may be achieved. In addition a maintenance free operation of the implanted sensor of the implantable device **500** may be achieved. Furthermore, direct RF-data communication via the booster antenna plaster or functional skin patch **100** using an external NFC device of the external transceiver **600** to read-out the measurement results is possible. A local (on-skin-power generation for trend measurements over the day without the need of an external field source leads to the possibility of performing a long term monitoring of body functions of a human or an animal for medical or scientific reasons.

[0065] Although specific embodiments have been illustrated and described herein, it will be appreciated by those of ordinary skill in the art that a variety of alternate and/or equivalent implementations may be substituted for the specific embodiments shown and described without departing from the scope of the present invention. This application is intended to cover any adaptations or variations of the specific embodiments discussed herein. Therefore, it is intended that this invention be limited only by the claims and the equivalents thereof.

What is claimed is:

1. A functional skin patch, comprising:

a first surface;

a second surface opposite the first surface;

a functional unit comprising a thermo harvester, the thermo harvester having a first terminal thermally connected to the first surface and a second terminal; and

an antenna unit having a first terminal thermally connected to the second terminal of the thermo harvester and a second terminal thermally connected to the second surface,

wherein the antenna unit has a stacked layer structure comprising, in this sequence, a metal layer thermally connected to the second terminal of the thermo harvester, a ferrite layer thermally connected to the metal layer, and an antenna layer thermally connected to the ferrite layer.

2. The functional skin patch of claim 1, wherein the metal layer is a flexible metal foil having a thickness in a range between 5 μm and 1000 μm .

3. The functional skin patch of claim 1, wherein the ferrite layer is a flexible ferrite foil having a thickness in a range between 5 μm and 1000 μm .

4. The functional skin patch of claim 1, wherein the antenna layer includes an antenna pattern printed on the ferrite layer.

5. The functional skin patch of claim 1, wherein the metal layer, the ferrite layer, and the antenna layer are in direct contact with each other.

6. The functional skin patch of claim 1, wherein the antenna layer further comprises a metal dot layer printed on the ferrite layer for enhancing the surface area of the antenna layer.

7. The functional skin patch of claim 1, wherein the area of the first and the second surfaces of the functional skin patch are in a range of 20 cm^2 to 500 cm^2 .

8. The functional skin patch of claim 1, further comprising:

a heat collector unit having a first terminal thermally connected to the first surface and a second terminal thermally connected to the first terminal of the thermo harvester; and

a thermally isolating layer,

wherein the thermo harvester is embedded in the thermally isolating layer.

9. The functional skin patch of claim 1, wherein the functional unit comprises an RF-circuit connected to the antenna layer via a connection plug extended through the metal layer and the ferrite layer.

10. The functional skin patch of claim 1, wherein the functional unit comprises a sensor unit configured to sense a body health parameter including at least one of a body temperature, a body pulse frequency, an electrocardiogram recording, an electroencephalogram recording, a body function, a blood sugar value, a blood pressure, and a blood heparin value.

11. The functional skin patch of claim 1, wherein the thermo harvester comprises an energy storage unit configured to store harvested body energy.

12. The functional skin patch of claim 1, wherein the functional unit comprises a processing unit configured to process measurement data of the sensor unit and transmit the measurement data to the RF-circuit.

13. The functional skin patch of claim 1, further comprising a coupling antenna configured to communicate with or energize an implantable device.

14. The functional skin patch of claim 13, wherein the antenna layer is connected to the coupling antenna so as to boost transmission from an external transceiver to the implantable device.

15. The functional skin patch of claim 13, wherein the functional unit comprises an energizing unit configured to energize the implantable device via the coupling antenna.

16. The functional skin patch of claim 15, wherein the energizing unit comprises a DC/AC-transformer having a DC-terminal connected to the thermo harvester and an AC-terminal connected to the coupling antenna.

17. The functional skin patch of claim 15, wherein the energizing unit comprises a switch configured to selectively connect the energizing unit with the thermo harvester.

18. The functional skin patch of claim 1, further comprising a data storage unit, wherein the functional unit is configured to temporarily energize the implantable device, to receive measurement data transmitted from the implantable device, and to store the transmitted measurement data from the implantable device in the data storage unit.

19. The functional skin patch of claim 1, wherein the thermo harvester comprises a Peltier element including Bi_2Te_3 .

20. A system for monitoring a body health parameter, comprising:

an implantable device; and

a functional skin patch,

wherein the functional skin patch comprises a first surface, a second surface opposite the first surface, a functional unit comprising a thermo harvester having a first terminal thermally connected to the first surface and a second terminal, an antenna unit having a first terminal thermally connected to the second terminal of the thermo harvester and a second terminal thermally connected to the second surface, and a coupling antenna configured to communicate with or energize the implantable device, wherein the antenna unit has a stacked layer structure comprising, in this sequence, a metal layer thermally connected to the second terminal of the thermo harvester, a ferrite layer thermally connected to the metal layer, and an antenna layer thermally connected to the ferrite layer, wherein the implantable device comprises a sensor unit configured to measure at least one body health parameter, a data transceiver unit configured to transmit measurement data containing the at least one body health parameter to the functional skin patch, and an energy receiving unit configured to receive electromagnetic energy from the coupling antenna of the functional skin patch.

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摘要(译)

提供具有第一表面和与第一表面相对的第二表面的功能性皮肤贴片。功能性皮肤贴片包括具有热采集器和天线单元的功能单元。热采集器具有热连接到第一表面的第一端子和第二端子。天线单元具有热连接到热采集器的第二端子的第一端子和热连接到第二表面的第二端子。天线单元具有堆叠层结构，该层叠结构按顺序包括热连接到热收集器的第二端子的金属层，热连接到金属层的铁氧体层，以及热连接到铁氧体层的天线层。

