



US007332784B2

(12) **United States Patent**
Mills et al.

(10) **Patent No.:** **US 7,332,784 B2**
(45) **Date of Patent:** ***Feb. 19, 2008**

(54) **METHOD OF PROVIDING AN
OPTOELECTRONIC ELEMENT WITH A
NON-PROTRUDING LENS**

(75) Inventors: **Michael A. Mills**, Mission Viejo, CA
(US); **James P. Coffin, IV**, Trabuco
Canyon, CA (US)

(73) Assignee: **Masimo Corporation**, Irvine, CA (US)

(*) Notice: Subject to any disclaimer, the term of this
patent is extended or adjusted under 35
U.S.C. 154(b) by 0 days.

This patent is subject to a terminal dis-
claimer.

(21) Appl. No.: **11/475,725**

(22) Filed: **Jun. 27, 2006**

(65) **Prior Publication Data**

US 2007/0007612 A1 Jan. 11, 2007

Related U.S. Application Data

(60) Continuation of application No. 10/337,058, filed on
Jan. 3, 2003, now Pat. No. 7,067,893, which is a
division of application No. 09/038,494, filed on Mar.
10, 1998, now Pat. No. 6,525,386.

(51) **Int. Cl.**
H01L 31/0203 (2006.01)
H01L 31/0232 (2006.01)

(52) **U.S. Cl.** **257/433; 257/432; 257/687;**
257/787

(58) **Field of Classification Search** **257/687,**
257/787, 432-433; H01L 31/0203, 31/0232
See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

3,769,974 A 11/1973 Smart et al.

3,981,023 A 9/1976 King et al.
4,182,956 A 1/1980 Funk, Jr. et al.
4,267,559 A 5/1981 Johnson et al.
4,698,730 A 10/1987 Sakai et al.
4,703,219 A 10/1987 Mesquida
4,733,094 A 3/1988 Carpentier et al.
4,841,344 A 6/1989 Heinen
4,880,304 A 11/1989 Jaeb et al.
4,889,311 A 12/1989 Anglin

(Continued)

FOREIGN PATENT DOCUMENTS

JP 60-96424 5/1985

(Continued)

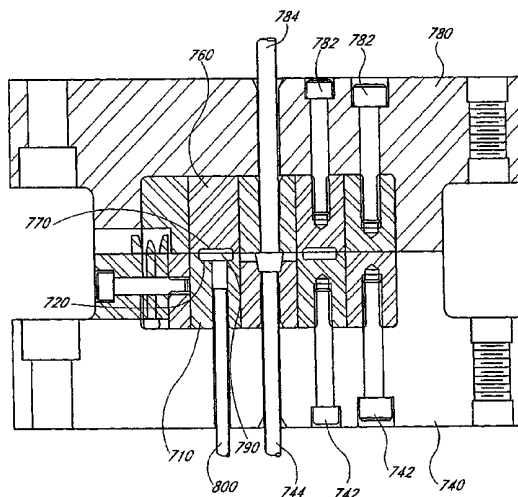
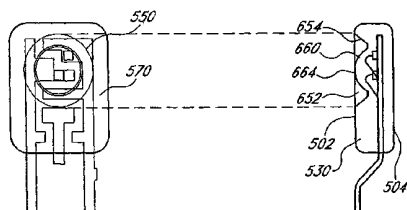
Primary Examiner—Theresa T Doan

(74) *Attorney, Agent, or Firm*—Knobbe Martens Olson &
Bear LLP

(57) **ABSTRACT**

An optoelectronic component has a lens that is formed in the surface of an encapsulant surrounding a semiconductor diode element. With respect to emitters, the lens reduces internal reflection and reduces dispersion to increase overall efficiency. With respect to detectors, the lens focuses photons on the active area of the detector, increasing detector sensitivity, which allows a detector having a reduced size and reduced cost for a given application. The lens portion of the encapsulant is generally non-protruding from the surrounding portions of the encapsulant reducing contact surface pressure caused by the optoelectronic component. This non-protruding lens is particularly useful in pulse oximetry sensor applications. The lens is advantageously formed with a contoured-tip ejector pin incorporated into the encapsulant transfer mold, and the lens shape facilitates mold release.

19 Claims, 14 Drawing Sheets



U.S. PATENT DOCUMENTS			
4,935,856 A	6/1990	Dragoon	5,913,819 A 6/1999 Taylor et al.
4,946,242 A	8/1990	Tanno et al.	5,919,134 A 7/1999 Diab
4,959,761 A	9/1990	Critelli et al.	5,934,925 A 8/1999 Tobler et al.
4,960,128 A	10/1990	Gordon et al.	5,940,182 A 8/1999 Lepper, Jr. et al.
4,964,408 A	10/1990	Hink et al.	5,970,749 A 10/1999 Bloom
5,041,187 A	8/1991	Hink et al.	5,985,214 A 11/1999 Stylli et al.
5,069,213 A	12/1991	Polczynski	5,995,855 A 11/1999 Kiani et al.
5,130,531 A	7/1992	Ito et al.	5,997,343 A 12/1999 Mills et al.
5,163,438 A	11/1992	Gordon et al.	6,002,952 A 12/1999 Diab et al.
5,249,576 A	10/1993	Goldberger et al.	6,011,986 A 1/2000 Diab et al.
5,296,715 A	3/1994	Kronberg	6,027,452 A 2/2000 Flaherty et al.
5,317,149 A *	5/1994	Uebbing et al. 250/231.14	6,036,642 A 3/2000 Diab et al.
5,337,744 A	8/1994	Branigan	6,045,509 A 4/2000 Caro et al.
5,347,605 A	9/1994	Isaksson	6,067,462 A 5/2000 Diab et al.
D353,195 S	12/1994	Savage et al.	6,081,735 A 6/2000 Diab et al.
D353,196 S	12/1994	Savage et al.	6,088,607 A 7/2000 Diab et al.
5,387,122 A	2/1995	Goldberger et al.	6,110,522 A 8/2000 Lepper, Jr. et al.
5,419,697 A	5/1995	Hirano et al.	6,144,868 A 11/2000 Parker
5,431,170 A	7/1995	Mathews	6,151,516 A 11/2000 Kiani-Azarbayjany et al.
D361,840 S	8/1995	Savage et al.	6,152,754 A 11/2000 Gerhardt et al.
D362,063 S	9/1995	Savage et al.	6,157,850 A 12/2000 Diab et al.
5,452,717 A	9/1995	Branigan et al.	6,165,005 A 12/2000 Mills et al.
5,453,961 A	9/1995	Brazas	6,184,521 B1 2/2001 Coffin, IV et al.
RE35,069 E	10/1995	Hallenbeck et al.	6,206,830 B1 3/2001 Diab et al.
D363,120 S	10/1995	Savage et al.	6,229,856 B1 5/2001 Diab et al.
5,482,036 A	1/1996	Diab et al.	6,236,872 B1 5/2001 Diab et al.
5,485,317 A	1/1996	Perissinotto et al.	6,252,252 B1 6/2001 Kunii et al.
5,485,538 A	1/1996	Bowen et al.	6,256,523 B1 7/2001 Diab et al.
5,487,124 A	1/1996	Bowen et al.	6,263,222 B1 7/2001 Diab et al.
5,488,468 A	1/1996	Kawanishi et al.	6,274,924 B1 8/2001 Carey et al.
5,490,505 A	2/1996	Diab et al.	6,278,522 B1 8/2001 Lepper, Jr. et al.
5,494,043 A	2/1996	O'Sullivan et al.	6,280,213 B1 8/2001 Tobler et al.
5,506,445 A	4/1996	Rosenberg	6,285,896 B1 9/2001 Tobler et al.
5,516,727 A	5/1996	Broom	6,321,100 B1 11/2001 Parker
5,533,511 A	7/1996	Kaspari et al.	6,334,065 B1 12/2001 Al-Ali et al.
5,559,358 A	9/1996	Burns et al.	6,343,224 B1 1/2002 Parker
5,562,002 A	10/1996	Lalin	6,349,228 B1 2/2002 Kiani et al.
5,578,156 A	11/1996	Kamakura et al.	6,360,114 B1 3/2002 Diab et al.
5,590,649 A	1/1997	Caro et al.	6,371,921 B1 4/2002 Caro et al.
5,602,924 A	2/1997	Durand et al.	6,374,129 B1 * 4/2002 Chin et al. 600/322
5,625,733 A	4/1997	Frigo et al.	6,377,829 B1 4/2002 Al-Ali
5,631,987 A	5/1997	Lasky et al.	6,388,240 B2 5/2002 Schulz et al.
5,632,272 A	5/1997	Diab et al.	6,397,091 B2 5/2002 Diab et al.
5,638,816 A	6/1997	Kiani-Azarbayjany et al.	6,430,525 B1 8/2002 Weber et al.
5,638,818 A	6/1997	Diab et al.	6,463,311 B1 10/2002 Diab
5,645,440 A	7/1997	Tobler et al.	6,470,199 B1 10/2002 Kopotic et al.
5,678,544 A	10/1997	DeLonzor et al.	6,501,975 B2 12/2002 Diab et al.
5,685,299 A	11/1997	Diab et al.	6,515,273 B2 2/2003 Al-Ali
D393,830 S	4/1998	Tobler et al.	6,519,487 B1 2/2003 Parker
5,743,261 A	4/1998	Mainiero et al.	6,525,386 B1 2/2003 Mills et al.
5,743,262 A	4/1998	Lepper, Jr. et al.	6,526,300 B1 2/2003 Kiani et al.
5,758,644 A	6/1998	Diab et al.	6,541,756 B2 4/2003 Schulz et al.
5,760,910 A	6/1998	Lepper, Jr. et al.	6,542,764 B1 4/2003 Al-Ali et al.
5,769,785 A	6/1998	Diab et al.	6,580,086 B1 6/2003 Schulz et al.
5,782,757 A	7/1998	Diab et al.	6,584,336 B1 6/2003 Ali et al.
5,785,659 A	7/1998	Caro et al.	6,595,316 B2 7/2003 Cybulski et al.
5,791,347 A	8/1998	Flaherty et al.	6,597,933 B2 7/2003 Kiani et al.
5,803,579 A	9/1998	Turnbull et al.	6,606,511 B1 8/2003 Ali et al.
5,806,579 A	9/1998	Judkins	6,632,181 B2 10/2003 Flaherty et al.
5,807,248 A	9/1998	Mills	6,640,116 B2 10/2003 Diab
5,810,734 A	9/1998	Caro et al.	6,643,530 B2 11/2003 Diab et al.
5,823,950 A	10/1998	Diab et al.	6,650,917 B2 11/2003 Diab et al.
5,830,131 A	11/1998	Caro et al.	6,654,624 B2 11/2003 Diab et al.
5,833,618 A	11/1998	Caro et al.	6,658,276 B2 12/2003 Kiani et al.
5,844,722 A	12/1998	Stephens et al.	6,661,161 B1 12/2003 Lanzo et al.
5,852,696 A	12/1998	Collins et al.	6,671,531 B2 12/2003 Al-Ali et al.
5,855,994 A	1/1999	Biebuyck et al.	6,678,543 B2 1/2004 Diab et al.
5,860,919 A	1/1999	Kiani-Azarbayjany et al.	6,684,090 B2 1/2004 Ali et al.
5,864,146 A	1/1999	Karellas	6,684,091 B2 1/2004 Parker
5,890,929 A	4/1999	Mills et al.	6,697,656 B1 2/2004 Al-Ali
5,904,654 A	5/1999	Wohltmann et al.	6,697,658 B2 2/2004 Al-Ali
			RE38,476 E 3/2004 Diab et al.
			6,699,194 B1 3/2004 Diab et al.

6,714,804 B2	3/2004	Al-Ali et al.	6,970,792 B1	11/2005	Diab
RE38,492 E	4/2004	Diab et al.	6,979,812 B2	12/2005	Al-Ali
6,721,585 B1	4/2004	Parker	6,985,764 B2	1/2006	Mason et al.
6,725,075 B2	4/2004	Al-Ali	6,993,371 B2	1/2006	Kiani et al.
6,735,459 B2	5/2004	Parker	6,996,427 B2	2/2006	Ali et al.
6,745,060 B2	6/2004	Diab et al.	6,999,904 B2	2/2006	Weber et al.
6,760,607 B2	7/2004	Al-Ali	7,003,338 B2	2/2006	Weber et al.
6,770,028 B1	8/2004	Ali et al.	7,003,339 B2	2/2006	Diab et al.
6,771,994 B2	8/2004	Kiani et al.	7,015,451 B2	3/2006	Dalke et al.
6,792,300 B1	9/2004	Diab et al.	7,024,233 B2	4/2006	Ali et al.
6,813,511 B2	11/2004	Diab et al.	7,027,849 B2	4/2006	Al-Ali
6,816,741 B2	11/2004	Diab	7,030,749 B2	4/2006	Al-Ali
6,822,564 B2	11/2004	Al-Ali	7,039,449 B2	5/2006	Al-Ali
6,826,419 B2	11/2004	Diab et al.	7,041,060 B2	5/2006	Flaherty et al.
6,830,711 B2 *	12/2004	Mills et al. 264/1.32	7,044,918 B2	5/2006	Diab
6,850,787 B2	2/2005	Weber et al.	7,067,893 B2	6/2006	Mills et al.
6,850,788 B2	2/2005	Al-Ali	7,096,052 B2	8/2006	Mason et al.
6,852,083 B2	2/2005	Caro et al.	7,096,054 B2	8/2006	Abdul-Hafiz et al.
6,861,639 B2	3/2005	Al-Ali	FOREIGN PATENT DOCUMENTS		
6,898,452 B2	5/2005	Al-Ali et al.			
6,920,345 B2	7/2005	Al-Ali et al.	JP	360096424 A	5/1985
6,931,268 B1	8/2005	Kiani-Azarbayjany et al.	JP	404025185 A	1/1992
6,934,570 B2	8/2005	Kiani et al.	JP	404025185 A *	1/1992
6,939,305 B2	9/2005	Flaherty et al.	JP	6-310550	11/1994
6,943,348 B1	9/2005	Coffin IV	* cited by examiner		
6,950,687 B2	9/2005	Al-Ali			
6,961,598 B2	11/2005	Diab			

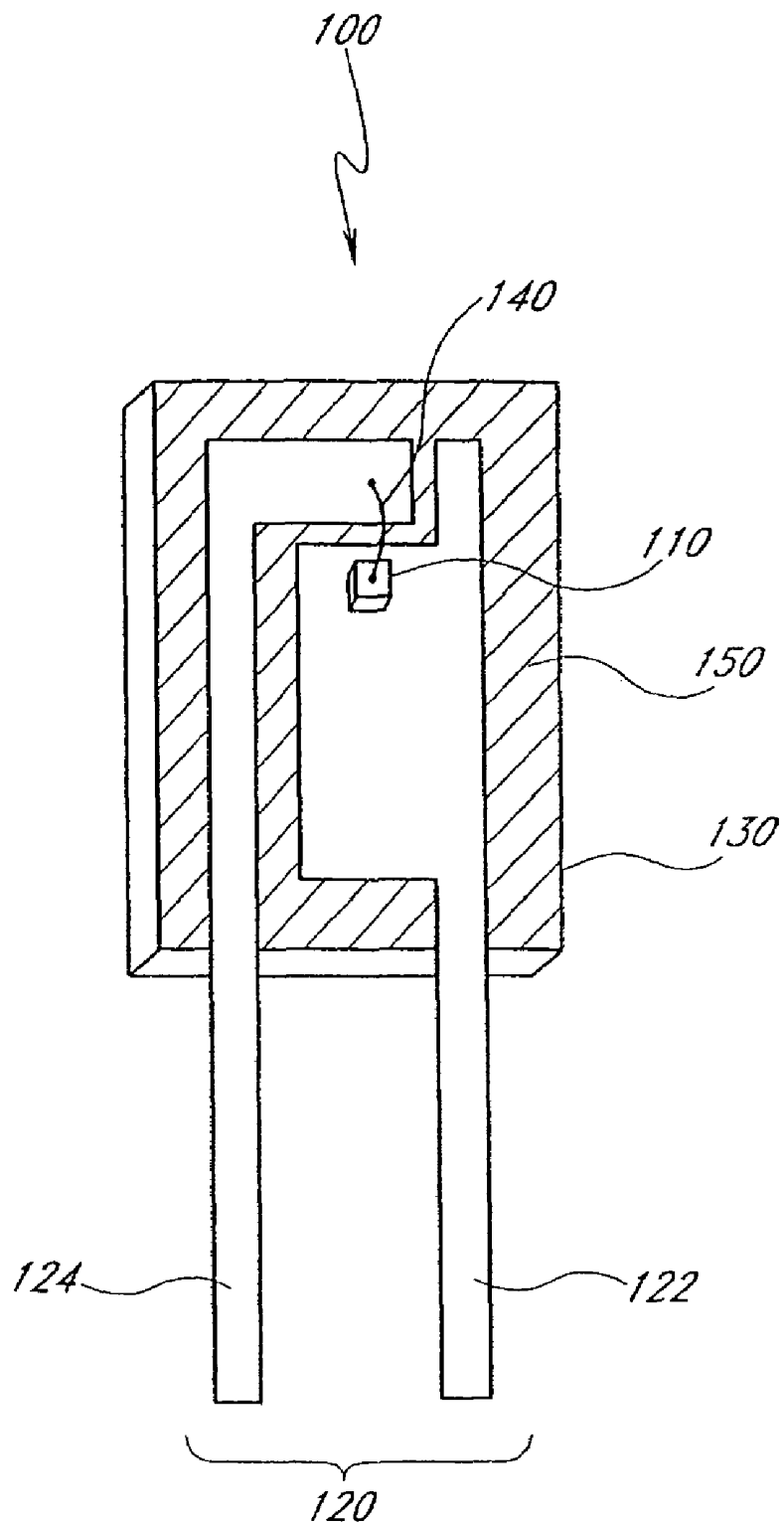


FIG. 1
(PRIOR ART)

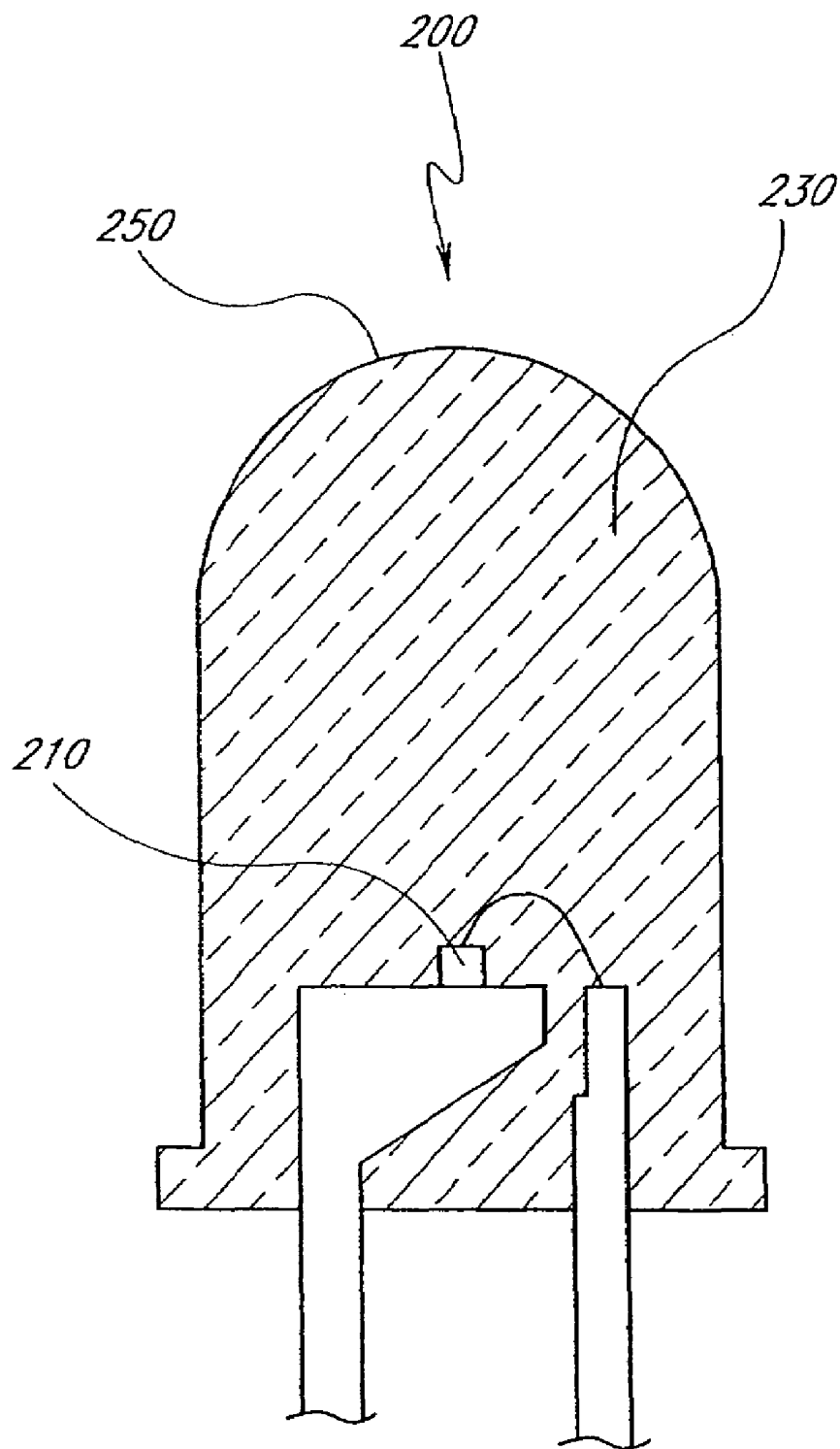
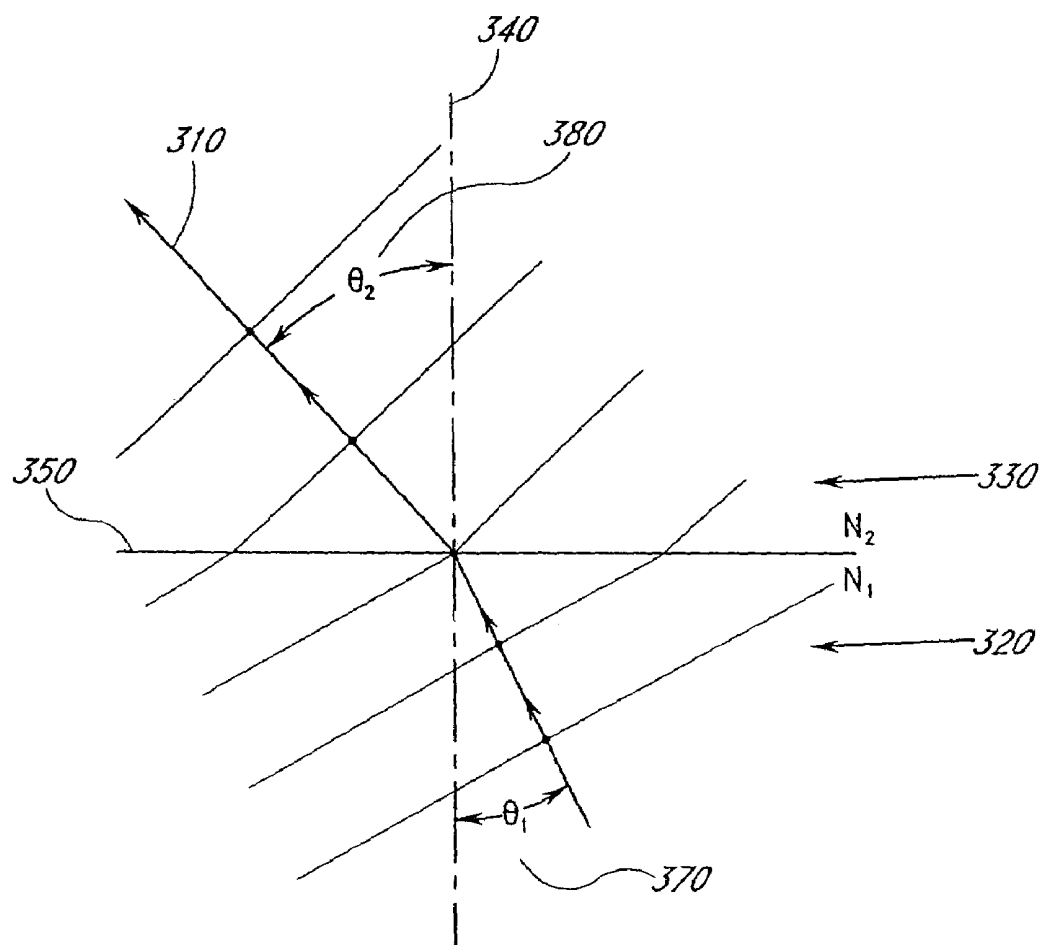
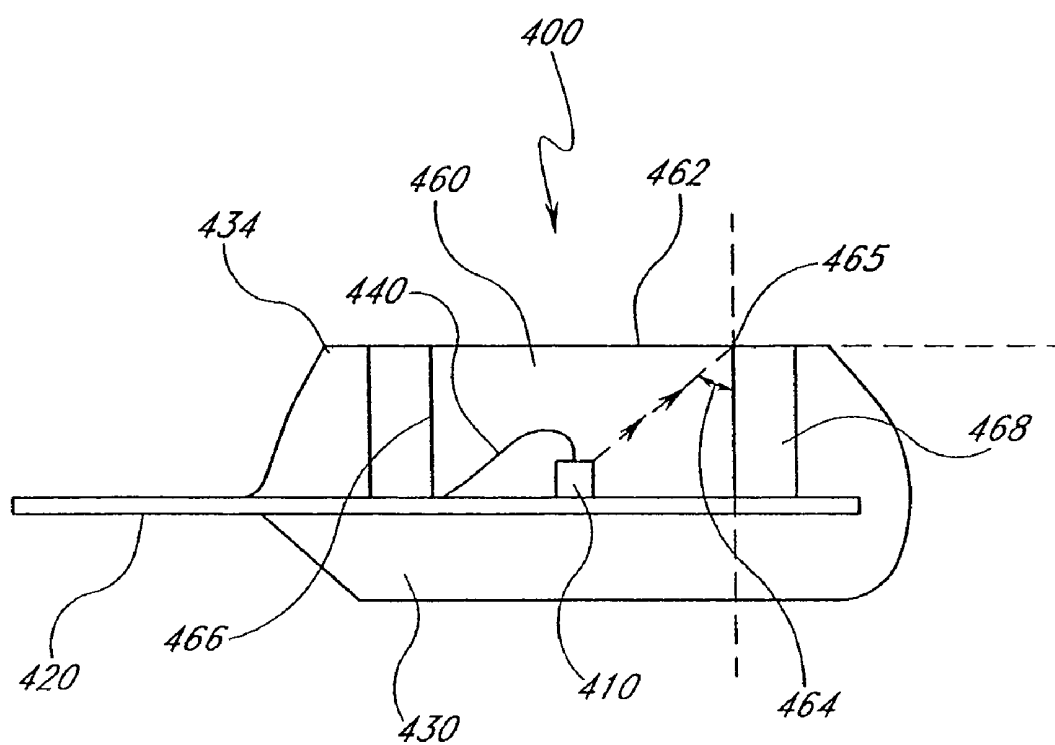
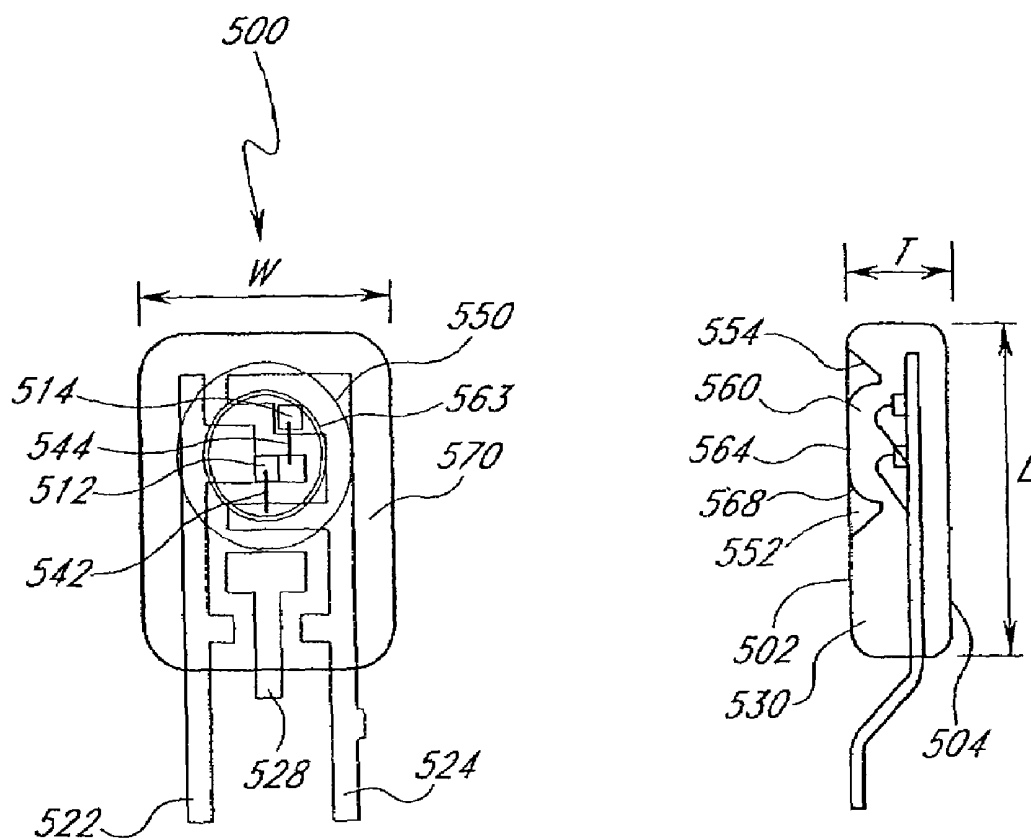
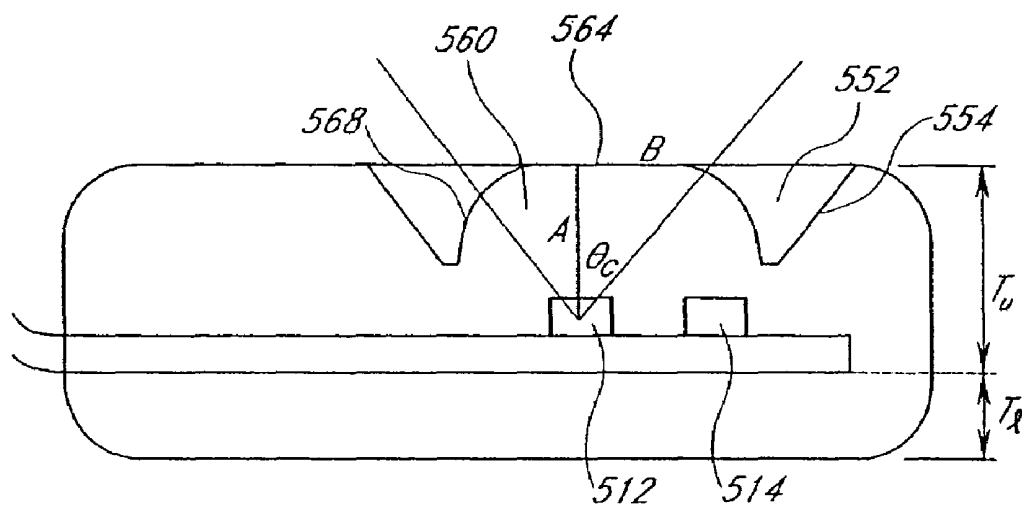


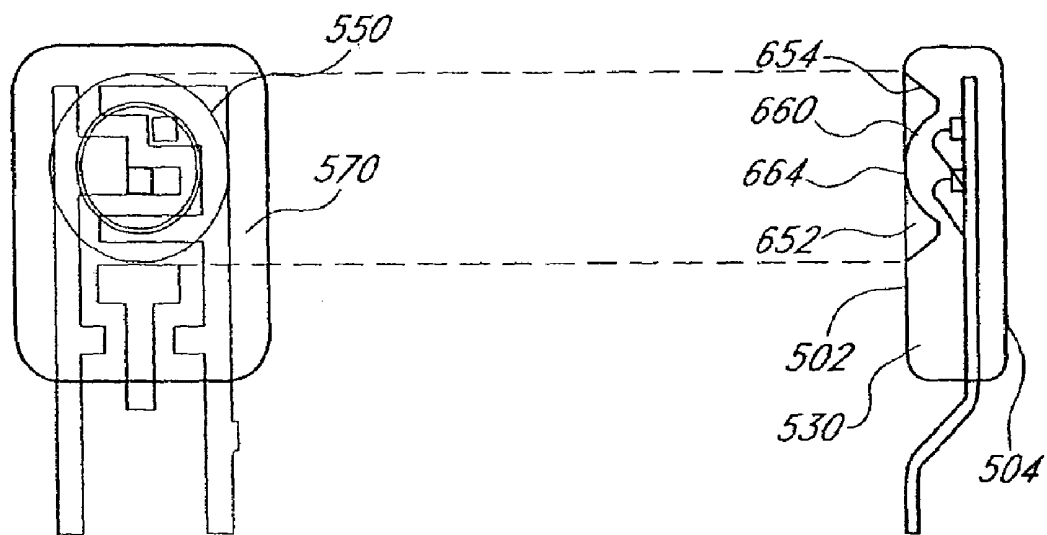
FIG. 2
(PRIOR ART)

**FIG. 3**

**FIG. 4**

**FIG. 5A**

**FIG. 5B**

*FIG. 6*

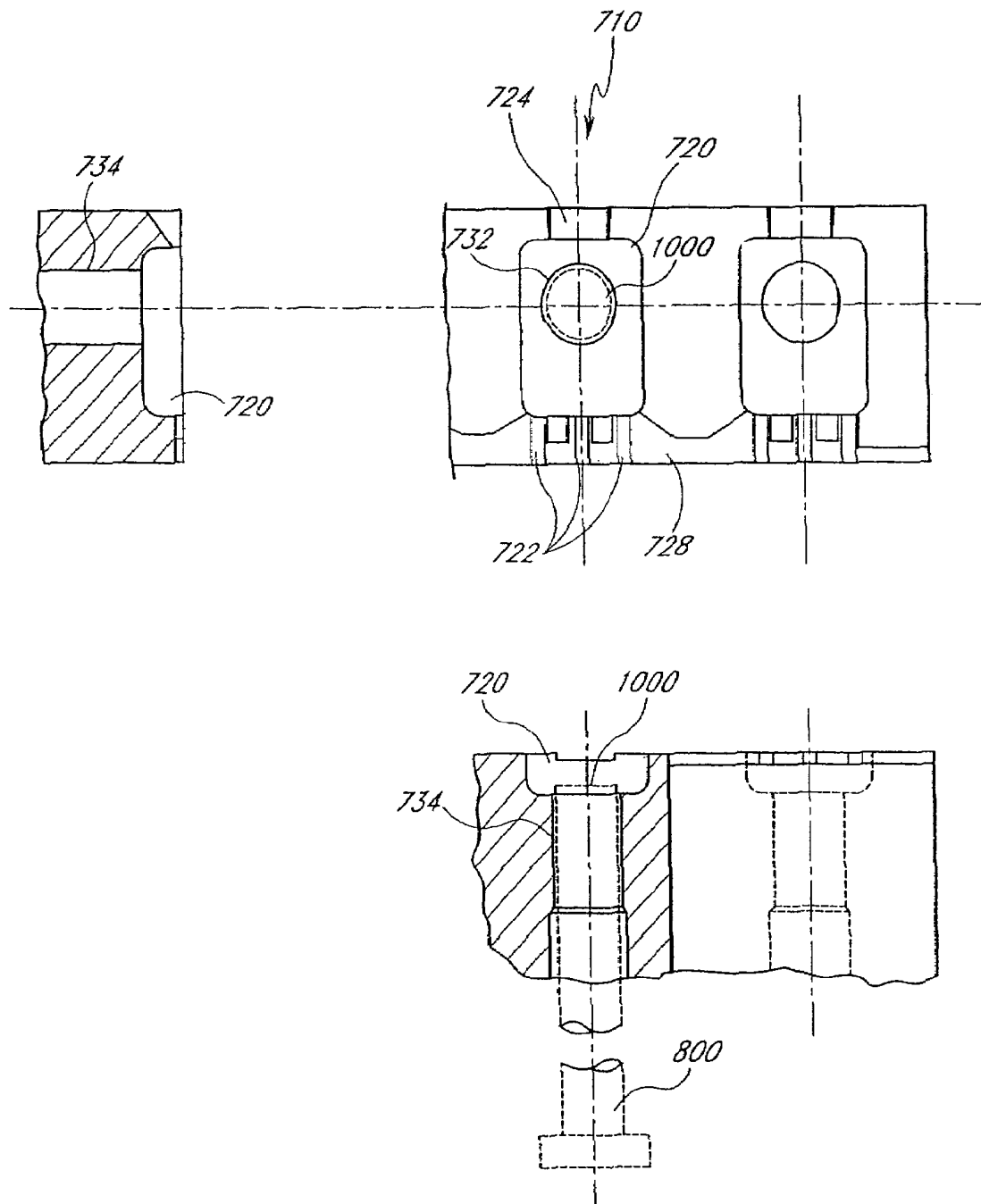


FIG. 7A

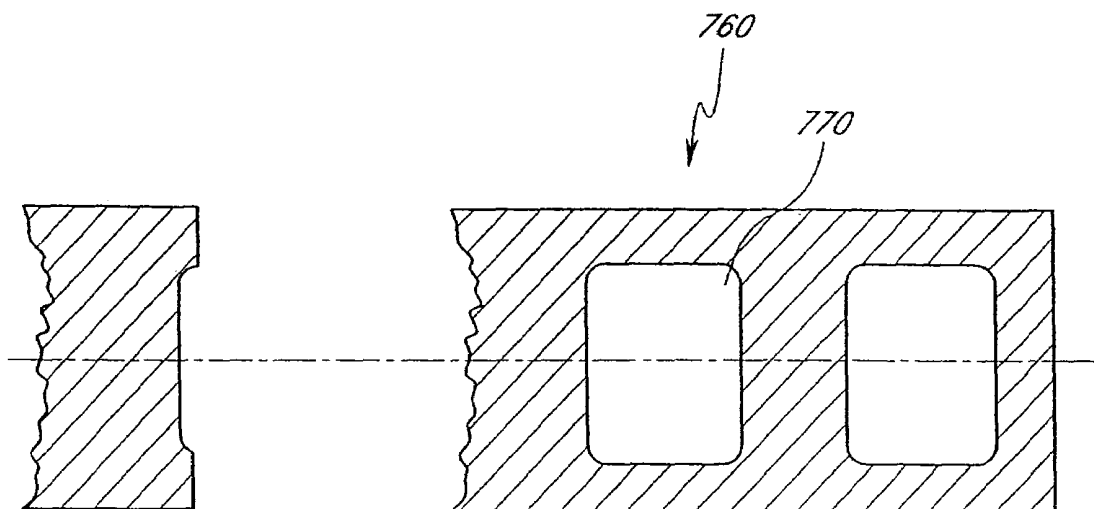
*FIG. 7B*

FIG. 7C

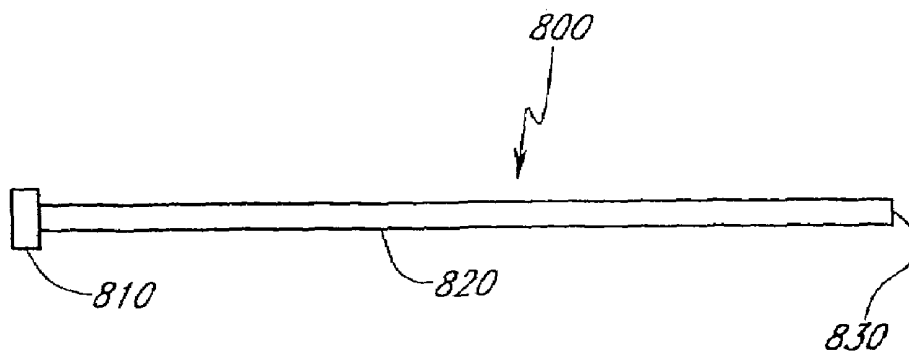


FIG. 8A
(PRIOR ART)

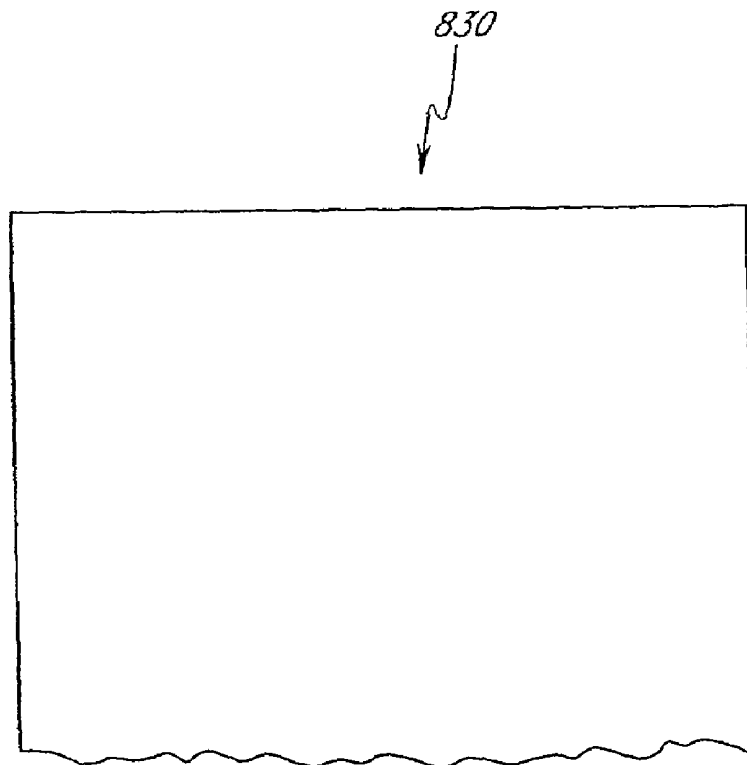


FIG. 8B
(PRIOR ART)

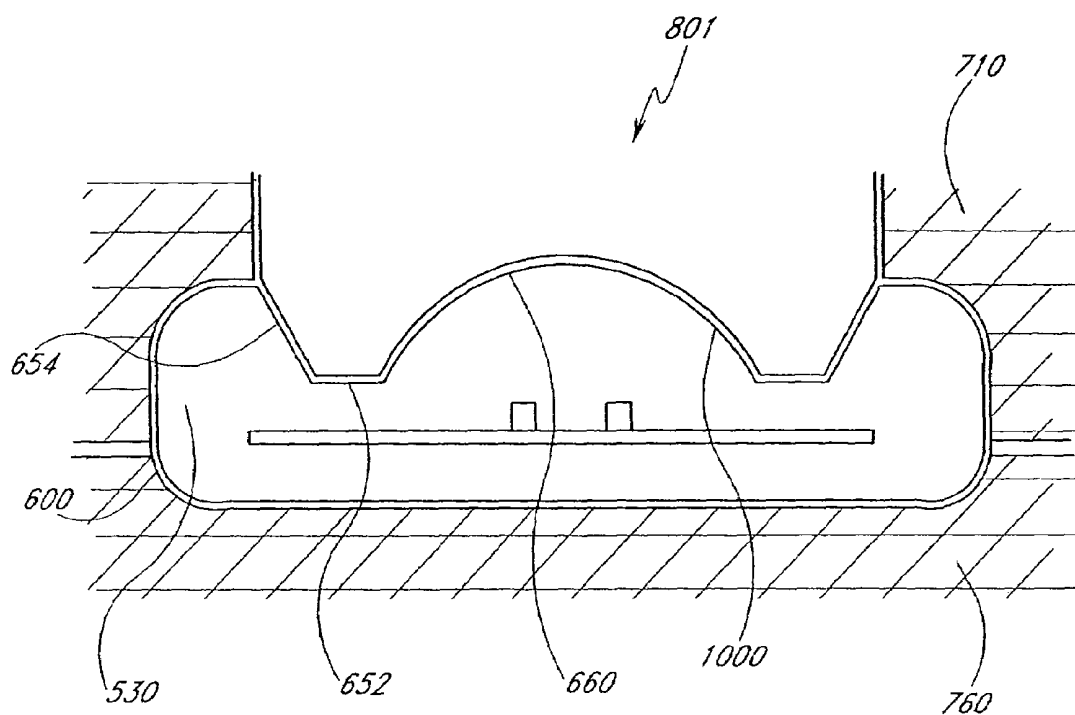
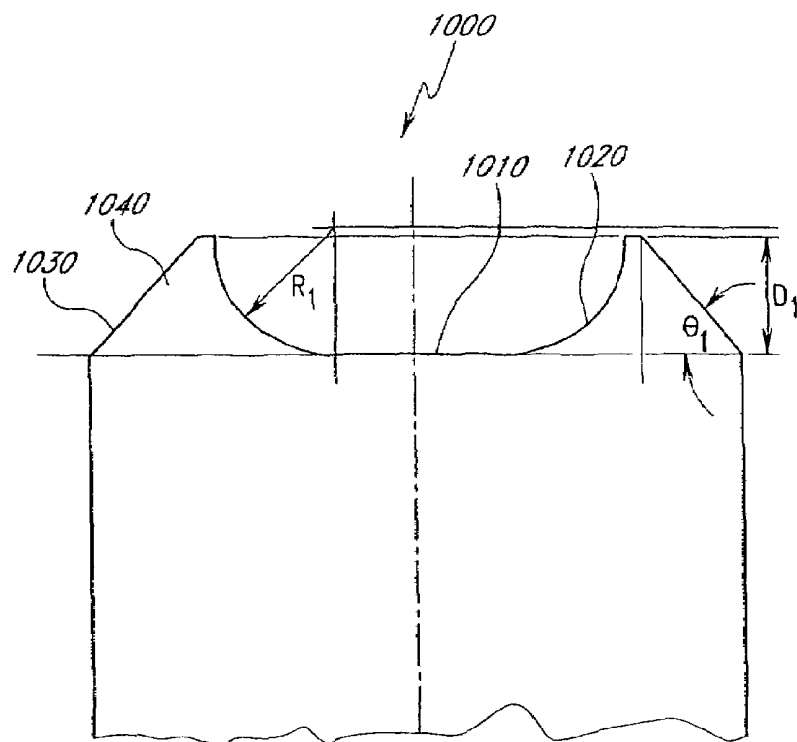
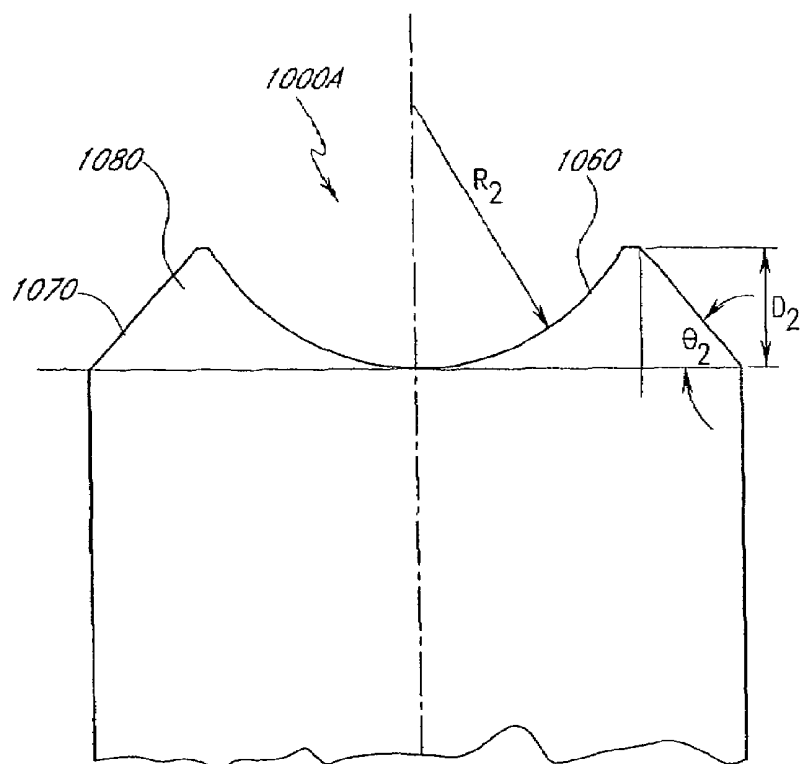
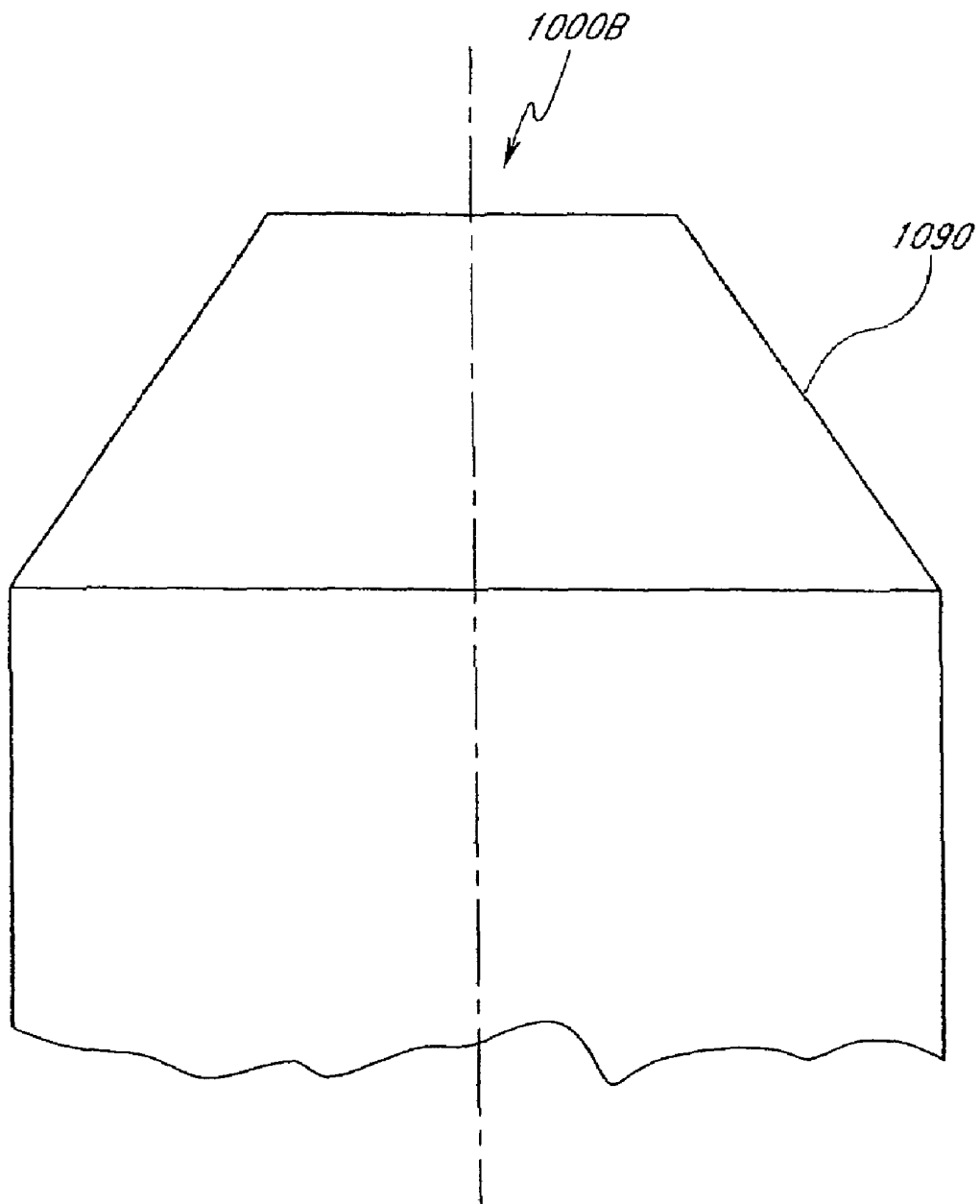


FIG. 9

**FIG. 10A****FIG. 10B**

*FIG. 10C*

METHOD OF PROVIDING AN OPTOELECTRONIC ELEMENT WITH A NON-PROTRUDING LENS

CLAIM OF PRIORITY

This application a continuation of U.S. patent application Ser. No. 10/337,058, filed Jan. 3, 2003 now U.S. Pat. No. 7,067,893, which is a divisional of U.S. patent application Ser. No. 09/038,494 filed Mar. 10, 1998 (now U.S. Pat. No. 6,525,386). The present application also incorporates the foregoing utility disclosures herein by reference.

BACKGROUND OF THE INVENTION

1. Field of the Invention

This invention relates to the field of optoelectronics, which includes light emitting components, such as light emitting diodes (LED) and laser diodes, and which also includes light detecting components, such as photodiodes, phototransistors, photodarlington and photovoltaic cells. Optoelectronics also includes various devices which incorporate optoelectronic components, such as displays, photo-sensors, optocouplers, and fiberoptic transmitters and receivers. In particular, this invention relates to lenses to increase the efficiency of optoelectronic emitters and the sensitivity of optoelectronic detectors.

2. Description of the Related Art

A prior art LED **100** is shown in FIG. **1** and consists of a semiconductor diode element **110** electrically connected to a leadframe **120** and surrounded by an encapsulating material **130**. The diode element **110** is typically mounted to one lead **122** of the leadframe **120** and connected to a second lead **124** of the leadframe **120** by a wire bond **140**. These two leads provide an electrical connection between an external current source and the anode and cathode of the diode element **110**. The external current source supplies power to the diode device **100** that is converted to emitted light by the photoelectric effect, which occurs at the semiconductor junction within the diode element **110**.

Internal inefficiencies within a semiconductor diode result in very low net efficiencies, which is the ratio of emitted light power to input power. Internal inefficiencies arise from a low ratio of minority carriers injected into the diode semiconductor junction to photons generated at the junction; photon loss due to internal reflection at the semiconductor/encapsulant interface; and absorption of photons within the semiconductor material. Because of these low net efficiencies, many LED applications require high input current, resulting in heat dissipation and device degradation problems in order to obtain sufficient light.

As illustrated in FIG. **1**, the encapsulant **130** forms a flat light-transmitting surface **150**. A flat surface is convenient in many applications where the LED is mounted to another surface that is also generally flat or in applications that otherwise cannot accommodate a protruding surface. The inefficiencies described above, however, are compounded by the configuration of the LED encapsulant/air interface. An encapsulant having a flat surface, such as in FIG. **1**, allows photons transmitted by the diode element **110** to have considerable dispersion. A flat encapsulant surface also results in internal reflection at the encapsulant/air interface, further reducing photon transmission and increasing photon absorption within the encapsulant material.

FIG. **2** illustrates a prior art LED **200** having an encapsulant **230** that forms a spherical surface **250**. A spherical or other curved surface gives a larger angle of incidence for

photons emitted from the semiconductor diode element **210**, reducing losses due to internal reflection. Further, this surface **250** acts as a lens to reduce the dispersion of generated photons. Unfortunately, a protrusion, such as this curved surface, is difficult to accommodate in many applications.

SUMMARY OF THE INVENTION

An optoelectronic device according to the present invention incorporates a lens that increases component performance. For example, the output of an LED utilizing the lens is increased by, in part, reducing internal reflection. Internal reflection results from the differing indices of refraction at the interface between the LED encapsulant and the surrounding air.

As shown in FIG. **3**, when a light ray **310** passes from a media having a higher index of refraction **320** to a media having a lower index of refraction **330**, the ray **310** is refracted away from the normal **340** to the surface **350**. The angle, θ_1 , is customarily referred to as the angle of incidence **370** and the angle θ_2 is customarily referred to as the angle of refraction **380**. As the angle of incidence **370** is increased, the angle of refraction **380** increases at a greater rate, in accordance with Snell's Law:

$$\sin \theta_2 = (N_1/N_2) \sin \theta_1,$$

where ($N_1 > N_2$). When the angle of incidence **370** reaches a value such that $\sin \theta_1 = N_2/N_1$, then $\sin \theta_2 = 1.0$ and $\theta_2 = 90^\circ$. At this point none of the light is transmitted through the surface **350**, the ray **310** is totally reflected back into the denser medium **320**, as is any ray which makes a greater angle to the normal **340**. The angle at which total reflection occurs:

$$\theta_c = \arcsin N_2/N_1$$

is referred to as the critical angle. For an ordinary air-glass surface, where the index of refraction is 1.5, the critical angle is about 42° . For an index of 1.7, the critical angle is near 36° . For an index of 2.0, the critical angle is about 30° . For an index of 4.0, the critical angle is about 14.5° .

An optoelectronic device according to the present invention has an encapsulant that functions as a lens. For emitter applications, the lens reduces internal reflection and dispersion without having a protruding curved surface. Thus, LEDs utilizing the present invention have an improved efficiency compared with prior art flat-surfaced LEDs and similar devices, without the physical interface difficulties of the prior art curved-surface LEDs and similar devices. For detector applications, the lens focuses photons on the active area of the detector, increasing detector sensitivity. This increased detector sensitivity allows a detector having a reduced size, hence a reduced cost, to be used for a given application.

A particularly advantageous application of an optoelectronic device with a non-protruding lens is in pulse oximetry, and in particular, as an emitter in pulse oximetry probes. Pulse oximetry is the noninvasive measurement of the oxygen saturation level of arterial blood. Early detection of low blood oxygen saturation is critical because an insufficient supply of oxygen can result in brain damage and death in a matter of minutes. The use of pulse oximetry in operating rooms and critical care settings is widely accepted.

A pulse oximetry probe is a sensor having a photodiode which detects light projected through a capillary bed by, typically, red and infrared LED emitters. The probe is attached to a finger, for example, and connected to an

instrument that measures oxygen saturation by computing the differential absorption of these two light wavelengths after transmission through the finger. The pulse oximetry instrument alternately activates the LED emitters then reads voltages indicating the resulting intensities detected at the photodiode. A ratio of detected intensities is calculated, and an arterial oxygen saturation value is empirically determined based on the ratio obtained:

$$I_{red}/I_{ir} = \text{Ratio} \Rightarrow \% \text{ O}_2 \text{ Saturation}$$

Typically, a look up table or the like correlates the Ratio to saturation. The use of conventional LEDs within pulse oximetry probes has a number of drawbacks. Pulse oximetry performance is limited by signal-to-noise ratio which, in turn, is improved by high light output emitters. LEDs without lenses, such as illustrated in FIG. 1, are not optimized to transmit the maximum amount of light into the skin. LEDs with protruding lenses, such as illustrated in FIG. 2, create increased pressure on the skin, resulting in perfusion necrosis, i.e. a reduction of arterial blood flow, which is the medium to be measured. A solution to this problem in accordance with the present invention is an LED incorporating a non-protruding lens.

One aspect of the present invention is an optoelectronic device that comprises an encapsulant having a surface, a lens portion of the surface, and a filler portion having a generally planar surface. The filler portion is disposed around the lens, and the lens does not extend substantially beyond the plane of the generally planar surface. The optoelectronic device also comprises an optoelectronic element embedded in the encapsulant and operable at at least one wavelength of light. The lens being configured to transmit or receive the at least one wavelength.

Another aspect of the present invention is a mold tool for an optoelectronic device that comprises a first mold piece having a surface that defines a first cavity and an aperture within the first cavity. The mold tool also comprises a second mold piece having a surface which defines a second cavity. The first cavity and second cavity cooperate to form a molding compound into a predetermined shape. The mold tool further comprises an ejector pin having a contoured tip. The pin is movably located within the aperture between a first position retracted within the cavity and a second position extended from the aperture. In the first position, the tip constitutes an integral portion of the first cavity. In the second position, the ejector pin facilitates removal of the compound from the first cavity. The ejector pin tip at least partially defines the predetermined shape.

Another aspect of the present invention is an optoelectronic method comprising the steps of providing a generally planar surface at a predefined distance from an optoelectronic element, defining a light transmissive region of that surface within the critical angle of the optoelectronic element, and contouring the surface within the transmissive region without exceeding the predefined distance. These steps create a non-protruding lens for the optoelectronic element. In one embodiment, the transmissive region has a circular cross-section. The optoelectronic method can comprise the further step of shaping a surrounding region adjacent said transmissive region.

Yet another aspect of the present invention is an optoelectronic device comprising an encapsulant means for embedding an optoelectronic element and a lens means for conveying light between the optoelectronic element and a media surrounding the encapsulant means. In one embodiment, the optoelectronic device further comprises a flat surface means for providing a low-pressure contact surface

for the lens means. In that embodiment, the optoelectronic device can further comprise an arcuate surface means for avoiding total internal reflection of light from the flat surface means. In another embodiment, the optoelectronic device further comprises a surrounding surface means for providing a contact surface for the encapsulant from which the lens means does not protrude.

BRIEF DESCRIPTION OF THE DRAWINGS

The present invention is described in detail below in connection with the following drawing figures in which:

FIG. 1 is a cross-section view of a prior art LED having an encapsulant with a flat light-transmitting surface;

FIG. 2 is a cross-section view of a prior art LED incorporating a protruding, spherical light-transmitting surface;

FIG. 3 generally illustrates light refraction at a surface between two media having different indices of refraction;

FIG. 4 is a cross-section view of an LED incorporating a single emitter and a flat-surfaced, vertical-side lens according to the present invention;

FIG. 5A is a plan view of an LED incorporating dual-emitters and a flat-element, non-protruding lens;

FIG. 5B is an enlarged view of a portion of FIG. 5A illustrating the critical angle;

FIG. 6 is a plan view of another LED incorporating dual-emitters and a spherical-element, non-protruding LED lens;

FIG. 7A is a plan view of the lower cavity of a production mold tool for encapsulating an optoelectronic element;

FIG. 7B is a plan view of the upper cavity of a production mold tool for encapsulating an optoelectronic element;

FIG. 7C is a cross section view of the upper cavity and the lower cavity of a production mold tool in a closed position;

FIG. 8A is an illustration of a prior art ejector pin for a production mold tool;

FIG. 8B is a cross-section view of a prior art ejector pin tip;

FIG. 9 is a cross-section view of a non-protruding optoelectronic lens being formed in a mold tool with a contoured ejector pin tip according to the present invention;

FIG. 10A is a cross-section view of an ejector pin tip for creating a non-protruding optoelectronic lens featuring a flat surface element;

FIG. 10B is a cross-section view of an ejector pin tip for creating a non-protruding optoelectronic lens featuring a spherical surface element; and

FIG. 10C is a cross-section view of an ejector pin tip for creating a detector cavity.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

FIG. 4 illustrates an embodiment of an LED having a non-protruding or minimally protruding lens according to the present invention. The LED 400 consists of at least one semiconductor diode element 410, which is mounted to one lead of a leadframe 420 and connected to another lead of a leadframe 420 with a bond wire 440. The diode element 410, bond wire 440 and portions of the leadframe 420 are surrounded by an encapsulant 430. A lens 460 is molded into a portion of the encapsulant 430. The lens 460 has a generally flat, surface portion 462 that is at or below the plane of the surrounding surface portions 434 of the encapsulant 430. The lens extends radially from the diode element 410 out to the critical angle 464, at which point total internal reflection of photons emitted from the diode element would

occur. Past the critical angle **464**, the lens **460** has a steep side surface portion **466**, which extends below the surface of the surrounding filler portion **434** of the encapsulant **430** to prevent internal reflection. A trough **468** is located between the flat surface portion **462** of the lens **460** and the surface of the surrounding filler portion **434** of the encapsulant **430**. Due to refraction, light rays exiting the side surface portion **466** are bent towards the lens **460**, reducing dispersion as compared to the prior art LED of FIG. 1.

Manufacturability considerations may limit the lens embodiment described above. If the lens side surface portion **466** is too steep, the LED may be difficult to release from the encapsulant mold. Further, the depth of the trough **468** may restrict the flow of encapsulant during the molding process and may also interfere with the bond wire **440**. Optical considerations also may constrain this embodiment. The sharp transition **465** between the flat surface portion **462** and side surface portion **466** of the lens **460** results in an abrupt directional change of light rays exiting the lens **460** on either side of this transition **465**, which may be problematic in some applications.

FIG. 5A illustrates an embodiment of a non-protruding lens LED for pulse oximetry applications. Pulse oximetry requires transmission of two wavelengths. Thus, this LED **500** utilizes dual semiconductor diode elements, a "red emitter" **512** producing wavelengths in the red portion of the spectrum and an "IR emitter" **514** producing infrared wavelengths. One type of red emitter is an AlGaAs chip available from, among others, Opto Tech Corporation, Hsinchu Science-Based Industrial Park, Taiwan, R.O.C., part number ED-014-UR/3. This part has a peak emission at 660 ± 3 nm and a radiant power of 1.3 mW minimum. One type of IR emitter is a GaAs chip available from, among others, Infratech Corporation, 10440 Miller Road, Dallas, Tex., part number INF905N13H. This part has a peak emission at 905 ± 10 nm and a radiant power of 1.8 mW typical.

The cathode side of the red emitter **512** is mounted to a first lead **522** and the cathode side of the IR emitter is mounted to a second lead **524**. A third lead **528** is unused. A first bond wire **542** connects the anode side of the red emitter **512** to the second lead **524**. A second bond wire **544** connects the anode side of the IR emitter **514** to the first lead **522**. With this configuration, the red emitter **512** and IR emitter **514** are electrically connected in parallel and "back-to-back," i.e. cathode to anode. In this manner, the red emitter **512** and IR emitter **514** are activated one at a time by alternating the polarity of a voltage applied between the first lead **522** and second lead **524**.

The semiconductor diode elements **512**, **514**, the leads **522**, **524**, **528** and associated bond wires **542**, **544** are all encapsulated after the mounting and bonding process. Encapsulation is accomplished with a transfer mold process as described in detail below. The encapsulant **530** is molded into a standard-sized planar package having a length, L, of 220 mils, a width, W, of 170 mils and a thickness, T, of 70 mils. This forms a light transmitting side **502** and a backside **504** for the LED **500**. One available encapsulant is HYSOL® MG18, which is from The Dexter Corporation, Electronic Materials Division, Industry, Calif. The index of refraction, I_R , for MG18 is 1.52. Thus, the critical angle, θ_c , is $\arcsin(1/1.52) = 41.1^\circ$. Another available encapsulant is NT-300H, which is from Nitto Denko America, Inc., 55 Nicholson Lane, San Jose, Calif. The index of refraction and critical angle for NT-300H is $I_R = 1.564$ and $\theta_c = 39.7^\circ$.

A lens is advantageously formed in the encapsulant during the molding process, as further described below. The light transmitting side **502** of the encapsulant **530** contains a

contoured region **550** and a flat, filler region **570**. The contoured region **550** is a shaped-surface within a circular cross-section 125 mils in diameter. The flat region **570** is a planar surface that surrounds the contoured region **550**. Within the contoured region **550** are a lens **560** and a trough **552** having a sidewall **554**. The lens **560** has a circular cross-section **563**, a flat surface element **564**, and an arcuate surface element **568**. The flat surface element **564** is a substantially flat, circular portion of the lens **560** having a 30-mil diameter in one embodiment. The arcuate surface element **568** is a curved portion of the lens **560** having a 25-mil radius extending from the edge of the flat surface element **564** to the beginning of the trough **552** in one embodiment. The trough **552** has a depth of 22 mils and a bottom width of 4.2 mils in one embodiment. The sidewall **554** is constructed at an angle of 50° with respect to the flat region **570**. With the lens configuration described above, the flat surface element **564** of the lens **560** is in the same plane as the flat region **570** surrounding the lens. This creates a non-protruding lens surface, which avoids pressure necrosis when the emitter with a lens in accordance with the present invention is used is a sensor.

As depicted in FIG. 5B, if the center of an emitter **512** is assumed to be a point source, the maximum distance, B, along the flat surface element before total internal reflection of light occurs is calculated as follows:

A=the distance to the lens surface

=thickness of encapsulant top-half-lead thickness-1/2 emitter thickness=(50-10-4)=36 mil

$B/A = \tan(\pi - \theta_c / 180^\circ) = 0.83$, for $\theta_c = 39.7^\circ$, therefore

$B = 0.83 \cdot 36 \approx 30$ mil

Thus, the entirety of the flat surface element **564**, which has a diameter of 30 mil, is within the critical angle of light rays from either the red emitter **512** or the IR emitter **514**, as illustrated in FIG. 5B and by the calculations above.

The red emitter **512** is advantageously mounted only slightly offset with respect to the center of the lens **560**. Although there is no total internal reflection of light from either emitter **512**, **514** at any portion of the flat surface element **564**, internal reflection increases as the incident angle approaches the critical angle. The red emitter **512** has a lower efficiency as compared to the IR emitter **514**, as apparent from the 1.3 mW versus 1.8 mW radiant power, respectively, for the parts described above. The placement of the red emitter **512** near the lens center minimizes losses from internal reflection in the red spectrum to somewhat compensate for the red emitter's lower efficiency. This placement, however, is somewhat at the expense of the IR emitter **514**, which has a higher efficiency and is, accordingly, mounted near the periphery of the lens **560** due to the space constraints imposed by the red emitter **512** placement and the configuration of the leads **522**, **524** and bond wires **542**, **544**. At its location, the IR emitter **514** may incur significant internal reflection at portions of the lens **560** and uncalculated optical effects due to the proximity of the trough **552** and the trough sidewall **554**.

The embodiment illustrated in FIGS. 5A-B overcomes the limitations of the non-protruding LED lens described with respect to FIG. 4. The trough **552** is shallow enough to allow encapsulant flow and to avoid bond wires. The sidewall **554** is angled to allow easy release of the part from the molding tool. The arcuate portion **568** provides a smooth transition between the flat surface portion **564** and the trough **552** to reduce corner effects.

FIG. 6 illustrates another preferred embodiment of the LED that incorporates a non-protruding spherical lens. As in the embodiment described with respect to FIGS. 5A-B, the light transmitting side 502 of the encapsulant 530 contains a contoured region 550 and a flat, filler region 570. The contoured region 550 and flat region 570 are as described above. Within the contoured region 550 are a lens 660 and a trough 652 having a sidewall 654. The lens 660 has a spherical surface element 664 having a curved surface with a radius of 50 mils. In this configuration, the trough 652 has a depth of 25 mils and a bottom width of 2.7 mils. The sidewall 654 is constructed at an angle of 56° 35' with respect to the flat region 570. With the lens configuration described above, the apex portion of the spherical surface element 664 is in the same plane as the flat region 570 surrounding the lens. As with the lens described with respect to FIGS. 5A-B, this creates a non-protruding lens surface, which avoids pressure necrosis. One of ordinary skill in the art will recognize that other lens shapes are also feasible within the scope of the current invention, such as a lens with a parabolic surface element.

FIG. 7A depicts top, front and side views of the lower cavity portion 710 of a production transfer mold for encapsulating an LED according to the present invention. An available mold has 200 cavities and is manufactured by Neu Dynamics Corp., 110 Steamwhistle Drive, Ivyland, Pa., part number 97-3239. As shown in FIG. 7A, the lower cavity portion 710 has a cavity 720 for each LED to be molded. Placed into this mold are leadframe strips each containing the components for multiple LEDs. Each cavity has portions 722 to accommodate the three leadframe leads allocated to each LED. Each cavity 720 also has a gate 724 through which encapsulant is injected during the molding process, which is described in detail below. A vent 728 allows excess encapsulant and air to be ejected from the cavity. The depth of each cavity 720 is 50 mils, which, with reference to FIG. 5B, corresponds to the thickness, $T_{1/2}$, of the encapsulant upper half.

Each cavity 720 in the lower cavity portion 710 of the mold tool contains an ejector pin 800. When the mold press is opened, these ejector pins 800 protrude into the cavities 720, separating the encapsulated leadframes from the mold tool and allowing removal of the encapsulated leadframes. Within each cavity 720 is an aperture 732 that accommodates the ejector pin tip 1000 as described below. The ejector pin 800 for each cavity is installed in a shaft 734 in the body of the lower cavity portion 710.

FIG. 7B depicts the upper cavity portion 760 of the production transfer mold corresponding to FIG. 7A. As shown in FIG. 7B, the upper cavity portion 760 has a cavity 770 for each LED to be molded. The depth of each cavity 770 is 20 mils, which, with reference to FIG. 5B, corresponds to the thickness, T_1 , of the encapsulant lower half. The production mold, including the lower 710 and upper 760 cavity mold portions are mounted on lower and upper platens, respectively, of a standard production press. An available press is an 83-ton press manufactured by Fujiwa Seiki, model number TEP75-30, available from ESC International, Four Ivybrook Blvd., Ivyland, Pa.

A transfer molding process is utilized to encase the semiconductor diode elements, interconnecting gold bond wire and leadframe within a thermosetting epoxy resin, which is optically transmissive. Further conventional processing results in a completed LED device. Initially, the mold tool is brought to an operating temperature between 140-175° C. The mold tool is brought to an open position. One or more leadframes having multiple leads 522, 524,

528, mounted emitters 512, 514 and bond wires 542, 544 are loaded into a carriage so that the emitters 512, 514 will be face down in the lower mold cavities 720, which form the light emitting side 502 of the encapsulant 530. The lead-frame carriage is then preheated to 325° F. and loaded into the mold tool. The mold press is closed, exerting maximum pressure on the mold tool. Mold compound pellets, which have been preheated for approximately 25 seconds to the consistency of a marshmallow are then loaded into a mold compound pot. A transfer ram injects the molten encapsulant into each cavity gate 724 at a pressure of between 500-1000 psi, and air and excess encapsulant are ejected through each cavity vent 728. The mold cycle time is between 2-5 minutes and nominally 3:00 minutes. After transfer molding, the clear molding resin is cured in an oven at 150° C. $\pm$ 10° C. for 2-4 hours.

FIG. 7C shows a side, cross-section view of the upper cavity portion 760 and the lower cavity portion 710 of the mold tool in the closed position. The upper cavity portion 760 is shown attached to the upper mold tool base 780 with bolts 782. The lower cavity portion 710 is shown attached to the lower mold tool base 740 with bolts 742. In this closed position, each upper cavity 770 and lower cavity 720 together form a whole cavity 790 that accepts and shapes mold compound to form the LED encapsulant. Also shown is a cavity ejector pin 800 that functions as described above for separating an encapsulated leadframe from the mold tool. In addition, there is a runner ejector pin 744 that functions similarly to the cavity ejector pin 800 to separate an encapsulated leadframe from the mold tool. A runner holddown pin 784 serves to position a leadframe within the mold tool.

FIG. 8A illustrates a conventional ejector pin 800. The pin 800 has a base 810, a rod 820 and a tip 830. FIG. 8B illustrates the flat surface at the tip 830 of a prior art ejector pin 800. A pin 801 with a contoured tip 1000 according to the present invention, as described below with respect to FIGS. 10A-B, is installed in the shaft 734 of the lower cavity portion 710 described with reference to FIG. 7A. The rod 820 can freely slide within the shaft 734 such that the tip 1000 is flush with or protrudes into the cavity 720 through the aperture 732. A separate portion of the mold tool presses against the base 810 to actuate the ejector pin 800 when the press is opened or closed. With the prior art ejector pin 800, discontinuities between the pin tip 830 and the surrounding tool and the fact that the pin tip 830 is not exactly flush with the surrounding tool result in imperfections on the surface of the mold compound. This undesirable ejector pin mark typically has to be polished off or placed on a portion of the molded part where the mark has no effect. With respect to molding LED devices, the ejector pin mark can distort the optical properties of the LED encapsulant surface. As a result, in a typical LED molding process, ejector pins are placed on the backside or non-emitting surface of the LED.

FIG. 9 illustrates a mold tool that advantageously utilizes the presence of the ejector pin in each mold cavity to shape the mold compound. This is in stark contrast to the prior art, which attempts to minimize the ejector pin effect. With respect to molding an LED, such as that shown in FIG. 6, the ejector pin 800 is located such that it contacts the light transmitting surface 502 of the LED 600, rather than the backside surface 504. The ejector pin 800 is located within a cavity 720 of the lower cavity portion 710 of the mold tool so that it becomes an integral part of the molding process. As illustrated in FIG. 9, the pin tip 1000 is contoured to form the lens 660, trough 652 and trough sidewall 654 of the LED 600.

The ejector pin **801** according to the present invention functions both to remove the molded parts from the tool and impart a contour to the surface of the LED. As shown in FIG. 9, in the mold tool closed position, the ejector pin **801** provides a shaped surface for molding a lens **660** into the encapsulant **530**. In the mold tool open position, the ejector pin **801** serves the function of separating the encapsulated LED **600** from the mold tool **710** to facilitate removal.

FIG. 10A illustrates an embodiment of a contoured-tip ejector pin according to the present invention. The ejector pin tip **1000** is advantageously shaped to create an LED **500** having a non-protruding lens **560** with a flat surface element **564** corresponding to the illustration of FIG. 5A. The ejector pin tip **1000** of FIG. 10A has an optically ground and polished flat circular surface **1010** of 30 mil diameter which corresponds to the flat surface element **564** of the LED lens **560**. The ejector pin tip **1000** also features a curved portion **1020** of 25 mil radius, R_1 , blending into the flat surface **1010** which is similarly ground into the pin tip **1000** and which corresponds to the arcuate surface element **568** of the LED lens **560**. The pin tip **1000** has a combination of a 50° angle, θ_1 , and a 0.023 inch height, D_1 , taper **1030** ground and optically polished on the outer diameter of the pin tip **1000** which corresponds to the LED encapsulant sidewall **554**. The tip area **1040** between the curved portion **1020** and taper **1030** corresponds to the LED encapsulant trough **552**.

FIG. 10B illustrates another embodiment of a contoured-tip ejector pin according to the present invention. The ejector pin tip **1000A** is advantageously shaped to create an LED **600** having a non-protruding lens **660** with a spherical surface element **664** corresponding to the illustration of FIG. 6. The ejector pin tip **1000A** of FIG. 10B has an optically ground and polished spherical dome **1060** of 50-mil radius, R_2 , which corresponds to the spherical surface element **664**. The tip **1000A** also has a 56° , $35'$ angle, θ_2 , and 0.025 inch height, D_2 , taper **1070** ground and optically polished on the outer diameter of the pin tip **1000A** which corresponds to the encapsulant sidewall **654**. The tip area **1080** between the spherical dome **1060** and taper **1070** corresponds to the encapsulant trough **652**. Neu Dynamics, Ivyland, Pa., is capable of manufacturing ejector pins with contoured tips such as shown in FIGS. 10A-B.

FIG. 10C illustrates yet another embodiment of a contoured-tip ejector pin according to the present invention. The ejector pin tip **1000B** is advantageously shaped to create a generally cone-shaped chamber in the encapsulant to concentrate or "funnel" energy onto the surface of a detector element embedded in the encapsulant. This creates a one-piece detector device that functions similarly to a photodetector mounted within a separate chamber, as described in U.S. Pat. No. 5,638,818 and assigned to the assignee of the present invention. The tip **1000B** features a taper **1090** that is ground and optically polished on the outer diameter of the pin tip **1000B** and that corresponds to the chamber walls.

The non-protruding optoelectronic lens and associated contoured-tip ejector pins have been disclosed in detail in connection with the various embodiments of the present invention. These embodiments are disclosed by way of examples only and are not to limit the scope of the present invention, which is defined by the claims that follow. One of ordinary skill in the art will appreciate many variations and modifications within the scope of this invention. For example, although the current invention was described above mostly with respect to LED embodiments, the current invention also applies to non-protruding lenses for encapsulated photodiode detectors and to detector cavities.

What is claimed is:

1. A mold tool for an optoelectronic device comprising:
 - a first mold piece having a surface that defines a first cavity and that defines an aperture within said first cavity;
 - a second mold piece having a surface which defines a second cavity, said first cavity cooperating with said second cavity to at least partially form a molding compound into a predetermined shape; and
 - an ejector pin movably located within said aperture to facilitate removal of said compound from said first cavity, wherein said predetermined shape comprising a generally flat surface and a generally contoured surface at least partially within and not extending above said flat surface, said contoured surface including a lens surrounded by a trough, at least a portion of said trough including a sidewall opposite said lens, said predetermined shape embedding at least one optoelectronic element.
2. The mold tool of claim 1, wherein said ejector pin includes a contoured tip movably located within said aperture to form an integral portion of said first cavity, wherein said predetermined shape is at least partially defined by said contoured tip.
3. The mold tool of claim 2, wherein said contoured tip forms a surface configured to shape said compound into said lens.
4. The mold tool of claim 2, wherein said contoured tip forms a surface configured to shape said compound into said trough.
5. The mold tool of claim 2, wherein said contoured tip forms a surface configured to shape said compound into said trough sidewall.
6. The mold tool of claim 1, wherein said lens comprises a generally flat circular surface ending with an arcuate surface at its periphery.
7. The mold tool of claim 1, wherein said lens comprises a generally spherical surface.
8. The mold tool of claim 1, wherein said lens comprises a generally parabolic surface.
9. A mold for an optoelectronic device comprising:
 - a first mold section defining a first cavity; and
 - a second mold section defining a second cavity, wherein the first and second mold sections cooperate to form an encapsulant into a desired shape embedding a plurality of leads and at least one optoelectronic device comprising one of an emitter or a detector of a noninvasive optical oximetry sensor, the shape of the encapsulate including a generally flat surface and a generally contoured surface at least partially within and not extending above said flat surface, said contoured surface including a lens surrounded by a trough, at least a portion of said trough including a sidewall opposite said lens.
10. The mold of claim 9, wherein said at least one optoelectronic device comprises a plurality of emitters.
11. The mold of claim 10, wherein said emitters comprises first and second emitters.
12. The mold of claim 11, wherein said first emitter includes a first efficiency, said second emitter includes a second efficiency higher than said first efficiency, and wherein said first emitter is more centered under said lens than said second emitter.
13. The mold of claim 9, wherein said first mold section comprises an ejector pin including a contoured tip forming an integral portion of said first cavity, wherein said shape is at least partially defined by said contoured tip.

11

14. The mold of claim 13, wherein said contoured tip forms a surface of said first cavity configured to shape said encapsulant into said lens.

15. The mold of claim 13, wherein said contoured tip forms a surface of said first cavity configured to shape said 5 encapsulant into said trough.

16. The mold of claim 13, wherein said contoured tip forms a surface of said first cavity configured to shape said encapsulant into said trough sidewall.

12

17. The mold of claim 9, wherein said lens comprises a generally flat circular surface ending with an arcuate surface at its periphery.

18. The mold of claim 9, wherein said lens comprises a generally spherical surface.

19. The mold of claim 9, wherein said lens comprises a generally parabolic surface.

* * * * *

专利名称(译)	提供具有非突出透镜的光电元件的方法		
公开(公告)号	US7332784	公开(公告)日	2008-02-19
申请号	US11/475725	申请日	2006-06-27
[标]申请(专利权)人(译)	梅西莫股份有限公司		
申请(专利权)人(译)	Masimo公司		
当前申请(专利权)人(译)	Masimo公司		
[标]发明人	MILLS MICHAEL A COFFIN IV JAMES P		
发明人	MILLS, MICHAEL A. COFFIN, IV, JAMES P.		
IPC分类号	H01L31/0203 H01L31/0232 A61B5/00 H01L25/075 H01L33/54		
CPC分类号	B29C45/401 H01L31/0203 H01L31/0232 H01L33/54 A61B5/1455 B29C45/14655 H01L24/45 H01L25/0753 H01L2224/45144 H01L2224/48091 H01L2924/01077 H01L2924/01079 H01L2924/00014 H01L2924/12041 Y10S425/808 H01L2224/48247 H01L2924/1815 H01L31/02327 H01L2924/12042 H01L2924/12043 H01L2924/181 H01L2924/00 H01L2924/00012		
其他公开文献	US20070007612A1		
外部链接	Espacenet USPTO		

摘要(译)

光电子器件具有透镜，该透镜形成在围绕半导体二极管元件的密封剂的表面中。对于发射器，透镜减少了内部反射并减少了色散，从而提高了整体效率。关于探测器，透镜将光子聚焦在探测器的有效区域上，增加探测器灵敏度，这允许探测器具有减小的尺寸并降低给定应用的成本。密封剂的透镜部分通常不从密封剂的周围部分突出，从而减小由光电子器件引起的接触表面压力。这种非突出的镜片在脉搏血氧饱和度传感器应用中特别有用。有利地，透镜形成有结合到密封剂转移模具中的成型尖端顶出销，并且透镜形状有助于脱模。

