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(54) **APPARATUS AND METHOD FOR FREQUENCY-DOMAIN OPTICAL COHERENCE TOMOGRAPHY**

VORRICHTUNG UND VERFAHREN FÜR OPTISCHE FREQUENZBEREICHS-
KOHÄRENZTOMOGRAPHIE

APPAREIL ET PROCEDE DE TOMOGRAPHIE A COHERENCE OPTIQUE

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Description

BACKGROUND OF THE INVENTION

5 Field of the Invention

[0001] The present invention relates generally to apparatuses and methods for optical coherence tomography, and more specifically to apparatuses and methods for providing improved optical coherence tomography images.

10 DESCRIPTION OF THE RELATED ART

[0002] Optical coherence tomography (OCT) is widely used in medicine to image tissues of various part of the body. See, e.g., T. Asakura, "International trends in optics and photonics ICO IV," (Springer-Verlag, Berlin Heidelberg, 1999) pp. 359-389; D. Huang, et al. "Optical coherence tomography," Science, Vol. 254, pp. 1178-1181 (1991); J.G. Fujimoto, et al. "Optical biopsy and imaging using optical coherence tomography," Nature Medicine, Vol. 1, pp. 970-972 (1995); A.F. Fercher, C.K. Hitzenberger, G.Kamp, and S.Y. El-Zaiat, "Measurement of intraocular distances by backscattering spectral interferometry," Opt. Commun., Vol. 117, pp. 43-48 (1995); G. Hausler and M.W. Lindler, "Coherence radar and spectral radar- New tools for dermatological diagnosis," J. Biomed. Opt., Vol. 3, pp. 21-31 (1998); M. Wojtkowski, R.A. Leitgeb, A. Kowalczyk, T. Bajraszewski, and A.F. Fercher, "In vivo human retinal imaging by Fourier domain optical coherence tomography," J. Biomed. Opt., Vol. 7, pp. 457-463 (2003); R.A. Leitgeb, C.K. Hitzenberger, and A.F. Fercher, "Performance of Fourier domain vs. time domain optical coherence tomography," Optics Express, Vol. 11, pp. 889-894 (2003); M.A. Choma, M.V. Sarunic, C. Yang, and J.A. Izatt, "Sensitivity advantage of swept source and Fourier domain optical coherence tomography," Optics Express, Vol. 11, pp. 2183-2189 (2003); R.A. Leitgeb, C.K. Hitzenberger, A.F. Fercher, and T. Bajraszewski, "Phase-shifting algorithm to achieve high-speed long-depth-range probing by frequency domain optical coherence tomography," Opt. Lett., Vol. 28, pp. 2201-2203 (2003); R. A. Leitgeb et al. "Ultrahigh resolution Fourier domain optical coherence tomography," Optics Express, Vol. 12, pp. 2156-2165 (2004).

[0003] Figures 1A and 1B schematically illustrate two OCT configuration for use with the two major techniques of OCT, time-domain OCT and frequency-domain OCT, respectively, In both time-domain OCT and frequency-domain OCT, a broadband light source 10, such as a superluminescent diode, a mode-locked laser, or even a supercontinuum generating fiber, feeds an interferometer 20, typically a Michelson interferometer. A reference broadband mirror 30 is placed on one arm of the interferometer 20, and the tissue 40 is on the other arm of the interferometer. In the OCT configurations of Figures 1A and 1B, the light source is split into two fields using a beam splitter 50 or a fiber coupler (FC), and each field is directed towards one arm of the interferometer 20. The reflected light from the tissue 40 and from the reference mirror 30 are combined collinearly at the detector 60. The basic difference between time-domain OCT and frequency-domain OCT is that in time-domain OCT, the reference mirror 30 is a movable mirror, which is scanned as a function of time during the image acquisition. However, in the frequency-domain OCT, there are no moving parts, and at the detector end, the spectrum of the interference between the two reflected signals coming from each arm of the interferometer is recorded by means of an optical spectrum analyzer (OSA), e.g., a charged-coupled-device (CCD) array with the appropriate imaging optics. There are significant advantages of frequency-domain OCT over time-domain OCT, such as higher speed and higher sensitivity.

US2004/0239943 describes how a quadrature broadband interferometry system and method obtains a complete complex interferometric signal instantaneously in both homodyne and heterodyne systems in a simple, compact and inexpensive setup. Ozcan et al, "Iterative processing of second-order optical non-linearity depth profiles" Optics Express, vol.12, no. 15, 26 July 2001 pp3387-3376 and Ozcan et al, "Group delay recovery using iterative processing of amplitude of transmission spectra of fibre Bragg gratings". Electronics Letters, IEE Stevenage GB, vol.40, no.18, 2 September 2004, pp1104-1106 are also of interest as general background art but fail to teach or suggest the present invention

[0004] According to one aspect of the present invention there is provided a method based on minimum-phase functions for determining an estimated intermediate function which differs from a complex scattering function of a portion of a sample under analysis by the product of a spatial Dirac-delta function and a field reflectivity of a reference reflective element, whereby the intermediate function is close to a minimum-phase function, if not an exact minimum-phase function, the method comprising: (a) providing a magnitude spectrum of a complex spatial Fourier transform of a complex intermediate function, the complex intermediate function dependent on the complex scattering function of the portion of the sample under analysis, the magnitude spectrum obtained from power spectrum data of frequency-domain optical coherence tomography of the portion of the sample under analysis; (b) providing an estimated phase term of the complex spatial Fourier transform; (c) multiplying the magnitude spectrum and the estimated phase term together to generate an estimated complex spatial Fourier transform; (d) calculating an inverse Fourier transform of the estimated complex spatial Fourier transform, wherein the inverse Fourier transform of the estimated complex spatial Fourier transform is a spatial function; and (e) calculating the estimated intermediate function by applying at least one constraint to the inverse Fourier

transform of the estimated complex spatial Fourier transform.

[0005] According to another aspect of the present invention there is provided a computer system for performing the above method, comprising: means for obtaining a magnitude spectrum of a complex spatial Fourier transform of a complex intermediate function, the complex intermediate function differs from a complex scattering function of a portion of a sample under analysis by the product of a spatial Dirac-delta function and a field reflectivity of a reference reflective element, the magnitude spectrum obtained from power spectrum data of frequency-domain optical coherence tomography of the portion of the sample under analysis; means for estimating an estimated phase term of the complex spatial Fourier transform; means for multiplying the magnitude spectrum and the estimated phase term together to generate an estimated complex spatial Fourier transform; means for calculating an inverse Fourier transform of the estimated complex spatial Fourier transform, wherein the inverse Fourier transform of the estimated complex spatial Fourier transform is a spatial function; and means for calculating the estimated intermediate function by applying at least one constraint to the inverse Fourier transform of the estimated complex spatial Fourier transform.

[0006] Examples of an apparatus to measure a frequency-domain optical coherence tomography power spectrum from a sample are disclosed. The apparatus comprises a broadband light source. The apparatus further comprises an optical spectrum analyzer. The apparatus further comprises a partially reflective element optically coupled to the light source, to the optical spectrum analyzer, and to the sample. A first portion of light from the light source is reflected by the partially reflective element and propagates to the optical spectrum analyzer. A second portion of light from the light source propagates through the partially reflective element, impinges the sample, reflects from the sample, and propagates to the optical spectrum analyzer.

BRIEF DESCRIPTION OF THE DRAWINGS

[0007] Figures 1A and 1B schematically illustrate two OCT configurations for use with the two major techniques of OCT, time-domain OCT and frequency-domain OCT, respectively.

[0008] Figure 2 is a flow diagram of an example iterative error-reduction method for determining the complex scattering function $f(z)$ of a sample in accordance with certain embodiments described herein.

[0009] Figures 3A and 3B are graphs of the magnitude and phase, respectively, of an example simulated complex tissue scattering function (solid lines) and a recovered complex tissue scattering function (dashed lines).

[0010] Figure 4 is a graph of the computed power spectrum, *i.e.*, the square of the Fourier transform magnitude of the simulated tissue scattering function of Figures 3A and 3B.

[0011] Figures 5A and 5B show the magnitude and phase, respectively, of the simulated tissue scattering function (solid lines) and the recovered tissue scattering function (dashed lines) for another example simulation in which z_0 equals about 1.2 millimeters.

[0012] Figure 6 is a graph of the computed power spectrum of the simulated complex tissue scattering function of Figures 5A and 5B.

[0013] Figures 7A and 7B show the magnitude and phase, respectively, of an example simulated tissue scattering function (solid line) and a recovered tissue scattering function (dashed line) for a ratio of $R_{\max}\{|f(z')|\}$ approximately equal to 5.

[0014] Figure 8 is a graph of an example simulated power spectrum with an added 30% peak-to-peak amplitude uniform random noise.

[0015] Figures 9A and 9B are graphs of the magnitude and phase, respectively, of the simulated tissue scattering function (solid lines) corresponding to the simulated power spectrum of Figure 8 and the recovered tissue scattering function (dashed lines).

[0016] Figure 10 schematically illustrates an example frequency-domain OCT configuration.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

[0017] In the embodiments described herein, the concept of minimum-phase functions is applied to improve optical coherence tomography systems. The embodiments described herein advantageously provide a simple processing technique for the conventional frequency-domain OCT configuration that enables a better signal-to-noise ratio, an improved measurement range, and that requires a lower-resolution optical spectrum analyzer than the currently existing processing techniques. The embodiments described herein rely on the property of minimum-phase functions (MPFs) to advantageously allow a function, complex or real, to be recovered from only its Fourier transform (FT) magnitude data.

[0018] Certain embodiments described herein are useful in computer-implemented analyses of the complex field scattering function of frequency-domain OCT. The general-purpose computers used for such analyses can take a wide variety of forms, including network servers, workstations, personal computers, mainframe computers and the like. The code which configures the computer to perform such analyses is typically provided to the user on a computer-readable medium, such as a CD-ROM. The code may also be downloaded by a user from a network server which is part of a

local-area network (LAN) or a wide-area network (WAN), such as the internet.

[0019] The general-purpose computer running the software will typically include one or more input devices, such as a mouse, trackball, touchpad, and/or keyboard, a display and computer-readable memory media, such as random-access memory (RAM) integrated circuits and a hard-disk drive. It will be appreciated that one or more portions, or all of the code may be remote from the user and, for example, resident on a network resource, such as a LAN server, Internet server, network storage device, etc. In typical embodiments, the software receives as an input a variety of information concerning the material (e.g., structural information, dimensions, previously-measured magnitudes of reflection or transmission spectra).

[0020] In typical OCT configurations, such as those shown in Figures 1A and 1B, the effective complex scattering function, which includes in its definition both the tissue 40 and the reference mirror 30, either is a minimum-phase function (MPF) or is close to being one. In certain examples described herein, this property allows the effective complex scattering function to be recovered by means of either the analytical Hilbert transformation or the iterative processing of the measured power spectrum data.

[0021] In the frequency-domain OCT configuration schematically illustrated by Figure 1B, the complex field scattering function (sometimes also called the scattering potential) of the tissue of interest is $f(z)$, where z is simply the depth into the tissue, with $z \geq 0$ defining the tissue. The spectral intensity distribution of the broadband source is $S(k)$, where $k = 2\pi/\lambda$ and λ is the wavelength of light. In the following description, the notation is close to that given by G. Hausler and M.W. Lindler, "Coherence radar and spectral radar- New tools for dermatological diagnosis," J. Biomed. Opt., Vol. 3, pp. 21-31 (1998). The power spectrum detected at the optical spectrum analyzer (OSA) of Figure 1B can be written as:

$$I(k') = S(k') \cdot \left| \int_{-\infty}^{\infty} g(z') \cdot \exp(jk'2n_T z') \cdot dz \right|^2 \quad (1)$$

where $g(z') = R \cdot \delta(z') + f(z'-z_0)$ and is referred to herein as the intermediate function or the effective scattering function of the system, $\delta(z')$ is the spatial Dirac-delta function, $k' = k - 2\pi/\lambda_0$, λ_0 is the center frequency of $S(k)$, R is the field reflectivity of the reference mirror, z_0 is the offset distance between the reference arm and the tissue arm, as shown in Figure 1B, and n_T is the refractive index of the tissue, where the dispersion of the tissue has been assumed to be negligible and is ignored, i.e., $n_T(k) \approx n_T$. This last assumption is quite safe and has also been used in other treatments of OCT. If one defines the spatial Fourier transform (FT) frequency as $f = k' \cdot n_T / \pi$, then the expression in Eq. (1) takes the form of a Fourier transform:

$$I(f) = S(f) \cdot |G(f)|^2 \quad (2)$$

where $G(f)$ is the spatial FT of $g(z') = R \cdot \delta(z') + f(z'-z_0)$. If $S(f)$ is broad and smooth enough to determine the resolution of the OCT system, then $I(f) \approx s \cdot |G(f)|^2$, where s is simply a proportionality constant.

[0022] The conventional processing techniques of frequency-domain OCT measurements are based on a processing algorithm which directly takes the inverse FT of Eq. (2). Certain embodiments described herein are compared to the conventional processing techniques by assuming that $S(f)$ is broad enough to present a simple and fair comparison by assuming that, without loss of generality, the constant s has been dropped, i.e., $I(f) \approx |G(f)|^2$. This assumption will also be made for the conventional processing techniques, so it has no effect on the discussion herein and the effect of $S(f)$ on the resolution of the OCT system is not relevant to certain embodiments described herein.

[0023] In the conventional processing techniques, taking the inverse Fourier transform (IFT) of the measured OSA spectrum ($I(f) \approx |G(f)|^2$) directly yields:

$$IFT\{G(f)^2\} = |R|^2 \cdot \delta(z') + A.C.\{f(z')\} + R \cdot f^*(-z - z_0) + R^* \cdot f(z - z_0) \quad (3)$$

where A.C. denotes the complex auto-correlation function, and ** denotes the complex conjugate operation. The important term for the recovery of the tissue scattering function is the last term of Eq. (3), i.e., $R^* \cdot f(z - z_0)$. However, the A.C. $\{f(z')\}$ term in Eq. (3) is centered around $z = 0$ and usually obscures $R^* \cdot f(z - z_0)$ by spatial aliasing, thereby degrading the sensitivity and the signal-to-noise ratio of the frequency-domain OCT measurements. In the conventional processing techniques, z_0 is chosen to be large enough such that $R^* \cdot f(z - z_0)$ is shifted in space away from the origin, thereby reducing spatial aliasing with the A.C. $\{f(z')\}$ term. For example, for a broadband source with a coherence length of about

40 micrometers, a value of $z_0 > 200$ micrometers would be sufficient to significantly avoid the spatial overlap. By filtering the $R^* \cdot f(z-z_0)$ term around $z = z_0$, the complex scattering potential of the tissue of interest, $f(z)$, is recovered. However, choosing z_0 to be large enough to avoid spatial aliasing introduces other problems. For example, large values of z_0 cause the fringes observed in the OSA spectrum to get closer to one another, which can become a significant problem, especially for a low-resolution OSA. Furthermore, in general, a large value of z_0 reduces the accessible depth information in the tissue for a given OSA in the OCT configuration.

[0024] The embodiments described herein utilize a simple processing technique that is based on minimum-phase functions (MPFs) to improve the resolution, the signal-to-noise ratio, and the measurement range of the recovered images in frequency-domain OCT systems. The intermediate function $g(z') = R \cdot \delta(z') + f(z'-z_0)$ in an OCT system is close to an MPF, if not an exact MPF.

[0025] For the intermediate function $g(z') = R \cdot \delta(z') + f(z'-z_0)$, relevant to the power spectrum measurement of OCT, tissue typically has $n_T \approx 1.5$, so $\max\{|f(z')|\} \ll 1$ (where $\max\{|f(z')|\}$ is the maximum magnitude of the tissue scattering function), whereas R is approximately equal to 1. Therefore in such configurations, the intermediate function $g(z') = R \cdot \delta(z') + f(z'-z_0)$ has a dominant peak at the origin, so $g(z')$ either is close to an MPF or is an exact MPF. In certain embodiments, this property of the intermediate function $g(z')$ is used to uniquely recover the tissue scattering function $f(z)$ from only the knowledge of $|G(f)|$, regardless of the value of z_0 . In certain embodiments in which the condition of $\max\{|f(z')|\} \ll 1$ is not satisfied, more power can be directed to the reference arm to make R larger, and hence to have a dominant peak at the origin for $g(z') = R \cdot \delta(z') + f(z'-z_0)$.

[0026] It is generally not possible to fully recover a one-dimensional function from the knowledge of its FT magnitude alone. However, there are families of functions which are exceptions to this rule for which the FT phase can be recovered from the FT magnitude alone, and visa versa. One exemplary such family is the family of minimum-phase functions (MPFs). An MPF is characterized by having a z -transform with all its poles and zeros either on or inside the unit circle. As a result of this property, the FT phase and the logarithm of the FT magnitude of an MPF are Hilbert transforms of one another. See, e.g. V. Oppenheim and R.W. Schaffer, "Digital Signal Processing," (Prentice Hall, 2002), Chap. 7; T.F. Quatieri, Jr., and A.V. Oppenheim, "Iterative techniques for minimum phase signal reconstruction from phase or magnitude," IEEE Trans. Acoust. Speech, Signal Processing, Vol 29, pp. 1187-1193 (1981); M. Hayes, J.S. Lim, and A.V. Oppenheim, "Signal reconstruction from phase or magnitude," IEEE Trans. Acoust. Speech, Signal Processing, Vol. 28, pp. 672-680 (1980). Consequently, an MPF can be calculated from only its FT amplitude.

[0027] As an example, this recovery of the function of interest (e.g., the intermediate function $g(z') = R \cdot \delta(z') + f(z'-z_0)$) can be obtained from only its FT amplitude (e.g., $|G(f)|$) by first taking the Hilbert transform of the logarithm of the function's FT magnitude (e.g., the logarithmic Hilbert transform of the function's FT magnitude) to obtain the FT phase, and then inverting the full complex FT. However, this direct approach is not the preferred solution because of difficulties in its numerical implementation, in particular phase unwrapping. In certain embodiments, an iterative error-reduction technique is used, as described more fully below.

[0028] A second approach for the recovery of the function of interest (e.g., the intermediate function $g(z') = R \cdot \delta(z') + f(z'-z_0)$) is to use an iterative error-reduction method. Examples of iterative error-reduction methods include, but are not limited to, those described by J.R. Fienup, "Reconstruction of an object from the modulus of its Fourier transform," Opt. Lett., Vol. 3, pp. 27-29 (1978) or R.W. Gerchberg and W.O. Saxton, "Practical algorithm for the determination of phase from image and diffraction plane pictures," Optik, Vol. 35, pp. 237-246 (1972).

[0029] Figure 2 is a flow diagram of an exemplary iterative error-reduction method 100 for determining the complex tissue scattering function $f(z)$ of a portion of a sample under analysis in accordance with certain embodiments described herein. This iterative error-reduction method 100 involves using a known (e.g., measured) magnitude spectrum $|G(f)|$ of a complex spatial Fourier transform of a complex intermediate function $g(z')$, together with known properties of this function (e.g., that it is a real function or a causal function), to correct an initial guess of the intermediate function $g(z')$. In certain embodiments, this correction is done iteratively. In certain embodiments, the intermediate function $g(z')$ is dependent on the complex tissue scattering function $f(z)$ of the sample, as described more fully below.

[0030] In the embodiments, the only quantity that is fed into the method 100 is the magnitude spectrum $|G_M(f)|$ of the complex spatial FT of the complex intermediate function $g(z')$, where the subscript M denotes that this magnitude spectrum is a measured quantity, as shown by the operational block 110. In certain embodiments, providing the magnitude spectrum $|G_M(f)|$ corresponding to the intermediate function $g(z')$ comprises measuring a frequency-domain OCT power spectrum from the portion of the sample under analysis and calculating the square-root of the measured frequency-domain OCT power spectrum to yield the measured FT magnitude spectrum $|G_M(f)|$. In certain other embodiments, providing the magnitude spectrum $|G_M(f)|$ comprises providing a previously-measured frequency-domain OCT power spectrum and calculating the square-root of the previously-measured frequency-domain OCT power spectrum or providing the square-root of a previously-measured frequency-domain OCT power spectrum.

[0031] Since the FT phase term is missing from the measurement, an initial guess for the phase, $\phi_0(f)$, is used to provide an estimated phase term $\exp(j\phi_0)$ in the operational block 120. In certain embodiments, this initial guess does not significantly affect the accuracy of the result of the convergence of the method 100. For this reason, the initial guess

for the phase $\phi_0(f)$ can be conveniently chosen to equal zero (e.g., $\phi_0(f)=0$) or some other real or complex constant (e.g., π , $\pi/2$). In certain embodiments, the initial guess for the phase can be a previously-stored function $\phi_0(f)$ retrieved from the computer system. In certain embodiments, the initial guess for the phase can be a phase obtained from a different portion of the sample. For example, in tissue imaging, the initial guess for the phase $\phi_0(f)$ can be a phase resulting from a portion of the tissue adjacent to the portion of the surface under analysis. Thus, in a real imaging situation, the initial guess for the phase $\phi_0(f)$ can be dynamically assigned to be the new phase resulting from a previous measurement. In certain embodiments, the initial guess for the phase can be calculated from the measured magnitude spectrum $|G_M(f)|$ using a logarithmic Hilbert transform.

[0032] In the embodiments, the magnitude spectrum and the estimated phase term are multiplied together to generate an estimated complex spatial Fourier transform $|G_M| \cdot \exp(j\phi_0)$. The inverse Fourier transform (IFT) of $|G_M| \cdot \exp(j\phi_0)$ is then computed numerically, as shown by the operational block 130, to calculate an inverse Fourier transform $g'(z)$ of the estimated complex spatial Fourier transform, wherein the inverse Fourier transform $g'(z)$ is a spatial function. In certain embodiments, the operational block 140 comprises applying at least one constraint to the inverse Fourier transform $g'(z)$ to calculate an estimated intermediate function $g_1(z)$. In certain embodiments in which the sample has a known spatial extent, applying the at least one constraint comprises setting the IFT to zero for regions outside the known spatial extent of the sample. For example, since $g'(z)$ approximates a minimum-phase function (MPF) and since MPFs are causal, only the $z \geq 0$ portion of $g'(z)$ is retained (e.g., the causality condition), and all values of $g'(z)$ for $z < 0$ are set to zero, thereby producing a new function $g_1(z)$.

[0033] In certain embodiments in which the intermediate function $g(z)$ has a known spatial extent (e.g., to be less than 1 millimeter deep), the operational block 140 can also include setting the inverse Fourier transform $g'(z)$ to zero for regions outside the known spatial extent of the intermediate function $g(z)$ by inserting zeros for z greater than this limit (e.g., $z > 1$ millimeter) to produce the function $g_1(z)$, thereby advantageously speeding up convergence of the error-reduction method. In certain embodiments, the new function $g_1(z)$ provided by the operational block 140 serves as a first estimate of the complex MPF (i.e., the estimated intermediate function $g(z)$).

[0034] In certain embodiments, the FT of the estimated intermediate function $g_1(z)$ is calculated in the operational block 150, thereby providing a new calculated phase $\phi_1(f)$ (hence a new calculated phase term $\exp(j\phi_n)$) and a new magnitude spectrum $|G_1(f)|$ for the FT of the estimated intermediate function $g_1(z)$. In certain embodiments, the calculated FT magnitude spectrum $|G_1(f)|$ is replaced by the measured magnitude spectrum $|G_M(f)|$, as shown by the arrow 160. In certain embodiments, the loop is then repeated using the measured magnitude spectrum $|G_M(f)|$ and the calculated phase term $\exp(j\phi_1)$ as the new input function in the operational block 130, which provides a second function $g_2(z)$. In certain embodiments, only a single iteration is used, while in other embodiments, this loop is repeated until convergence is achieved. In certain embodiments, convergence is defined to be achieved when the difference between consecutive estimates of the function $\int |g_n(z) - g_{n-1}(z)|^2 dz / \int |g_n(z)|^2 dz$ is less than a predetermined value, for example 0.1%. In certain embodiments, less than 100 iterations are adequate for achieving convergence, taking less than a second to compute using a rather slow programming environment such as MATLAB 5 on a 500 MHz computer with 2^9 data points. In certain embodiments, applying the constraint in the operational block 140 advantageously reduces the number of iterations which achieve convergence.

[0035] In certain other embodiments, the loop is repeated a predetermined number of times (e.g., 100). In certain embodiments, the predetermined number of times is selected to be sufficiently large so that the method achieves, or is close to achieving, convergence. In certain embodiments, at the end of the n -th iteration, $g_n(z)$ is the recovered complex MPF.

[0036] In certain other embodiments, the iterations of the loop are stopped when the user (e.g., the doctor reviewing the OCT images) determines that the image quality is sufficient.

[0037] Empirical results indicate that such iterative error-reduction methods converge to the minimum-phase function corresponding to a given FT magnitude. (See, e.g., T.F. Quatieri, Jr., and A.V. Oppenheim, "Iterative techniques for minimum phase signal reconstruction from phase or magnitude," IEEE Trans. Acoust., Speech, Signal Processing, Vol. 29, pp. 1187-1193 (1981); A. Ozcan et al., "Iterative processing of second-order optical nonlinearity depth profiles," Opt. Express, Vol. 12, pp. 3367-3376 (2004); A. Ozcan et al., "Group delay recovery using iterative processing of amplitude of transmission spectra of fibre Bragg gratings," Electron. Lett., Vol. 40, pp. 1104-1106 (2004).) In other words, for the infinite family of FT phase functions that can be associated with a known (e.g., measured) FT magnitude, certain embodiments described herein converge to the one and only one FT phase function that has the minimum phase. Since this solution is unique, if it is known *a priori* that the function to be reconstructed is an MPF (or that the function approximates an MPF), then the solution provided by the error-reduction method is the correct function.

[0038] To understand intuitively which physical functions such as $g(z')$ are likely to be minimum-phase functions, $g_{min}(n)$ is used to denote an MPF, where n is an integer that numbers sampled values of the function variable (e.g., space z' for the tissue scattering potential $g(z')$). Because all physical MPFs are causal, $g_{min}(n)$ must be equal to zero for $n < 0$. As discussed by V. Oppenheim and R.W. Schaffer in "Digital Signal Processing," (Prentice Hall, 2002), Chap. 7, the

energy of a minimum-phase function, which is defined as $\sum_{n=0}^{m-1} |g_{min}(n)|^2$ for m samples of the function, satisfies the following inequality: $n=0$

$$\sum_{n=0}^{m-1} |g_{min}(n)|^2 \geq \sum_{n=0}^{m-1} |g(n)|^2 \quad (4)$$

for all possible values of $m > 0$. In Eq. (4), $g(n)$ represents any of the functions that have the same FT magnitude as $g_{min}(n)$. This property suggests that most of the energy of $g_{min}(n)$ is concentrated around $n = 0$. Stated differently, any function, complex or real, with a dominant peak around $n = 0$ (i.e., close to the origin) will be either a minimum-phase function or close to one, and thus the function will work extremely well with iterative error-reduction methods in accordance with certain embodiments described herein. Although there may be other types of MPFs besides functions with a dominant peak, this class of MPFs can be used as described herein because they are straightforward to construct with OCT data and because they yield exceedingly good results. See, also, A. Ozcan, M.J.F. Digonnet, and G.S. Kino, "Iterative processing of second-order optical nonlinearity depth profiles," Opt. Express, Vol. 12, pp. 3367-3376 (2004).

[0039] Recovering $f(z)$ from only the knowledge of $|G(f)|$ using error-reduction methods compatible with certain embodiments described herein advantageously provides significant advantages in frequency-domain OCT over the conventional processing approaches. In certain embodiments, the error-reduction method does not utilize a minimum constraint for z_0 , so z_0 can conveniently be chosen close to zero. Such embodiments provide a significant improvement on the resolution requirement of the OSA of the OCT system. Furthermore, since the depth measurement range into the tissue is inversely proportional to the maximum spatial frequency measured in the OSA spectrum, in principle, a value of z_0 close to zero allows a larger measurement range for the OCT configuration. In certain embodiments, the error-

reduction method deals with the square-root of the measured power spectrum $\sqrt{I(k')}$, whereas the conventional approaches take a direct IFT of $I(k')$ - In terms of noise sensitivity, in certain such embodiments, the error-reduction method performs much better than the conventional approach, since the noise term in $I(k')$ is much stronger than in $\sqrt{I(k')}$.

For example, by adding some random noise to $\sqrt{I(k')}$, i.e., $\sqrt{I(k')} + noise$, the added noise term becomes stronger, i.e., $\sqrt{I(k')}$. In certain embodiments, the error-reduction method advantageously avoids the degradation in the signal-to-noise ratio in the classical processing techniques associated with the spatial aliasing due to the A.C. $\{f(z)\}$ term in Eq (3), thereby yielding a better performance.

[0040] In an example numerical simulation, to simulate a rather challenging problem, the complex tissue scattering function is simulated to be a uniform random variable, both in magnitude and phase, as shown by solid lines in Figures 3A and 3B, respectively. In this example numerical simulation, it is assumed that $z_0 = 0$, which means that the length of the upper arm is roughly matched to the length of the lower arm of the Michelson interferometer in the OCT configuration schematically illustrated by Figure 1B. The field reflectivity of the tissue is allowed to vary in magnitude between 0.01 and 0.04. These numbers are not critical, and could as well be chosen to be rather different. For the same example simulation, the mirror reflectivity R used in the OCT configuration was chosen to be equal to 1, which is the source of the sharp peak observed in the scattering function shown in Figure 3A. The whole cross-section of the tissue is assumed to be about 0.25 millimeter, and this value could as well be chosen larger or smaller without any change in the results.

[0041] Figure 4 is a graph of the computed power spectrum, i.e., the square of the FT magnitude of the simulated scattering function shown in Figures 3A and 3B. For this computation, a resolution of about 0.5 nanometer was assumed for the OSA, and a center wavelength of 840 nanometers was assumed for the broadband source. The whole trace shown in Figure 4 has only 512 data points. Feeding the square-root of the power spectrum shown in Figure 4 to the iterative error-reduction method 100 shown by Figure 2 yields a recovered complex tissue scattering function as shown by the dashed lines in Figures 3A and 3B. The recovery for both the magnitude and the phase of the tissue scattering function is so good that the recovered curves cannot be distinguished from the originally simulated curves, as shown in Figures 3A and 3B. The calculation of the recovered curves took less than a second using MATLAB 5 on a 500-MHz computer, which suggests that by using a faster programming environment such as C++, together with a faster processor, sub-millisecond computation times can be achieved.

[0042] The solid lines of Figures 5A and 5B show the magnitude and phase, respectively, of the tissue scattering function for another example numerical simulation in which z_0 equals about 0.12 millimeter. The other parameters of

this simulation were assumed to be the same as in the example of Figures 3A, 3B, and 4. Figure 6 is a graph of the computed power spectrum of the simulated complex tissue scattering function of Figures 5A and 5B. Due to $z_0 \approx 0.12$ millimeter, the frequency of fringes in the power spectrum gets more rapid, as shown by a comparison of Figures 4 and 6. Feeding the square-root of the power spectrum of Figure 6 to the iterative error-reduction method 100 of Figure 2 yields a recovered complex tissue scattering function as shown by the dashed lines of Figures 5A and 5B. The recovery is again excellent, with the recovered complex tissue scattering function between about 0.12 and about 0.25 millimeter nearly indistinguishable from the simulated complex tissue scattering function. In the gap region, e.g., between 0 and 0.12 millimeter, the recovered phase of the tissue scattering function can simply be ignored since the magnitude of the function in that interval is zero, making the definition of a definite phase meaningless in the gap region.

[0043] The parameter of the ratio of R to $\max\{|f(z')|\}$ indicates how close the effective complex scattering function $g(z')=R \cdot \delta(z') + f(z'-z_0)$ is to a true MPF. In the example numerical simulations discussed above, this ratio was chosen to be $1/0.04=25$. For typical imaged tissue samples, the scattering function is quite weak, so a ratio of 25 is a reasonable assumption. However, for certain embodiments in which $\max\{|f(z')|\} \ll 1$ is not satisfied, an uneven beam splitter can be used in the OCT configuration to increase this ratio. Other numerical simulations have shown that the iterative error-reduction method 100 of Figure 2 converges for ratios of R to $\max\{|f(z')|\}$ greater than about 10. Figures 7A and 7B show the magnitude and phase, respectively, of a simulated tissue scattering function (solid line) and a recovered tissue scattering function (dashed line) using the iterative error-reduction method 100 of Figure 2 for which $z_0=0$ and R is reduced to 0.2 while still keeping $\max\{|f(z')|\}=0.04$, i.e., a ratio of 5. As shown in Figures 7A and 7B, the recovered tissue scattering function in this case deviates from the simulated tissue scattering function, which is due to the lower value of the $R/\max\{|f(z')|\}$ ratio.

[0044] In certain examples, the reference mirror used in the lower arm of the Michelson interferometer shown in Figure 1B is a broadband mirror with a spatial scattering function which is a Dirac-delta function $\delta(z')$. In certain other examples, the spatial scattering function of the reference mirror is not a true delta function. In certain such examples, the reference mirror has a broader spatial scattering function and comprises a stacked dielectric mirror or a fiber Bragg grating. In certain examples in which the scattering function of the reference mirror is much narrower than the width of $f(z)$ (e.g., by a factor of 10), the iterative error-reduction method 100 illustrated by Figure 2 still converges to the unique solution. For certain examples in which the tissue thickness that is imaged is 1 millimeter, a reference mirror that has a spatial scattering function width of about 50 micrometers or less can be successfully used. For typical metal-coated reference mirrors, the spatial scattering function width is essentially less than a micron, so the spatial scattering function of such reference mirrors can be approximated by a true Dirac-delta function $\delta(z')$.

[0045] Figure 8 is a graph of a simulated power spectrum (dashed line) with an added 30% peak-to-peak amplitude uniform random noise (solid line) to illustrate the strength in terms of noise sensitivity of certain embodiments described herein by showing how measurement errors and noise in the power spectrum affect the accuracy of the recovered tissue scattering function. The resolution of the OSA in the simulation of Figure 8 was again limited to about 0.5 nanometer and all the other parameters of the simulation of Figure 8 were chosen to be the same as in the simulation of Figure 3. Figures 9A and 9B are graphs of the magnitude and phase, respectively, of the simulated tissue scattering function (solid lines) corresponding to the simulated power spectrum of Figure 8 and the recovered tissue scattering function (dashed lines) using the iterative error-reduction method 100 shown by Figure 2. As shown in Figures 9A and 9B, the agreement of both the magnitude and the phase between the simulated and recovered tissue scattering functions, under even 30% uniform random noise, is quite impressive. Almost all the details of the tissue scattering function have been recovered, demonstrating that in certain embodiments, the iterative error-reduction method 100 shown in Figure 2 could confidently be used even in a fairly noisy OCT configuration.

[0046] Figure 10 schematically illustrates an example frequency-domain OCT configuration 200 which can provide a large and easily realizable $R/\max\{|f(z')|\}$ ratio (e.g., greater than 10) to be utilized for $g(z')=R \cdot \delta(z') + f(z'-z_0)$. The frequency-domain OCT configuration 200 schematically illustrated by Figure 10 is simpler than the classical frequency-domain OCT configuration schematically illustrated by Figure 1B in that the configuration 200 has a single arm extending from the fiber coupler 50 towards the sample 40. Instead of the reference mirror 30 in the lower arm of the Michelson interferometer 20 shown in Figure 1B, the frequency-domain OCT configuration 200 uses the back reflection from a partially reflective element (e.g., the fiber end 70) as the reference signal. The partially reflective element is optically coupled to the light source 10, to the ODA 60, and to the sample 40. A first portion of light from the light source 10 is reflected by the partially reflective element and propagates to the OSA 60. A second portion of light from the light source 10 propagates through the partially reflective element, impinges the sample 40, reflects from the sample 40, and propagates to the OSA 60. In this configuration 200, the effective complex scattering function will still be of the form: $g(z')=R \cdot \delta(z') + f(z'-z_0)$. However, for certain examples utilizing a bare fiber end 70 in air as the partially reflective element, R will be limited to about 0.2. In certain such examples, the tissue sample 40 will generate a maximum magnitude of the tissue scattering function of less than about 0.02, i.e., $\max\{|f(z')|\} \lesssim 0.02$. In certain such examples, the function $g(z')=R \cdot \delta(z') + f(z'-z_0)$ will be close enough to a true MPF such that the error-reduction methods described herein can successfully be applied to uniquely image the complex tissue scattering function. In certain examples, the partially

reflective element comprises a tilted broadband attenuator positioned between the fiber coupler 50 and the tissue sample 40 to reduce the maximum value of the measured magnitude of the tissue scattering function. In certain other examples, a fiber end 70 coated with a partially reflective material is used to increase the value of R . Other examples of configurations are also disclosed as providing sufficiently large ratios of $R/\max\{|f(z^1)|\}$ to utilize the error-reduction method described herein.

[0047] For certain examples in which an angled fiber end 70 is used in the configuration schematically illustrated by Figure 10, the value of R approximates zero, such that there is no interference at the OSA. In certain such examples, the measured quantity will be simply the power spectrum $|F(f)|^2$ of the tissue's complex scattering function, $f(z)$. In certain embodiments, $f(z)$ will have a sharp peak close to the origin, due to the high reflection from the air-tissue interface, such that $f(z)$ approximates an MPF. Thus, in certain such examples, the whole complex $f(z)$ can be fully recovered from only the measurement of $|F(f)|^2$ using the analytical Hilbert transformation or the iterative error-reduction method discussed herein. In certain examples, this relatively simple, non-interferometric method based on MPFs advantageously provides fast imaging of most tissues. In certain examples, e.g., for measurements made from tissue which is a strong scattering source in deeper parts of the body, $f(z)$ would not approximate an MPF. Therefore, in such examples, the complex $f(z)$ would not be fully recovered from only the measurement of $|F(f)|^2$. However, an interferometric configuration in which R does not approximate zero can be used for such strongly scattering tissue, as described herein.

[0048] Various embodiments of the present invention have been described above. Although this invention has been described with reference to these specific embodiments, the descriptions are intended to be illustrative of the invention and are not intended to be limiting. Various modifications and applications may occur to those skilled in the art without departing from the scope of the invention as defined in the appended claims.

Claims

1. A method (100) based on minimum-phase functions for determining an estimated intermediate function which differs from a complex scattering function of a portion of a sample under analysis by the product of a spatial Dirac-delta function and a field reflectivity of a reference reflective element, whereby the intermediate function is close to a minimum-phase function, if not an exact minimum-phase function, the method comprising:

- (a) providing a magnitude spectrum of a complex spatial Fourier transform of a complex intermediate function, the complex intermediate function dependent on the complex scattering function of the portion of the sample under analysis, the magnitude spectrum obtained from power spectrum data of frequency-domain optical coherence tomography of the portion of the sample under analysis (110);
- (b) providing an estimated phase term of the complex spatial Fourier transform (120);
- (c) multiplying the magnitude spectrum and the estimated phase term together to generate an estimated complex spatial Fourier transform;
- (d) calculating an inverse Fourier transform of the estimated complex spatial Fourier transform, wherein the inverse Fourier transform of the estimated complex spatial Fourier transform is a spatial function (130); and
- (e) calculating the estimated intermediate function by applying at least one constraint to the inverse Fourier transform of the estimated complex spatial Fourier transform.

2. The method of Claim 1, further comprising:

- (f) calculating a Fourier transform of the estimated intermediate function; and
- (g) calculating a calculated phase term of the Fourier transform of the estimated intermediate function.

3. The method of Claim 2, wherein calculating the calculated phase term of the Fourier transform of the estimated intermediate function comprises using a Hilbert transformation of the Fourier transform of the estimated intermediate function.

4. The method of Claim 2, further comprising:

- (h) using the calculated phase term of (g) as the estimated phase term of (c) and repeating (c)-(e).

5. The method of Claim 4, wherein (c)-(h) are iteratively repeated until the estimated intermediate function reaches convergence.

6. The method of Claim 5, wherein convergence is reached when a difference between estimated intermediate functions

obtained after two consecutive iterations is less than a predetermined value.

7. The method of Claim 6, wherein the predetermined value is 0.1 % of the estimated intermediate function of an iteration.

8. The method of Claim 4, wherein (c)-(h) are iteratively repeated a predetermined number of times.

9. The method of Claim 1, wherein providing the magnitude spectrum of the complex spatial Fourier transform comprises measuring a frequency-domain optical coherence tomography power spectrum from the portion of the sample under analysis and calculating the square-root of the measured frequency-domain optical coherence tomography power spectrum.

10. The method of Claim 1, wherein providing the magnitude spectrum of the complex spatial Fourier transform comprises providing a previously-measured frequency-domain optical coherence tomography power spectrum and calculating the square-root of the previously-measured frequency-domain optical coherence tomography power spectrum or providing the square-root of a previously-measured frequency-domain optical coherence tomography power spectrum.

11. The method of Claim 1, wherein providing the estimated phase term comprises providing an initial estimated phase equal to a real or complex constant.

12. The method of Claim 1, wherein providing the estimated phase term comprises providing an initial estimated phase equal to a previously-stored function retrieved from a computer system.

13. The method of Claim 1, wherein providing the estimated phase term comprises providing a phase obtained from a different portion of the sample.

14. The method of Claim 13, wherein the different portion is adjacent to the portion of the sample under analysis.

15. The method of Claim 1, wherein providing the estimated phase term comprises providing a phase calculated from the magnitude spectrum using a logarithmic Hilbert transform.

16. The method of Claim 1, wherein the sample has a known spatial extent and applying the at least one constraint to the inverse Fourier transform of the estimated complex spatial Fourier transform comprises setting the inverse Fourier transform to zero for regions outside the known spatial extent of the sample.

17. The method of Claim 16, wherein the estimated intermediate function is forced to be causal by setting the inverse Fourier transform of the estimated complex spatial Fourier transform equal to zero for regions outside the known spatial extent of the sample.

18. A computer-readable medium having instructions stored thereon which cause a general-purpose computer to perform the method of Claim 1.

19. A computer system for performing the method of claim 1, comprising:

means for obtaining a magnitude spectrum of a complex spatial Fourier transform of a complex intermediate function, the complex intermediate function differs from a complex scattering function of a portion of a sample under analysis by the product of a spatial Dirac-delta function and a field reflectivity of a reference reflective element, the magnitude spectrum obtained from power spectrum data of frequency-domain optical coherence tomography of the portion of the sample under analysis;

means for estimating an estimated phase term of the complex spatial Fourier transform;

means for multiplying the magnitude spectrum and the estimated phase term together to generate an estimated complex spatial Fourier transform;

means for calculating an inverse Fourier transform of the estimated complex spatial Fourier transform, wherein the inverse Fourier transform of the estimated complex spatial Fourier transform is a spatial function; and

means for calculating the estimated intermediate function by applying at least one constraint to the inverse Fourier transform of the estimated complex spatial Fourier transform.

Patentansprüche

1. Verfahren (100), das auf Minimalphasen funktionen basiert, zum Bestimmen einer geschätzten Zwischenfunktion, die sich von einer komplexen Streufunktion eines zu analysierenden Teils einer Probe durch das Produkt einer räumlichen Dirac 'schen-Delta-Funktion und einer Feldreflektivität eines Bezugsreflexionselements unterscheidet, wobei die Zwischenfunktion nahe einer Minimalphasenfunktion ist, wenn nicht eine exakte Minimalphasenfunktion ist, wobei das Verfahren umfasst:
 - (a) Bereitstellen eines Magnitudenspektrums einer komplexen räumlichen Fourier-Transformation einer komplexen Zwischenfunktion, wobei die komplexe Zwischenfunktion von der komplexen Streufunktion des zu analysierenden Teils der Probe abhängig ist, wobei das Magnitudenspektrum aus den Leistungsspektrumsdaten der optischen Frequenzdomänen-Kohärenztomographie des zu analysierenden Teils der Probe (110) erhalten wird;
 - (b) Bereitstellen einer geschätzten Phasenbedingung der komplexen räumlichen Fourier-Transformation (120);
 - (c) Multiplizieren des Magnitudenspektrums und der geschätzten Phasenbedingung, um eine geschätzte komplexe räumliche Fourier-Transformation zu erzeugen;
 - (d) Berechnen einer inversen Fourier-Transformation der geschätzten komplexen räumlichen Fourier-Transformation, wobei die inverse Fourier-Transformation der geschätzten komplexen räumlichen Fourier-Transformation eine räumliche Funktion (130) ist; und
 - (e) Berechnen der geschätzten Zwischenfunktion durch Anwenden zumindest einer Einschränkung auf die inverse Fourier-Transformation der geschätzten komplexen räumlichen Fourier-Transformation.
2. Verfahren nach Anspruch 1, ferner umfassend:
 - (f) Berechnen einer Fourier-Transformation der geschätzten Zwischenfunktion; und
 - (g) Berechnen einer berechneten Phasenbedingung der Fourier-Transformation der geschätzten Zwischenfunktion.
3. Verfahren nach Anspruch 2, wobei das Berechnen der berechneten Phasenbedingung der Fourier-Transformation der geschätzten Zwischenfunktion mithilfe einer Hilbert-Transformation der Fourier-Transformation der geschätzten Zwischenfunktion umfasst.
4. Verfahren nach Anspruch 2, ferner umfassend:
 - (h) Verwenden der berechneten Phasenbedingung von (g) als die geschätzte Phasenbedingung von (c) und Wiederholen von (c)-(e).
5. Verfahren nach Anspruch 4, wobei (c)-(h) iterativ wiederholt werden, bis die geschätzte Zwischenfunktion Konvergenz erreicht.
6. Verfahren nach Anspruch 5, wobei Konvergenz erreicht wird, wenn eine Differenz zwischen geschätzten Zwischenfunktionen, die nach zwei aufeinanderfolgenden Iterationen erhalten wurden, weniger als ein vorab definierter Wert beträgt.
7. Verfahren nach Anspruch 6, wobei der vorab definierte Wert 0,1 % der geschätzten Zwischenfunktion einer Iteration beträgt.
8. Verfahren nach Anspruch 4, wobei (c)-(h) eine vorab definierte Anzahl von Malen iterativ wiederholt werden.
9. Verfahren nach Anspruch 1, wobei das Bereitstellen des Magnitudenspektrums der komplexen räumlichen Fourier-Transformation das Messen eines Leistungsspektrums einer optischen Frequenzdomänen-Kohärenztomographie anhand des zu analysierenden Teils der Probe und das Berechnen der Quadratwurzel des gemessenen Leistungsspektrums der optischen Frequenzdomänen-Kohärenztomographie umfasst.
10. Verfahren nach Anspruch 1, wobei das Bereitstellen des Magnitudenspektrums der komplexen räumlichen Fourier-Transformation das Bereitstellen eines zuvor gemessenen Leistungsspektrums der optischen Frequenzdomänen-Kohärenztomographie und das Berechnen der Quadratwurzel des zuvor gemessenen Leistungsspektrums der optischen Frequenzdomänen-Kohärenztomographie oder das Bereitstellen der Quadratwurzel eines zuvor gemess-

senen Leistungsspektrums der optischen Frequenzdomänen-Kohärenztomographie umfasst.

11. Verfahren nach Anspruch 1, wobei das Bereitstellen der geschätzten Phasenbedingung das Bereitstellen einer anfänglichen geschätzten Phase umfasst, die einer reellen oder komplexen Konstante gleicht.

12. Verfahren nach Anspruch 1, wobei das Bereitstellen der geschätzten Phasenbedingung das Bereitstellen einer anfänglichen geschätzten Phase umfasst, die einer zuvor gespeicherten, aus einem Computersystem abgerufenen Funktion gleicht.

13. Verfahren nach Anspruch 1, wobei das Bereitstellen einer geschätzten Phasenbedingung das Bereitstellen einer Phase umfasst, die aus einem anderen Teil der Probe erhalten wurde.

14. Verfahren nach Anspruch 13, wobei der andere Teil benachbart dem zu analysierenden Teil der Probe vorliegt.

15. Verfahren nach Anspruch 1, wobei das Bereitstellen der geschätzten Phasenbedingung das Bereitstellen einer Phase umfasst, die mithilfe einer logarithmischen Hilbert-Transformation aus dem Magnitudenspektrum berechnet wurde.

16. Verfahren nach Anspruch 1, wobei die Probe eine bekannte räumliche Ausdehnung aufweist, und wobei das Anwenden der zumindest einen Einschränkung auf die inverse Fourier-Transformation der geschätzten komplexen räumlichen Fourier-Transformation das Einstellen der inversen Fourier-Transformation auf null für Bereiche außerhalb der bekannten räumlichen Ausdehnung der Probe umfasst.

17. Verfahren nach Anspruch 16, wobei die geschätzte Zwischenfunktion gezwungen wird, kausal zu sein, indem die inverse Fourier-Transformation der geschätzten komplexen räumlichen Fourier-Transformation auf gleich null für Bereiche außerhalb der bekannten räumlichen Ausdehnung der Probe eingestellt wird.

18. Computerlesbares Medium, auf dem Anweisungen gespeichert sind, die bewirken, dass ein Universal computer das Verfahren nach Anspruch 1 ausführt.

19. Computersystem zum Ausführen des Verfahrens nach Anspruch 1, umfassend:

Mittel zum Erhalten eines Magnitudenspektrums einer komplexen räumlichen Fourier-Transformation einer komplexen Zwischenfunktion, wobei sich die komplexe Zwischenfunktion von einer komplexen Streufunktion eines zu analysierenden Teils einer Probe durch das Produkt einer räumlichen Dirac'schen-Delta-Funktion und einer Feldreflektivität eines Bezugsreflexionselements unterscheidet, wobei das Magnitudenspektrum aus den Leistungsspektrumsdaten der optischen Frequenzdomänen-Kohärenztomographie des zu analysierenden Teils der Probe erhalten wird;

Mittel zum Schätzen einer geschätzten Phasenbedingung der komplexen räumlichen Fourier-Transformation; Mittel zum Multiplizieren des Magnitudenspektrums und der geschätzten Phasenbedingung, um eine geschätzte komplexe räumliche Fourier-Transformation zu erzeugen;

Mittel zum Berechnen einer inversen Fourier-Transformationen der geschätzten komplexen räumlichen Fourier-Transformation, wobei die inverse Fourier-Transformation der geschätzten komplexen räumlichen Fourier-Transformation eine räumliche Funktion ist; und

Mittel zum Berechnen der geschätzten Zwischenfunktion durch Anwenden zumindest einer Einschränkung auf die inverse Fourier-Transformation der geschätzten komplexen räumlichen Fourier-Transformation.

Revendications

1. Procédé (100) basé sur des fonctions à phase minimale pour déterminer une fonction intermédiaire estimée qui diffère d'une fonction de diffusion complexe d'une partie d'un échantillon faisant l'objet d'une analyse du produit d'une fonction delta de Dirac spatiale et d'une réflectivité de champ d'un élément réfléchissant de référence, moyennant quoi la fonction intermédiaire est proche d'une fonction à phase minimale, voire d'une fonction à phase minimale exacte, le procédé comprenant :

(a) la fourniture d'un spectre d'amplitude d'une transformée de Fourier spatiale complexe d'une fonction intermédiaire complexe, la fonction intermédiaire complexe dépendant de la fonction de diffusion complexe de la

partie de l'échantillon faisant l'objet de l'analyse, le spectre d'amplitude étant obtenu à partir des données de spectre de puissance de la tomographie par cohérence optique en domaine de fréquence de la partie de l'échantillon faisant l'objet de l'analyse (110) ;

(b) la fourniture d'un terme de phase estimé de la transformée de Fourier spatiale complexe (120) ;

(c) la multiplication du spectre d'amplitude par le terme de phase estimé pour générer une transformée de Fourier spatiale complexe estimée ;

(d) le calcul d'une transformée de Fourier inverse de la transformée de Fourier spatiale complexe estimée, la transformée de Fourier inverse de la transformée de Fourier spatiale complexe estimée étant une fonction spatiale (130) ; et

(e) le calcul de la fonction intermédiaire estimée en appliquant au moins une contrainte à la transformée de Fourier inverse de la transformée de Fourier spatiale complexe estimée.

2. Procédé selon la revendication 1, comprenant en outre :

(f) le calcul d'une transformée de Fourier de la fonction intermédiaire estimée ; et

(g) le calcul d'un terme de phase calculé de la transformée de Fourier de la fonction intermédiaire estimée.

3. Procédé selon la revendication 2, dans lequel le calcul du terme de phase calculé de la transformée de Fourier de la fonction intermédiaire estimée comprend l'utilisation d'une transformation de Hilbert de la transformée de Fourier de la fonction intermédiaire estimée.

4. Procédé selon la revendication 2, comprenant en outre :

(h) l'utilisation du terme de phase calculé de (g) en tant que terme de phase estimé de (c) et répéter (c) à (e).

5. Procédé selon la revendication 4, dans lequel (c) à (h) sont répétés itérativement jusqu'à ce que la fonction intermédiaire estimée atteigne la convergence.

6. Procédé selon la revendication 5, dans lequel la convergence est atteinte lorsqu'une différence entre les fonctions intermédiaires estimées obtenues après deux itérations consécutives est inférieure à une valeur prédéterminée.

7. Procédé selon la revendication 6, dans lequel la valeur prédéterminée représente 0,1 % de la fonction intermédiaire estimée d'une itération.

8. Procédé selon la revendication 4, dans lequel (c) à (h) sont répétés itérativement un nombre prédéterminé de fois.

9. Procédé selon la revendication 1, dans lequel la fourniture du spectre d'amplitude de la transformée de Fourier spatiale complexe comprend la mesure d'un spectre de puissance de la tomographie par cohérence optique en domaine de fréquence à partir de la partie de l'échantillon faisant l'objet de l'analyse et le calcul de la racine carrée du spectre de puissance de la tomographie par cohérence optique en domaine de fréquence mesurée.

10. Procédé selon la revendication 1, dans lequel la fourniture du spectre d'amplitude de la transformée de Fourier spatiale complexe comprend la fourniture d'un spectre de puissance de la tomographie par cohérence optique en domaine de fréquence précédemment mesurée et le calcul de la racine carrée du spectre de puissance de la tomographie par cohérence optique en domaine de fréquence précédemment mesurée ou la fourniture de la racine carrée du spectre de puissance de la tomographie par cohérence optique en domaine de fréquence précédemment mesurée.

11. Procédé selon la revendication 1, dans lequel la fourniture du terme de phase estimée comprend la fourniture d'une phase estimée initiale égale à une constante réelle ou complexe.

12. Procédé selon la revendication 1, dans lequel la fourniture du terme de phase estimée comprend la fourniture d'une phase estimée initiale égale à une fonction précédemment mémorisée récupérée à partir d'un système informatique.

13. Procédé selon la revendication 1, dans lequel la fourniture du terme de phase estimée comprend la fourniture d'une phase obtenue à partir d'une partie différente de l'échantillon.

14. Procédé selon la revendication 13, dans lequel la partie différente est adjacente à la partie de l'échantillon faisant

l'objet de l'analyse.

15. Procédé selon la revendication 1, dans lequel la fourniture du terme de phase estimé comprend la fourniture d'une phase calculée à partir du spectre d'amplitude au moyen d'une transformée de Hilbert logarithmique.

16. Procédé selon la revendication 1, dans lequel l'échantillon a une étendue spatiale connue et l'application de l'au moins une contrainte à la transformée de Fourier inverse de la transformée de Fourier spatiale complexe estimée comprend la définition de la transformée de Fourier inverse à zéro pour les régions extérieures à l'étendue spatiale connue de l'échantillon.

17. Procédé selon la revendication 16, dans lequel la fonction intermédiaire estimée est forcée à être causale par définition de la transformée de Fourier inverse de la transformée de Fourier spatiale complexe estimée égale à zéro pour les régions extérieures à l'étendue spatiale connue de l'échantillon.

18. Support lisible par ordinateur sur lequel sont stockées des instructions qui permettent l'exécution du procédé selon la revendication 1 par un ordinateur universel.

19. Système informatique pour effectuer le procédé selon la revendication 1, comprenant :

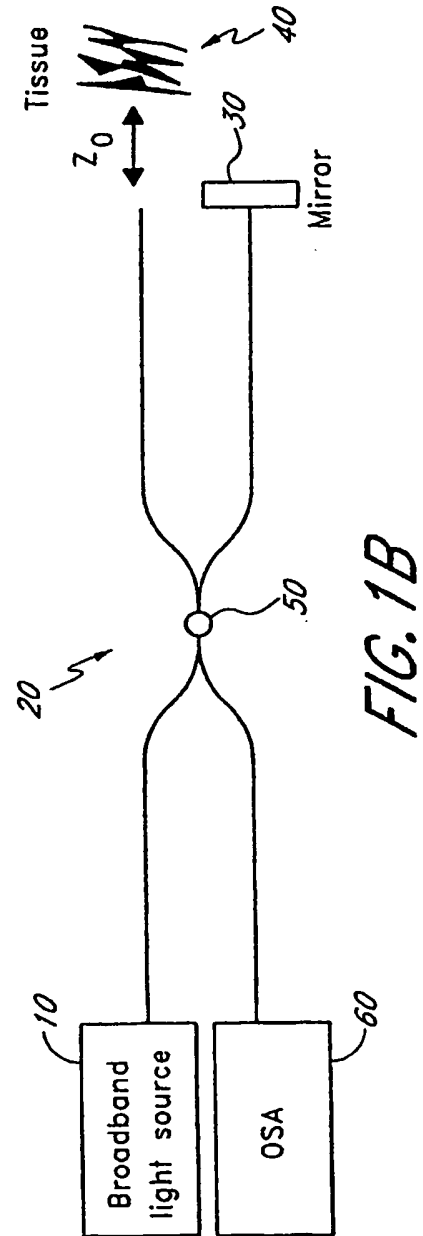
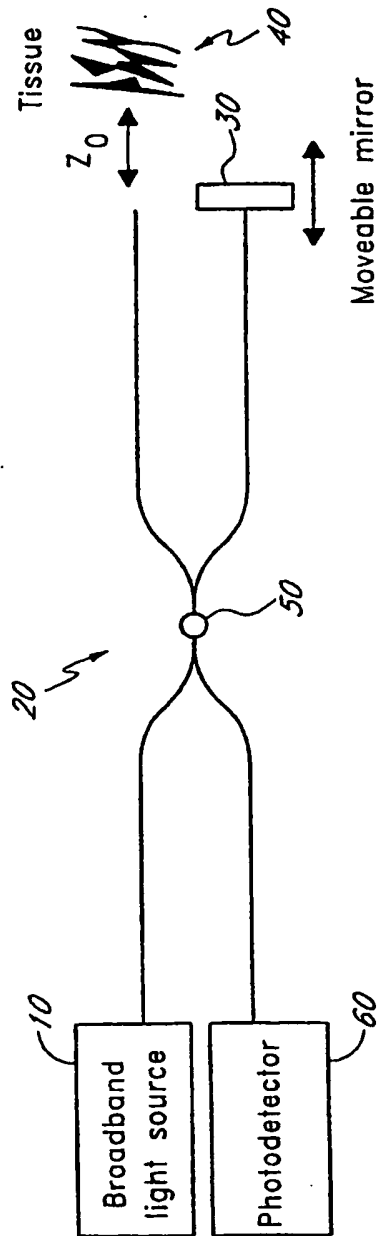
des moyens pour obtenir un spectre d'amplitude d'une transformée de Fourier spatiale complexe d'une fonction intermédiaire complexe, la fonction intermédiaire complexe différant d'une fonction de diffusion complexe d'une partie d'un échantillon faisant l'objet d'une analyse du produit d'une fonction delta de Dirac spatiale et d'une réflectivité de champ d'un élément réfléchissant de référence, le spectre d'amplitude étant obtenu à partir des données de spectre de puissance de la tomographie par cohérence optique en domaine de fréquence de la partie de l'échantillon faisant l'objet de l'analyse ;

des moyens pour estimer un terme de phase estimé de la transformée de Fourier spatiale complexe ;

des moyens pour multiplier le spectre d'amplitude par le terme de phase estimé pour générer une transformée de Fourier spatiale complexe estimée ;

des moyens pour calculer une transformée de Fourier inverse de la transformée de Fourier spatiale complexe estimée, la transformée de Fourier inverse de la transformée de Fourier spatiale complexe estimée étant une fonction spatiale ; et

des moyens pour calculer la fonction intermédiaire estimée en appliquant au moins une contrainte à la transformée de Fourier inverse de la transformée de Fourier spatiale complexe estimée.



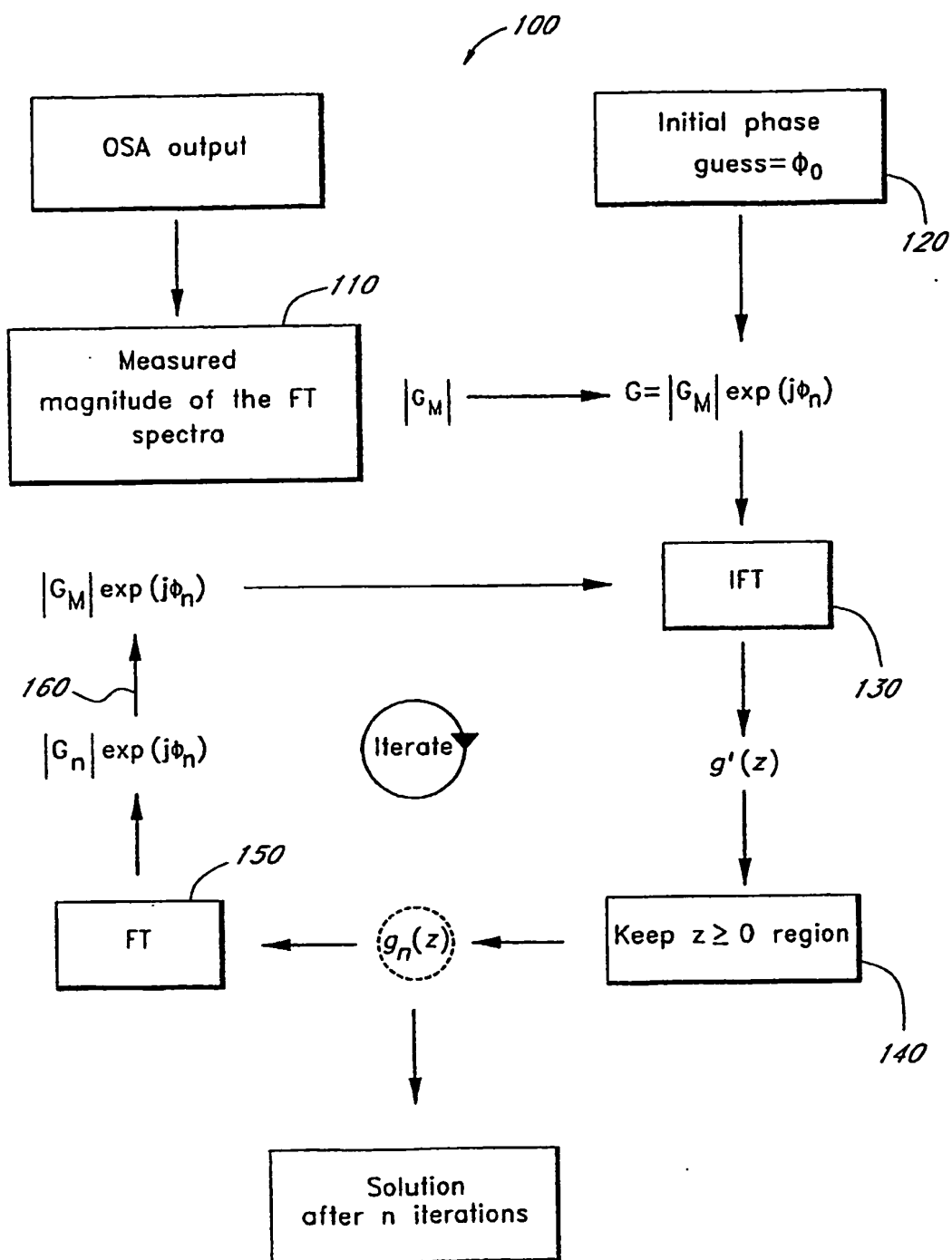


FIG. 2

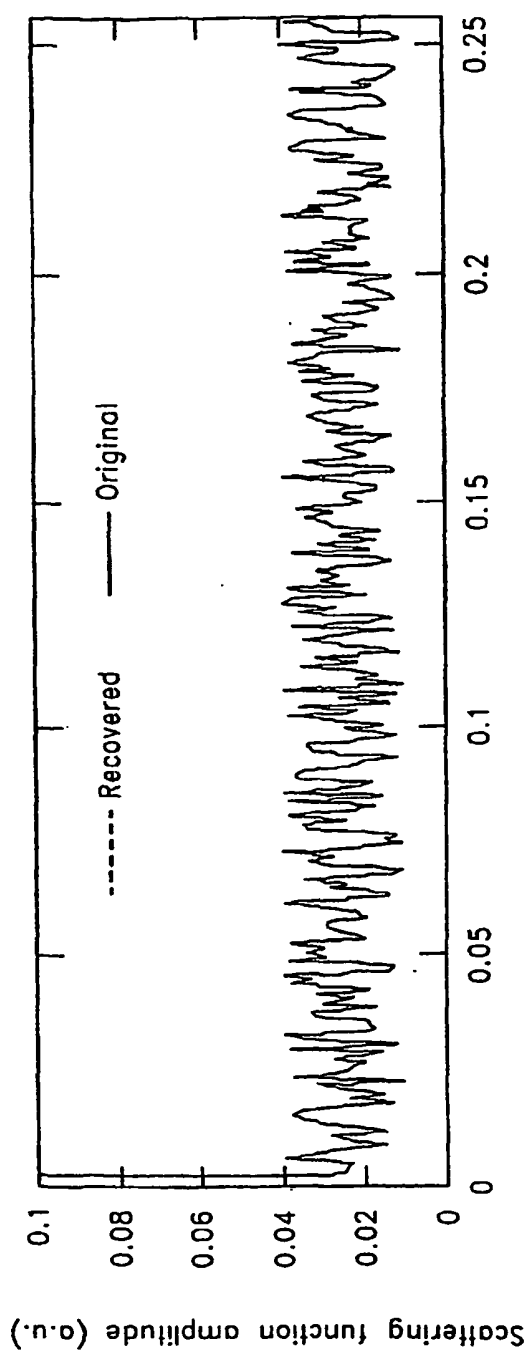


FIG. 3A

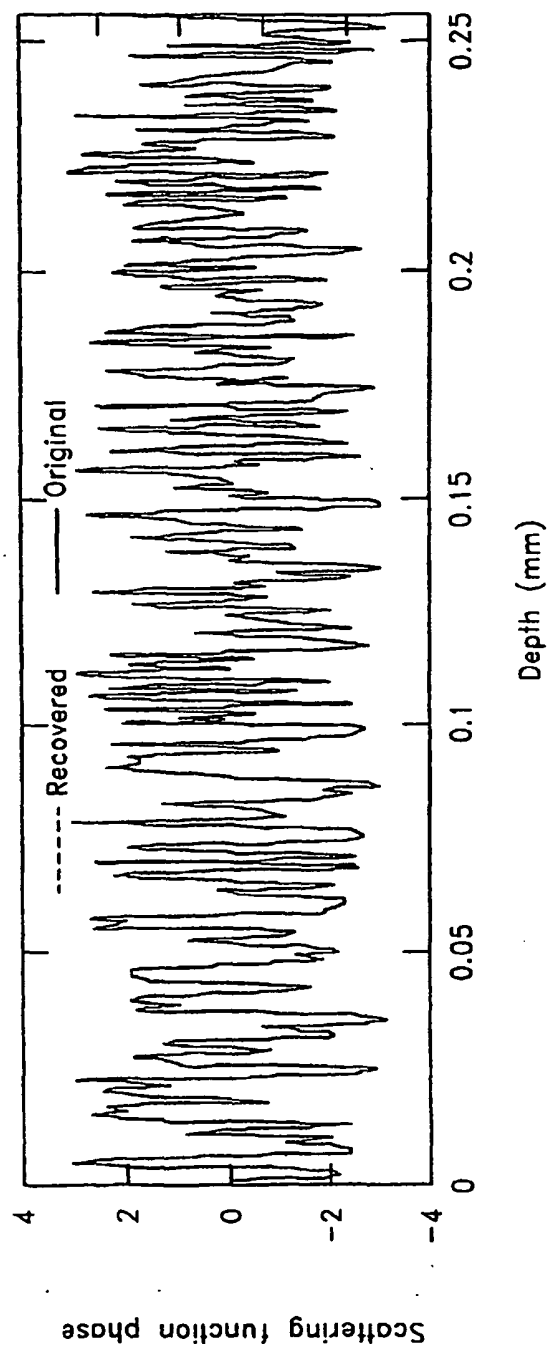


FIG. 3B

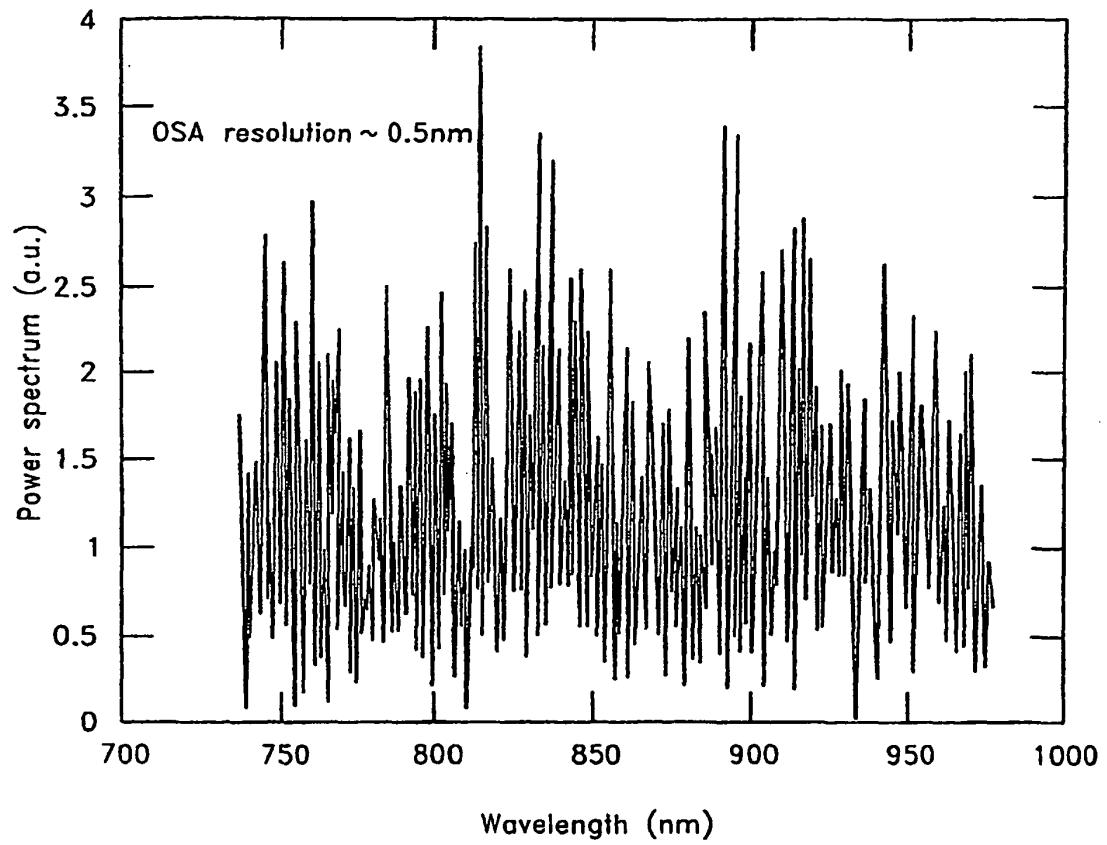


FIG. 4

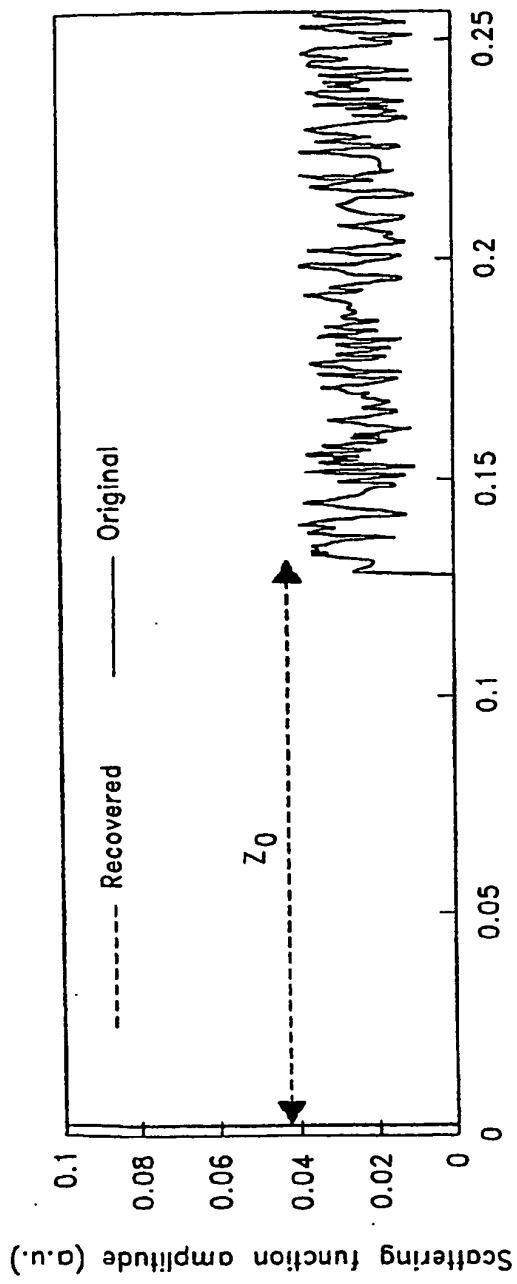


FIG. 5A

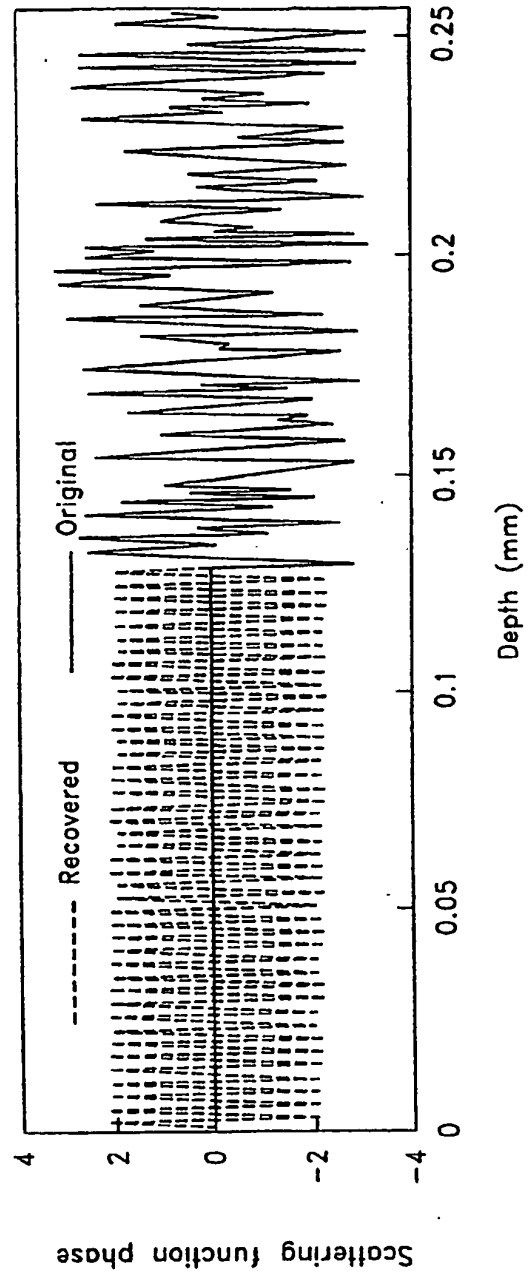


FIG. 5B

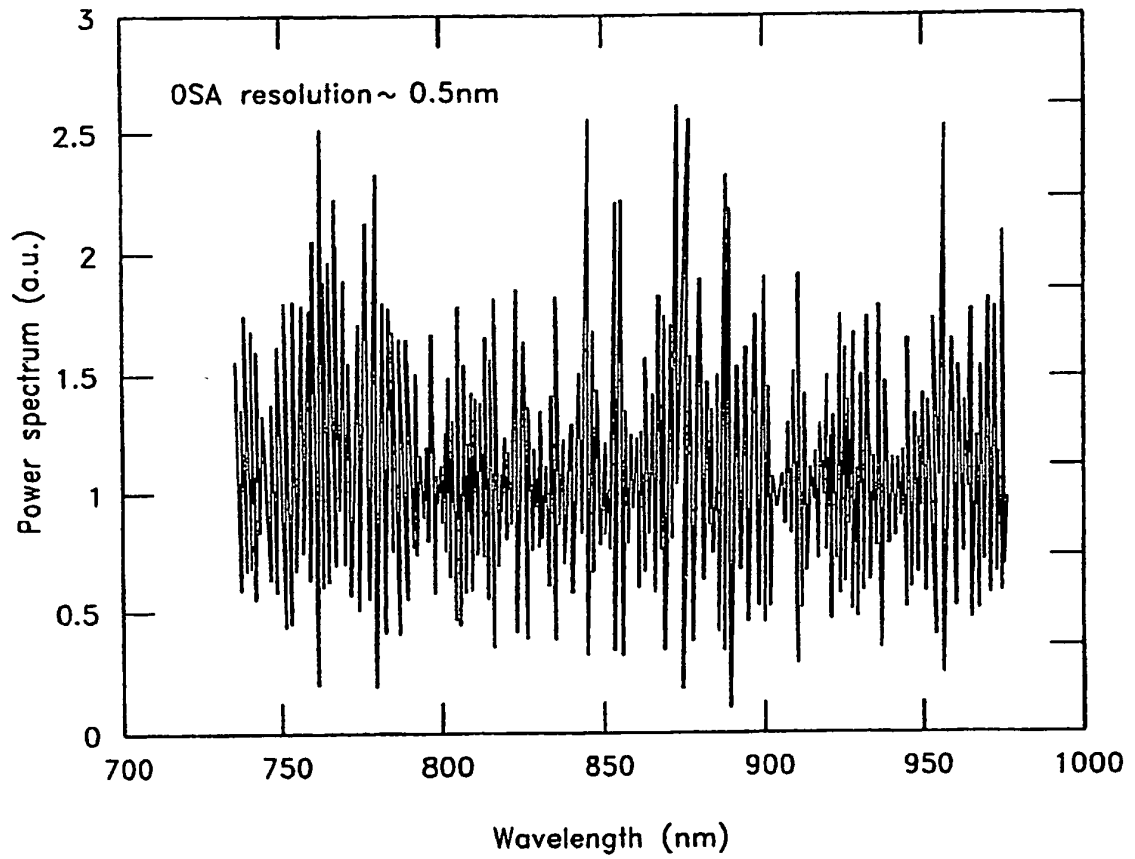


FIG. 6

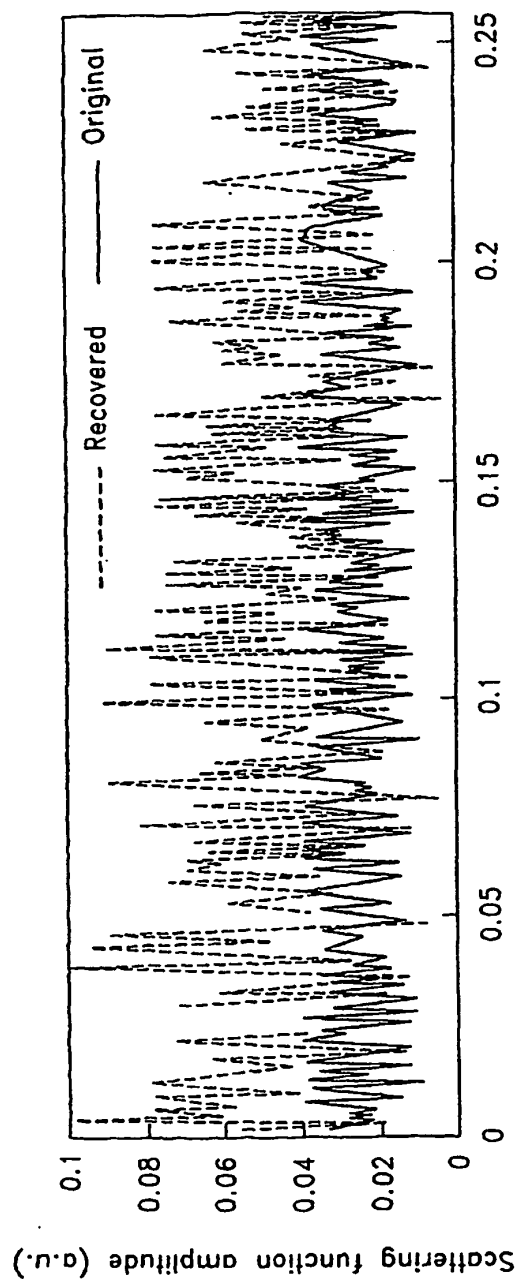


FIG. 7A

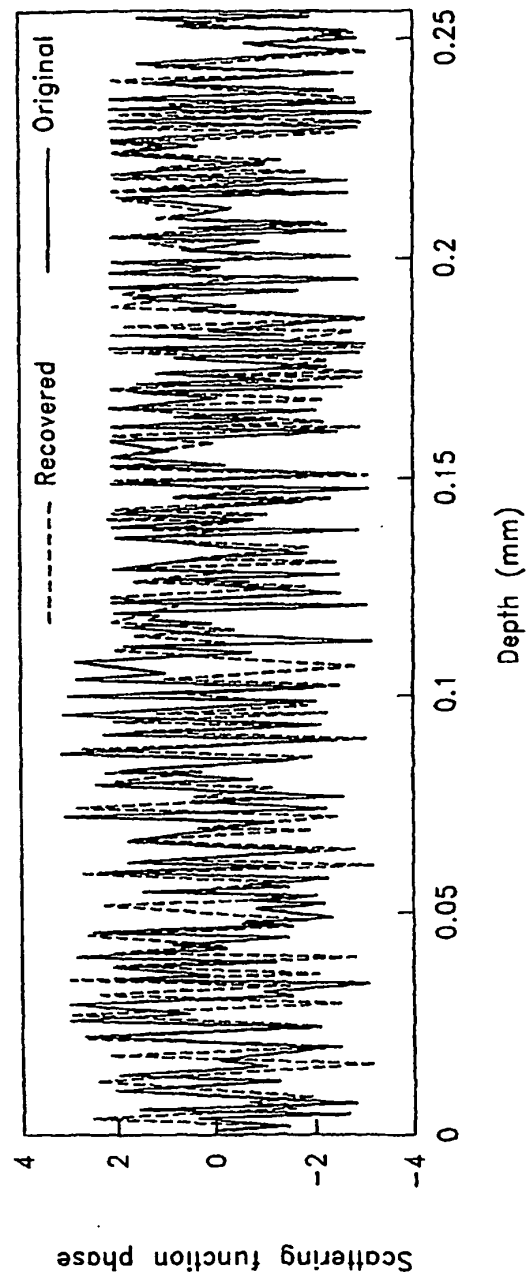
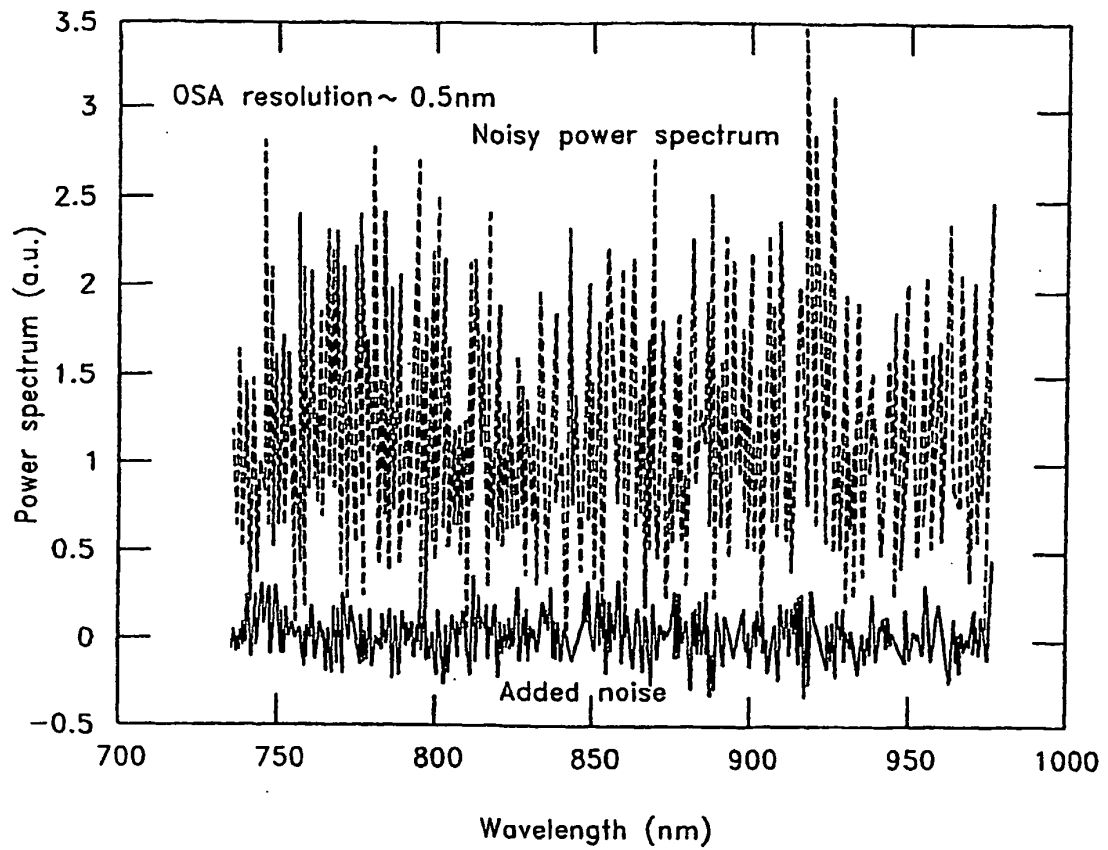


FIG. 7B

*FIG. 8*

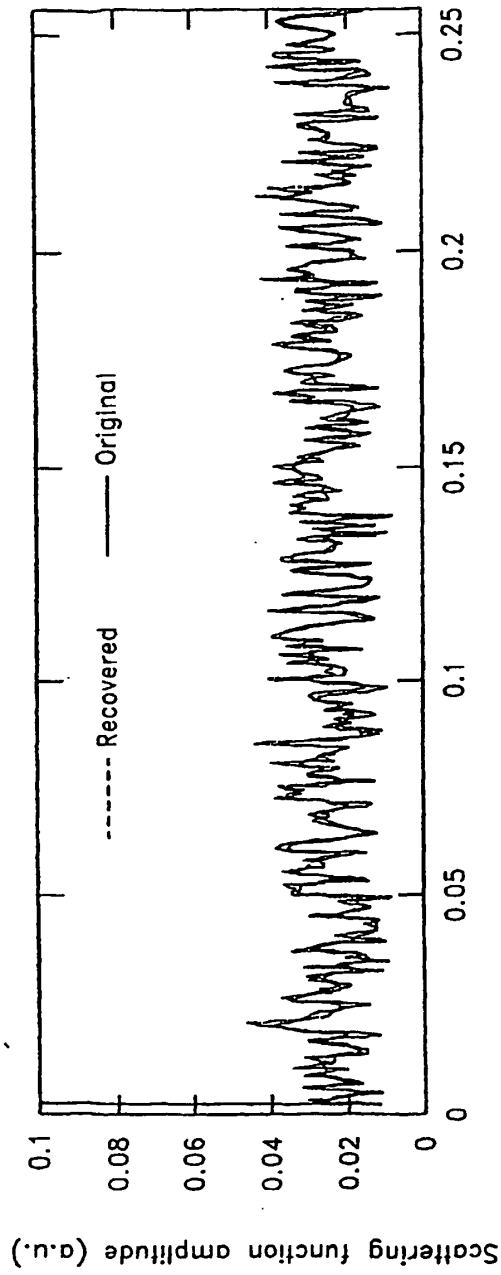


FIG. 9A

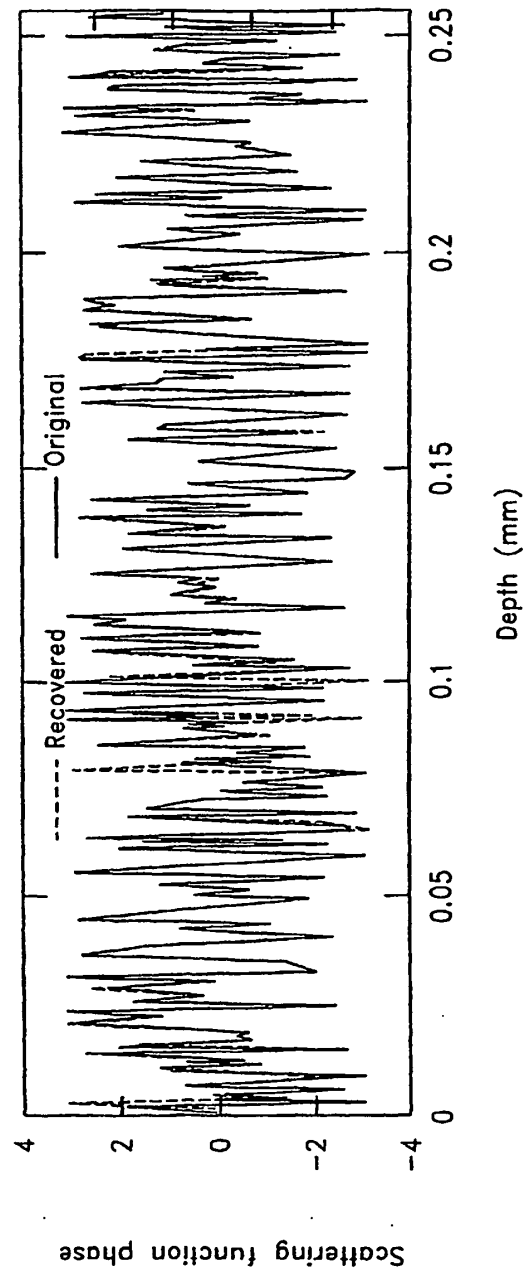


FIG. 9B

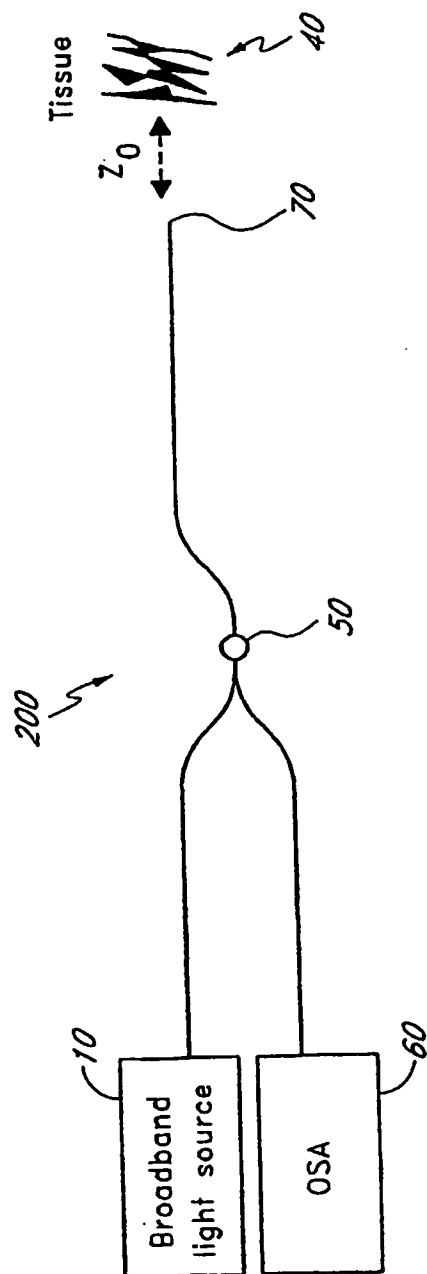


FIG. 10

REFERENCES CITED IN THE DESCRIPTION

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专利名称(译)	用于频域光学相干断层扫描的设备和方法		
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摘要(译)

方法确定分析中的一部分样品的复杂散射函数。该方法包括提供复杂中间函数的复空间傅里叶变换的幅度谱。复杂的中间函数取决于所分析样品部分的复杂散射函数。幅度谱是从正在分析的样品部分的频域光学相干断层扫描的功率谱数据获得的。该方法还包括提供复空间傅立叶变换的估计相位项。该方法还包括将幅度谱和估计的相位项相乘在一起以生成估计的复空间傅立叶变换。该方法还包括计算估计的复空间傅里叶变换的逆傅里叶变换。估计的复空间傅立叶变换的逆傅里叶变换是空间函数。该方法还包括通过将至少一个约束应用于估计的复空间傅立叶变换的逆傅立叶变换来计算估计的中间函数。

$$I(k') = S(k') \cdot \left| \int_{-\infty}^{\infty} g(z') \cdot \exp(jk'z') \cdot dz' \right|^2 \quad (1)$$