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Nishihara et al.

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(54) **LIQUID CRYSTAL DISPLAY DEVICE**

(75) Inventors: **Yusuke Nishihara**, Osaka (JP); **Iori Aoyama**, Osaka (JP); **Tokio Taguchi**, Osaka (JP); **Akihiro Yamamoto**, Osaka (JP); **Masumi Kubo**, Osaka (JP)

(73) Assignee: **Sharp Kabushiki Kaisha**, Osaka (JP)

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G02F 1/1335 (2006.01)

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349/56, 113, 116, 114, 136, 96, 97, 98, 99,
349/102, 103

See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

6,661,488 B1 12/2003 Takeda et al.

7,453,639 B2 * 11/2008 Katsura 359/460
2005/0213245 A1 * 9/2005 Katsura et al. 360/125
(Continued)

FOREIGN PATENT DOCUMENTS

JP 09-127309 A 5/1997
(Continued)

OTHER PUBLICATIONS

English translation of Official Communication issued in corresponding International Application PCT/JP2008/003443, mailed on Jun. 17, 2010.

(Continued)

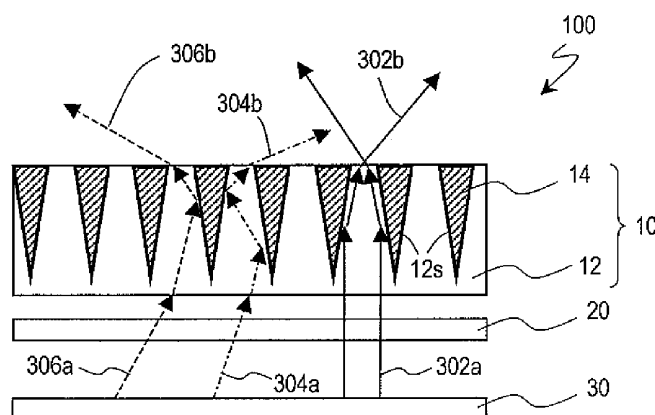
Primary Examiner — Brian Healy

(74) Attorney, Agent, or Firm — Keating & Bennett, LLP

(57) **ABSTRACT**

A liquid crystal display device of the present invention includes a liquid crystal display panel, and a light diffusing layer which has first and second major surfaces and which is arranged such that the first major surface opposes a viewer side surface of the liquid crystal display panel. The light diffusing layer includes a first region formed of a first substance which has a first refractive index N_1 and a plurality of second regions formed of a second substance which has a second refractive index N_2 ($<N_1$). The second regions are arranged in the first region at a predetermined pitch P in one direction in a plane parallel to the second major surface, each of the second regions forms interfaces with the first region, the interfaces being inclined by α° from a normal of the second major surface. θ_B which is expressed by $\theta_B = \tan^{-1}(a/Lb)$ is not more than 1.7 arc minutes where Lb is a typical viewing distance, and a is expressed by $a = \tan \theta' \times Lt$, in which θ' is an angle of incidence that is obtained from α , N_1 , and N_2 , and Lt is a distance from the second major surface to a liquid crystal layer side surface of a viewer side substrate of the liquid crystal display panel. According to the present invention, the viewing angle characteristics of a direct-viewing type liquid crystal display device can be improved by using a light diffusing layer that utilizes total reflection.

15 Claims, 13 Drawing Sheets



U.S. PATENT DOCUMENTS

2006/0245060 A1 11/2006 Goto
2010/0245736 A1* 9/2010 Nishihara et al. 349/112
2010/0245738 A1* 9/2010 Nishihara et al. 349/112
2010/0283947 A1* 11/2010 Nishihara et al. 349/112

FOREIGN PATENT DOCUMENTS

JP 2003-050307 A 2/2003
JP 2006-084876 A 3/2006
JP 2007-140403 A 6/2007
JP 2008-191176 A 8/2008

OTHER PUBLICATIONS

Official Communication issued in International Patent Application No. PCT/JP2008/003443, mailed on Dec. 16, 2008.
Aoyama et al., "Light Diffusion Sheet and Liquid Crystal Display Device," U.S. Appl. No. 12/681,414, filed Apr. 2, 2010.
Nishihara et al., "Light Diffusion Sheet and Liquid Crystal Display Device," U.S. Appl. No. 12/681,411, filed Apr. 2, 2010.
Nishihara et al., "Liquid Crystal Display," U.S. Appl. No. 12/743,935, filed May 20, 2010.

* cited by examiner

FIG. 1

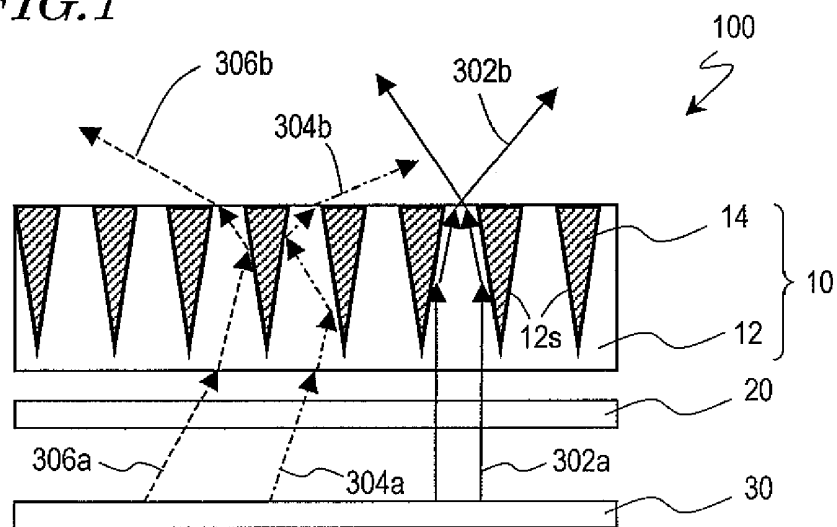


FIG. 2

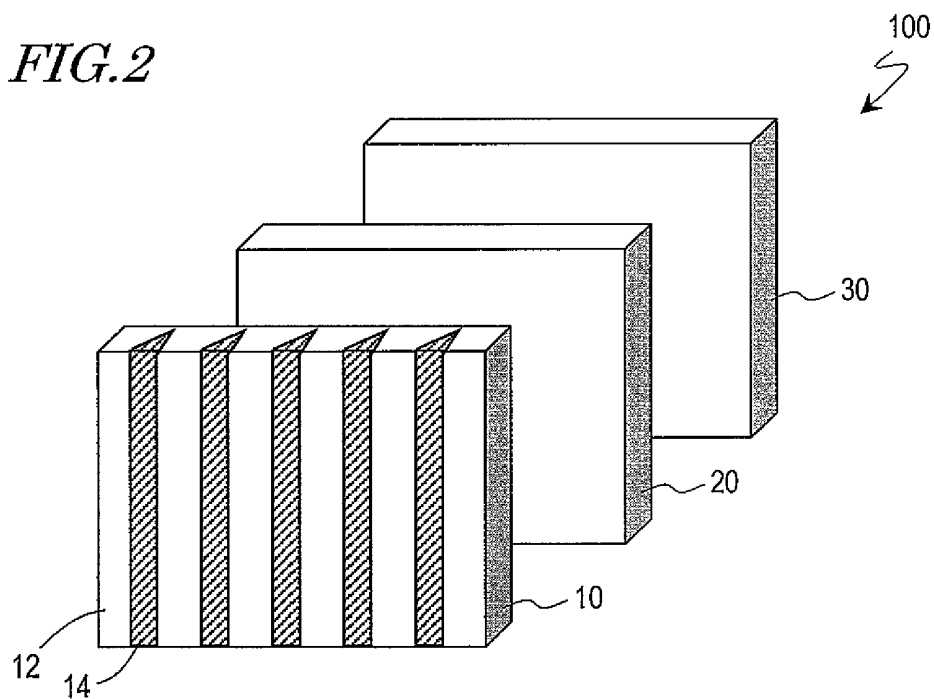


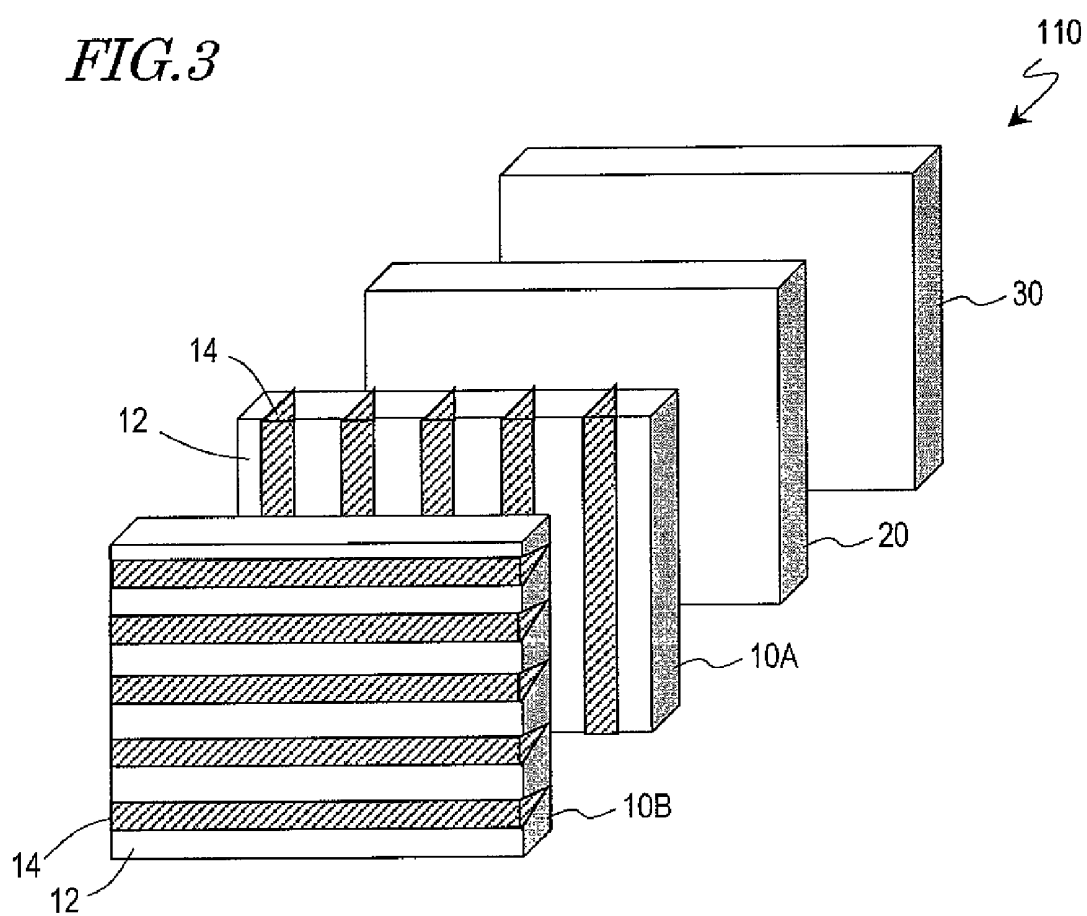
FIG. 3

FIG. 4

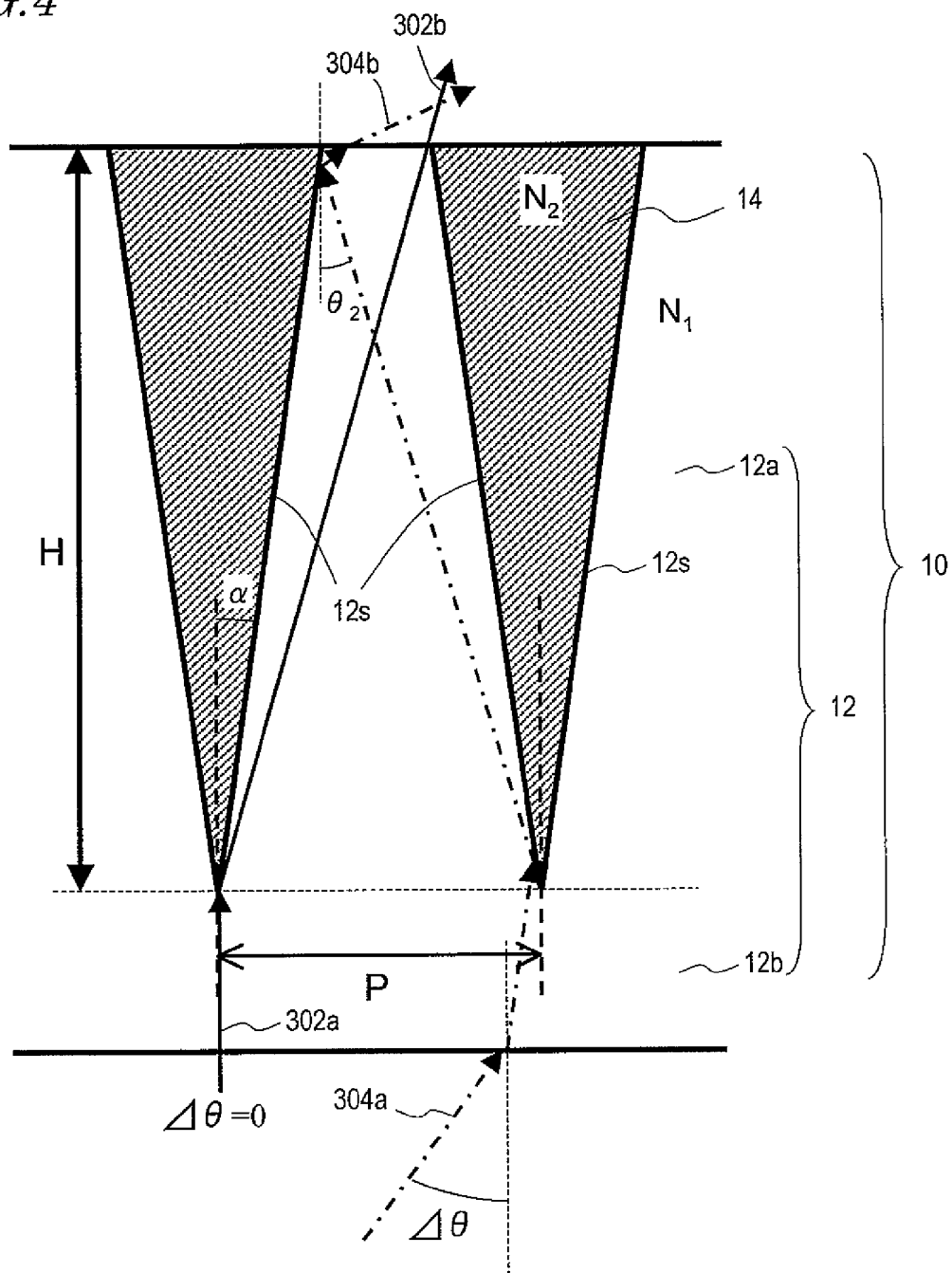


FIG. 5

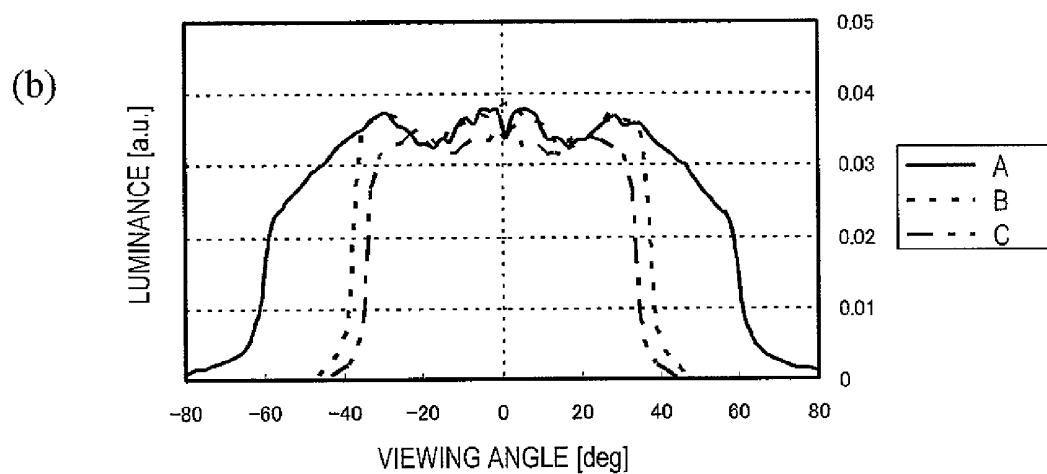
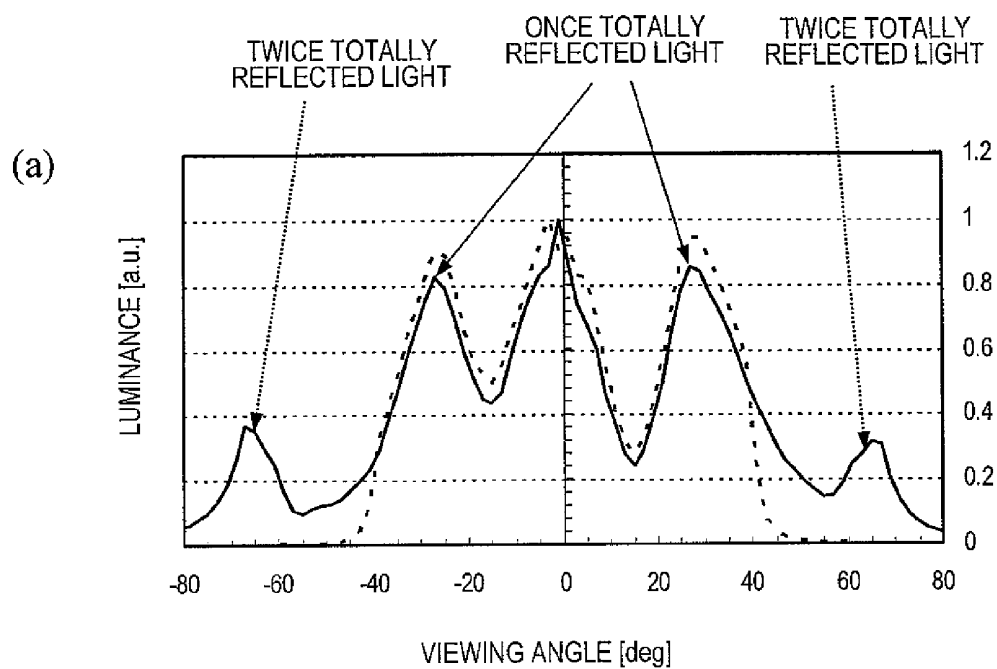


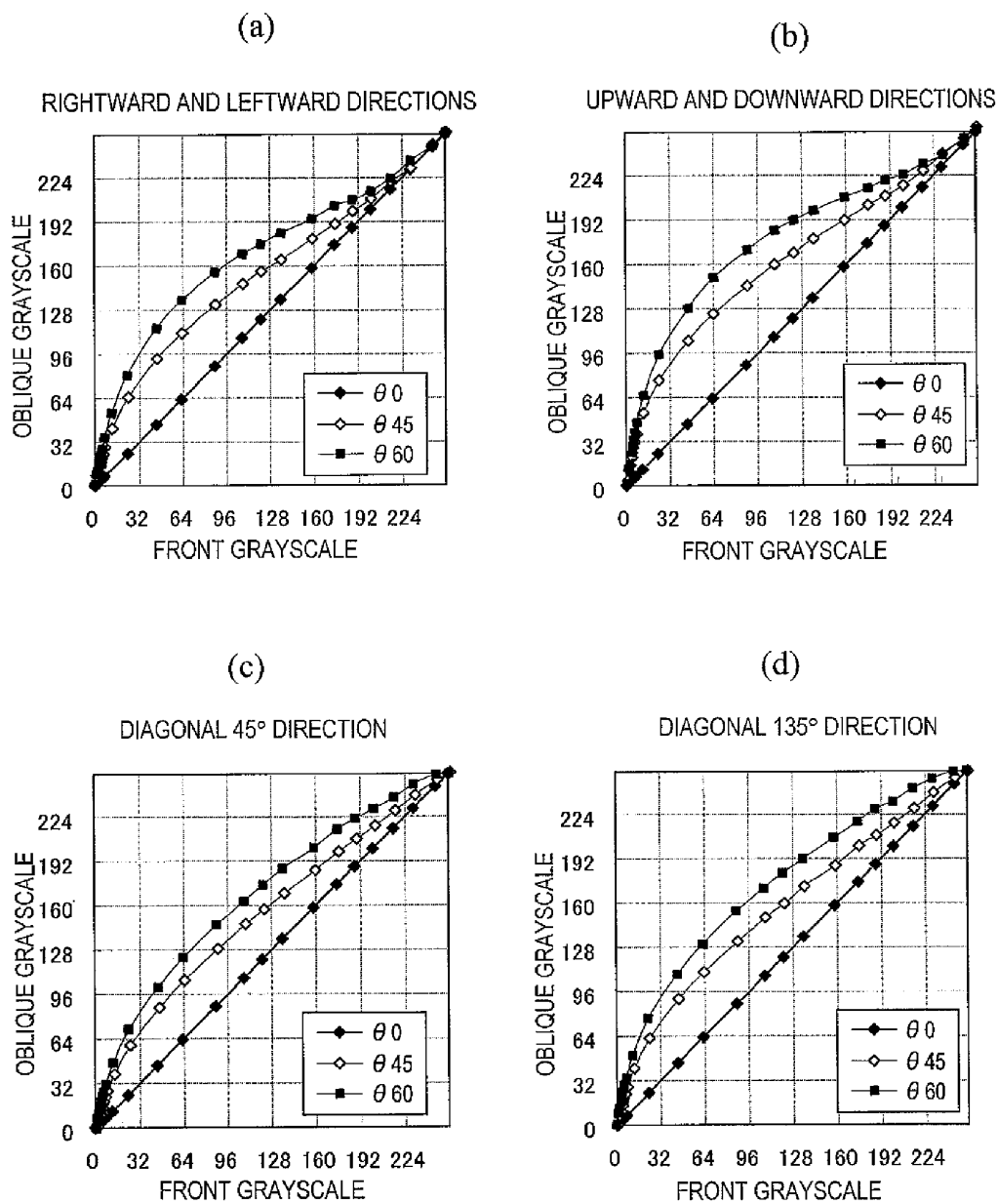
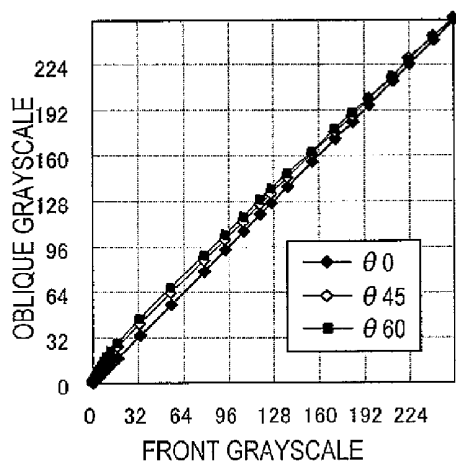
FIG. 6

FIG. 7

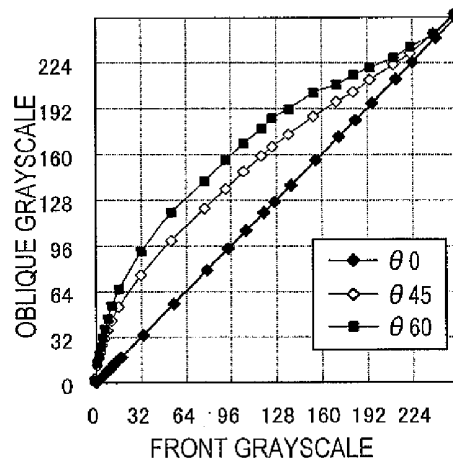
(a)

RIGHTWARD AND LEFTWARD DIRECTIONS



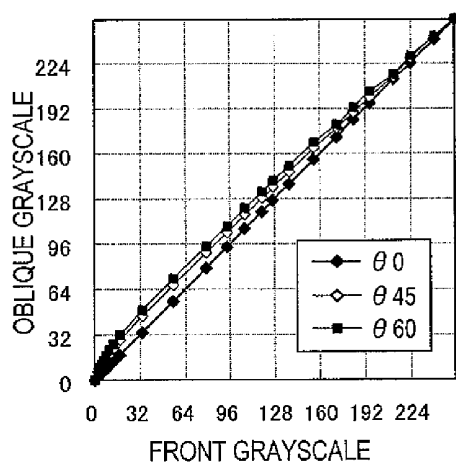
(b)

UPWARD AND DOWNWARD DIRECTIONS



(c)

DIAGONAL 45° DIRECTION



(d)

DIAGONAL 135° DIRECTION

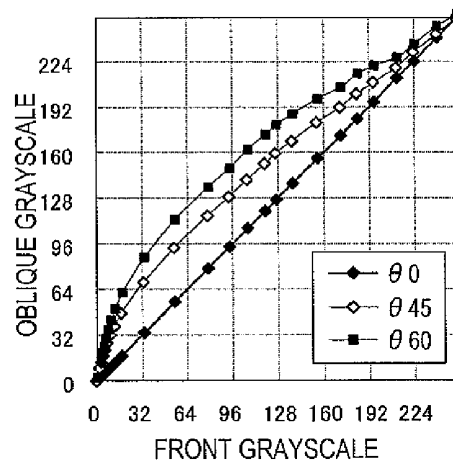
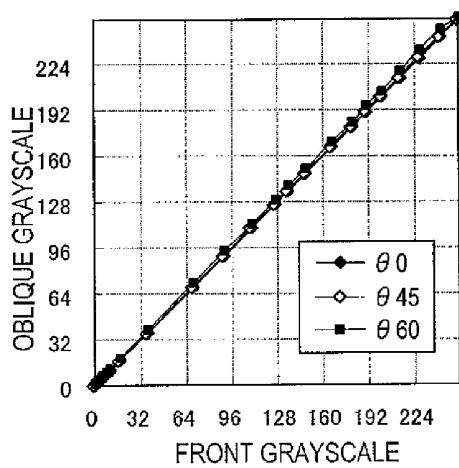


FIG. 8

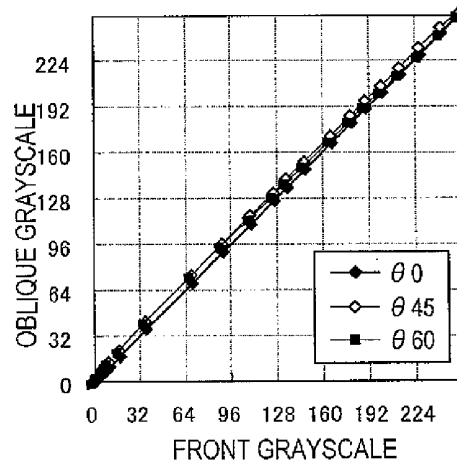
(a)

RIGHTWARD AND LEFTWARD DIRECTIONS



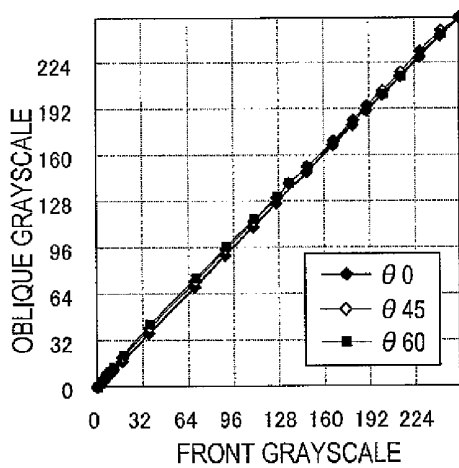
(b)

UPWARD AND DOWNWARD DIRECTIONS



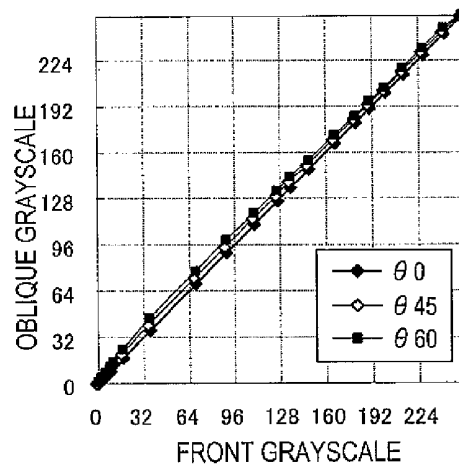
(c)

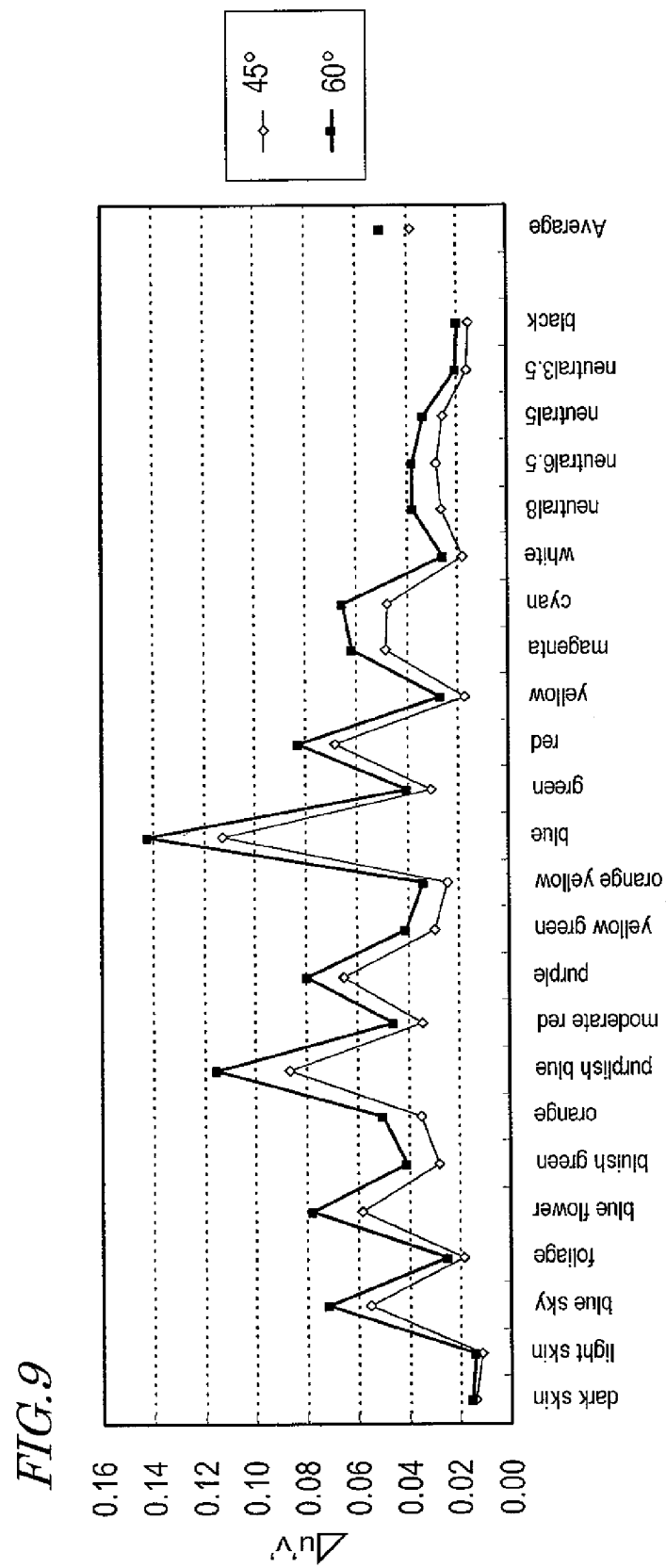
DIAGONAL 45° DIRECTION



(d)

DIAGONAL 135° DIRECTION





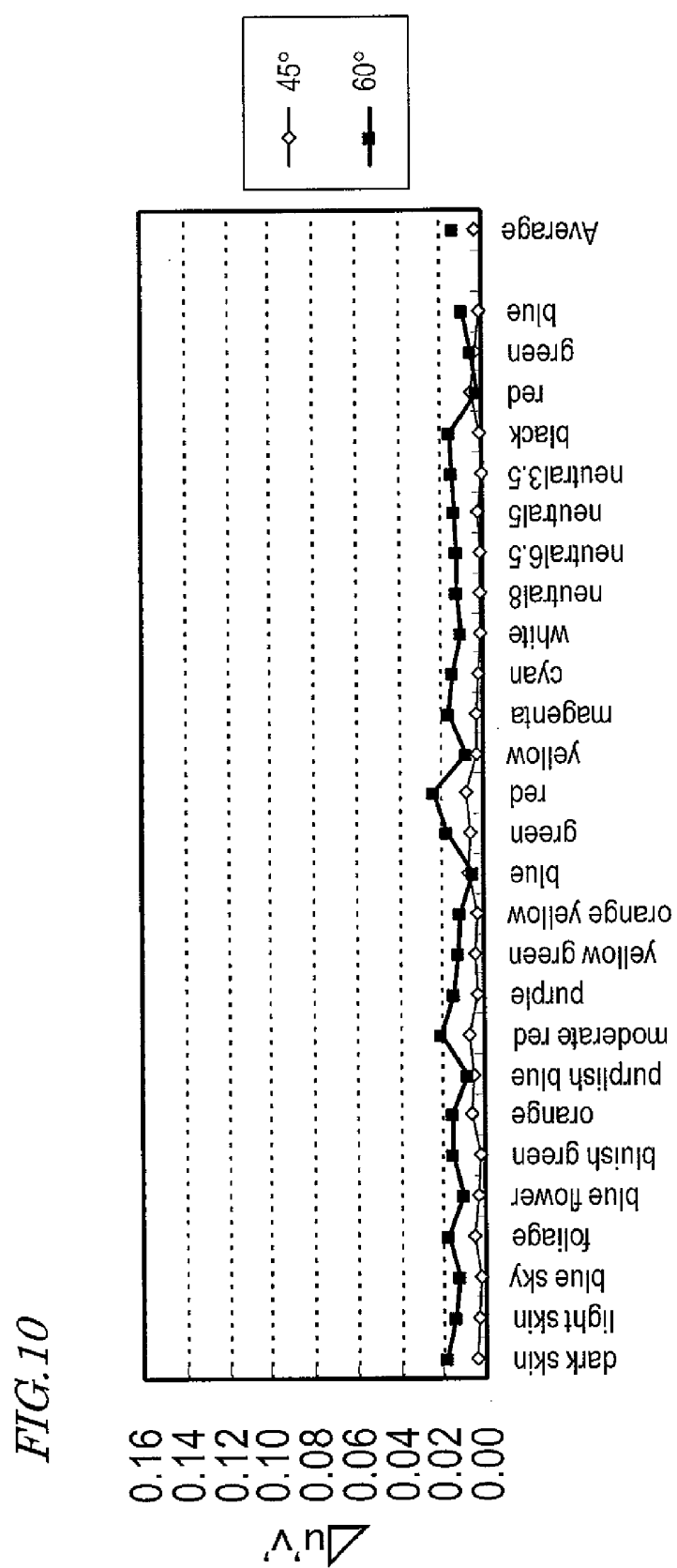
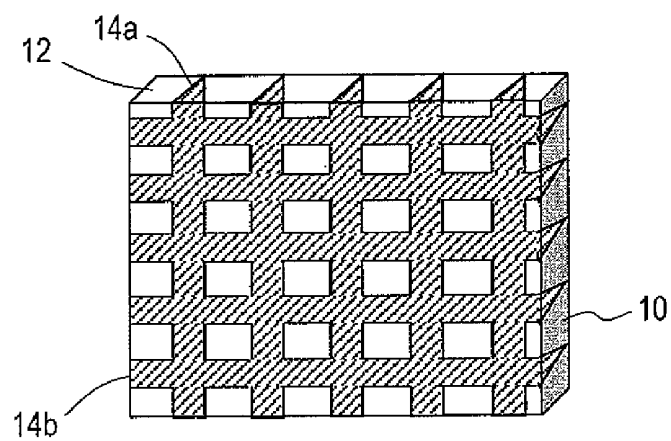


FIG. 11

(a)



(b)

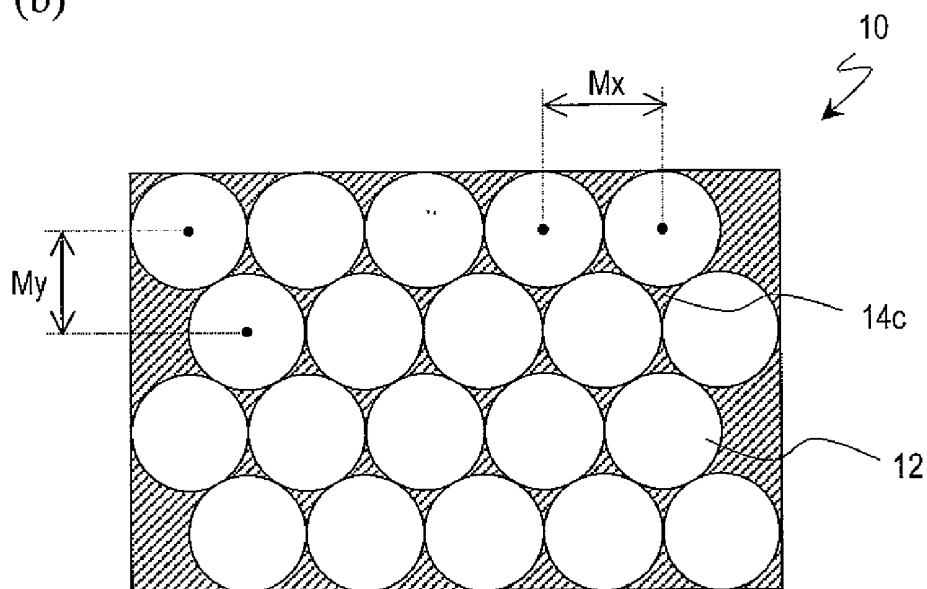


FIG. 12

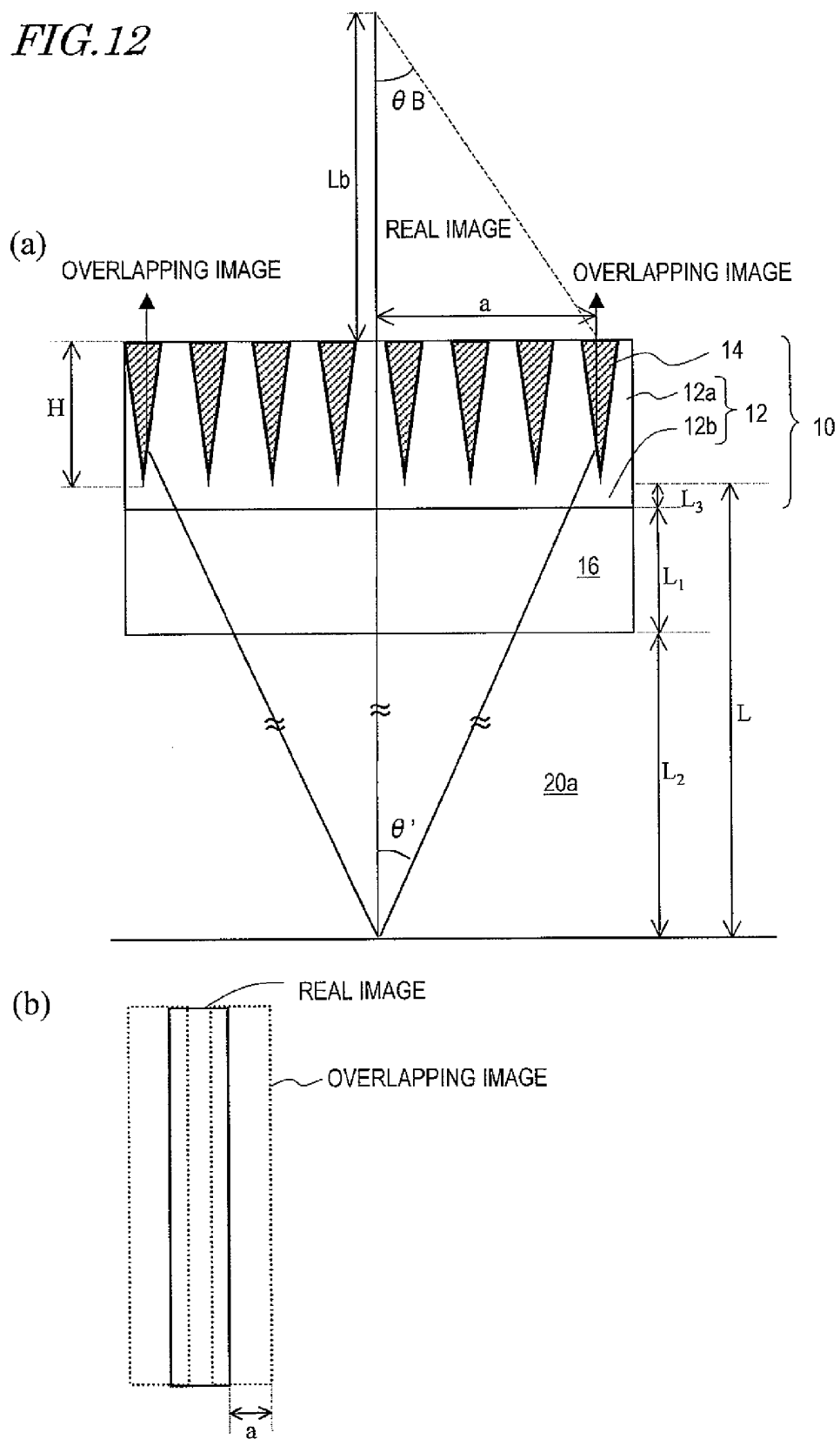


FIG. 13

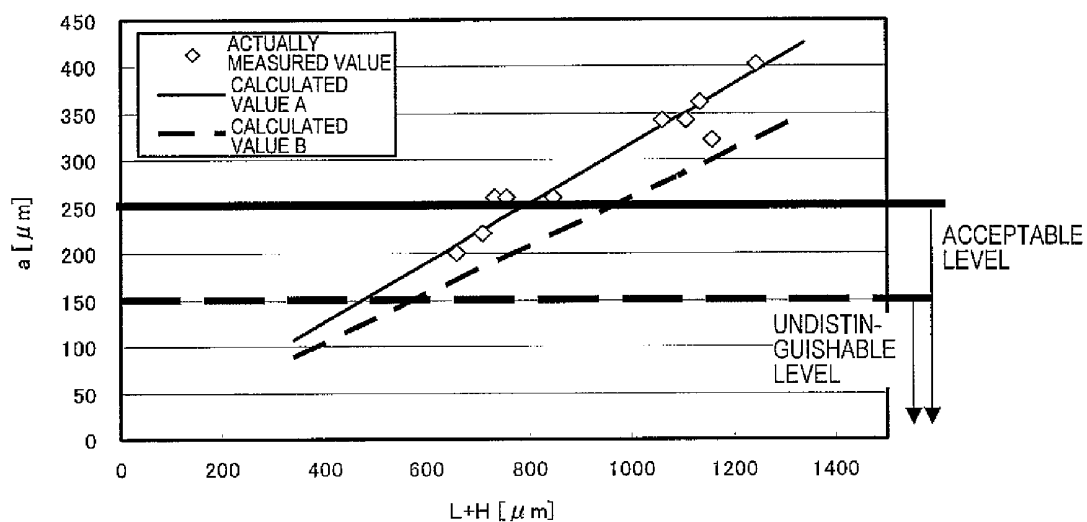


FIG. 14

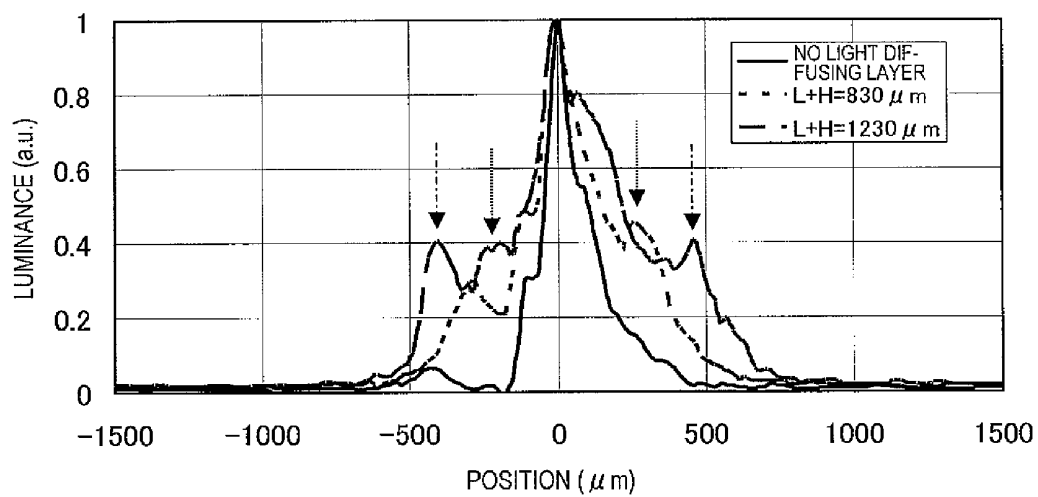
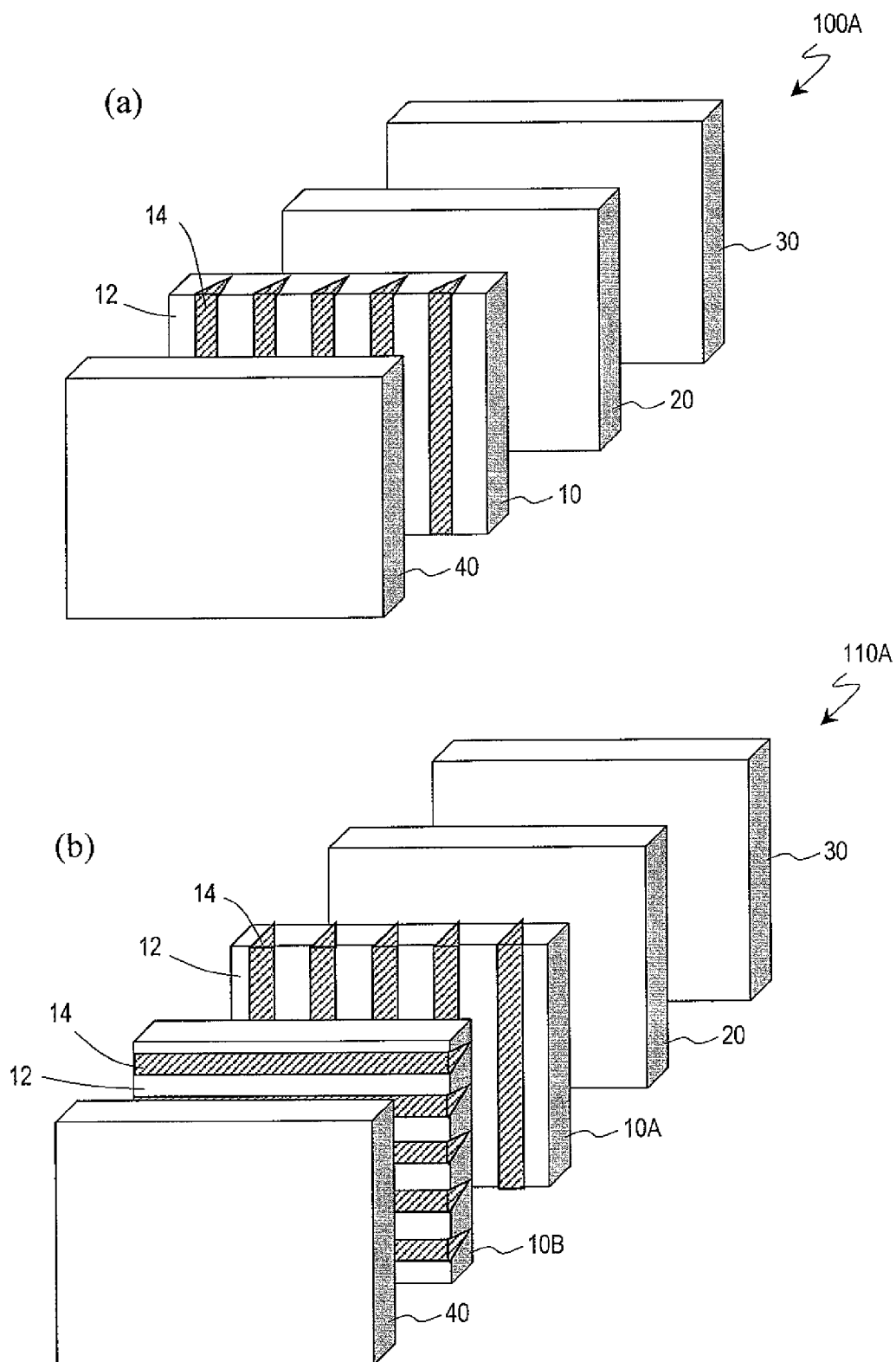


FIG. 15

LIQUID CRYSTAL DISPLAY DEVICE

TECHNICAL FIELD

The present invention relates to a liquid crystal display device and specifically to a direct-viewing type liquid crystal display device which has a light diffusing layer on the viewer side of a liquid crystal display panel.

BACKGROUND ART

Liquid crystal display devices are not self-emitting display devices and, therefore, almost all of them, excluding some reflection-type display devices, require a backside illuminator (so called "backlight unit") for supplying light for display to the liquid crystal display panel. The backlight units, which are to be provided on the backside of the liquid crystal display panel (opposite to the viewer side), are generally classified into edge light type backlights and direct lighting type backlights. The edge light type is a class of backlights in which light emitted by a light source (CCFT (Cold Cathode Fluorescent Tube) or LED) placed on a side face of a light guide plate is allowed to propagate in the light guide plate and to outgo toward the liquid crystal display panel side. The direct lighting type backlights are configured such that a plurality of light sources are arranged on the back surface of a liquid crystal display panel, and light emitted by the light sources enters the liquid crystal display panel without passing through a light guide plate.

The liquid crystal display devices have a problem that the appearance of display varies depending on the viewing direction, i.e., a problem that the viewing angle characteristics degrade depending on the viewing direction. This results from the fact that the liquid crystal layer has anisotropy in refractive index so that the effective phase difference (retardation) of the liquid crystal layer varies depending on the viewing direction.

One of the known methods for improving the viewing angle characteristics of liquid crystal display devices is controlling the directivity (degree of parallelism) of light from the backlight such that rays which do not adversely affect the viewing angle characteristics are mainly allowed to enter the liquid crystal display panel and omniazimuthally diffusing the rays transmitted through the liquid crystal display panel by means of a microlens or microlens array (e.g., Patent Document 1).

[Patent Document 1] Japanese Laid-Open Patent Publication No. H9-127309

[Patent Document 2] Japanese Laid-Open Patent Publication No. 2003-50307

[Patent Document 3] Japanese Laid-Open Patent Publication No. H11-242225

DISCLOSURE OF INVENTION

Problems to be Solved by the Invention

However, when the above-described microlens is used, in any of a microlens which has a concave/convex pattern in its outer surface and a microlens which has a refractive index distribution of a predetermined shape in a planer layer (sometimes called "planer microlens"), there are difficulty in controlling the shape of the lens, difficulty in precisely controlling the ratio between the thickness of a convex portion of the lens and the thickness of an adhesive layer, and/or difficulty in controlling the distribution of light beams with high accuracy. Especially, a lens which has a concave/convex pattern in its

outer surface is difficult to uniformly adhere to a display panel with high accuracy, and also has a problem that the lens characteristics vary depending on the size and shape of part of the lens which is buried in the adhesive layer. Therefore, the lens of this type has not been put to practice. Also, there is a problem that rearward scattering at the interface of the lens shape cannot be eliminated.

On the other hand, a light diffusion sheet which utilizes total reflection has been known (Patent Document 2). The light diffusion sheet disclosed in Patent Document 2 is a diffusion sheet for use in a rear projection type display device. This diffusion sheet is configured to diffuse highly-collimated image light that comes out of a display panel.

The present inventor examined, with the view of widening the viewing angle of a direct-viewing type liquid crystal display device, a configuration in which a light diffusing layer that utilizes total reflection is provided on the viewer side of a direct-viewing type liquid crystal display panel, and found a problem that an overlapping image and a local chromaticity change (a blue shift in chromaticity at a certain polar angle) in the polar angle dependence of the viewing angle characteristics are visually perceived. This problem is specific to a case where the light diffusing layer is applied to the direct-viewing type. Note that the "light diffusing layer which utilizes total reflection" does not mean that the light diffusing layer utilizes only total reflection but that the light diffusing layer utilizes at least total reflection. Light used for display includes total reflection and other types of reflections.

The present invention was conceived for the purpose of solving the above problems. One of the major objects of the invention is to improve the viewing angle characteristics of direct-viewing type liquid crystal display devices by using a light diffusing layer which utilizes total reflection.

Means for Solving the Problems

A liquid crystal display device of the present invention includes: a liquid crystal display panel which has a pair of polarizing plates; and a first light diffusing layer which has a first major surface and a second major surface opposing each other and which is arranged such that the first major surface opposes a viewer side surface of the liquid crystal display panel, wherein the first light diffusing layer includes a first region formed of a first substance which has a first refractive index N_1 and a plurality of second regions formed of a second substance which has a second refractive index N_2 , the second refractive index N_2 being smaller than the first refractive index N_1 , the plurality of second regions are arranged in the first region at a predetermined pitch P in one direction in a plane parallel to the second major surface, each of the plurality of second regions forms a plurality of interfaces with the first region, the interfaces being inclined by α° from a normal of the second major surface, and θ_B shown below is not more than 1.7 arc minutes

$$\theta_B = \tan^{-1} \left(\frac{a}{Lb} \right)$$

where Lb is a typical viewing distance of the liquid crystal display panel, and a is expressed as follows:

$$a = \tan \theta' \times Lt$$

in which Lt is a distance from the second major surface to a liquid crystal layer side surface of a viewer side substrate of the liquid crystal display panel, and θ' is expressed as follows:

$$\theta' = 90 - \sin^{-1}\left(\frac{N_2}{N_1} \times \cos\alpha\right) - \alpha.$$

More preferably, θ_B is not more than 1.0 arc minute.

In one embodiment, each of the second regions is approximated to an isosceles triangle where a base is on the second major surface side, a vertex is on the first major surface side, and a vertex angle is 2α .

In one embodiment, formulae shown below are met:

$$H \leq \frac{P}{\tan 2\alpha + \tan \alpha} \text{ and } \cos[\alpha(2n-1)] > \frac{N_2}{N_1}$$

where H is a height of the isosceles triangle, and n is an integer not less than 2.

In one embodiment, the plurality of second regions of the first light diffusing layer are arranged in a stripe pattern along a horizontal direction of the liquid crystal display panel.

In one embodiment, the liquid crystal display device further includes a light scattering layer on a viewer side of the first light diffusing layer.

In one embodiment, the liquid crystal display device further includes a second light diffusing layer on a viewer side of the first light diffusing layer, wherein the second light diffusing layer includes a first region formed of a first substance which has a first refractive index N_1 and a plurality of second regions formed of a second substance which has a second refractive index N_2 , the second refractive index N_2 being smaller than the first refractive index N_1 , the plurality of second regions are arranged in the first region at a predetermined pitch P in one direction in a plane parallel to the second major surface, and each of the plurality of second regions forms a plurality of interfaces with the first region, the interfaces being inclined by α° from a normal of the second major surface.

In one embodiment, each of the second regions is approximated to an isosceles triangle where a base is on the second major surface side, a vertex is on the first major surface side, and a vertex angle is 2α .

In one embodiment, formulae shown below are met:

$$H' \leq \frac{P}{\tan 2\alpha' + \tan \alpha'} \text{ and } \cos[\alpha'(2n'-1)] > \frac{N_2}{N_1}$$

where H' is a height of the isosceles triangle, and n' is an integer not less than 2.

In one embodiment, the plurality of second regions of the first light diffusing layer are arranged in a stripe pattern along a horizontal direction of the liquid crystal display panel, and the plurality of second regions of the second light diffusing layer are arranged in a stripe pattern along a vertical direction of the liquid crystal display panel.

In one embodiment, the liquid crystal display device further includes a light scattering layer on a viewer side of the second light diffusing layer.

In one embodiment, when the first light diffusing layer is viewed in a direction perpendicular to the second major surface, the plurality of first regions each have a generally circular shape and are arranged in a square grating arrangement or a closest packed arrangement.

In one embodiment, a difference between a maximum and a minimum of N_1/N_2 in a wavelength range from 400 nm to 800 nm is not more than 0.02 of an average of N_1/N_2 in the wavelength range.

In one embodiment, the second regions further include a substance which absorbs visible light.

In one embodiment, the predetermined pitch P is not more than three quarters of a pixel pitch in the direction.

Effects of the Invention

According to the present invention, the viewing angle characteristics of a direct-viewing type liquid crystal display device can be improved by using a light diffusing layer (light diffusion sheet) which utilizes total reflection. In a liquid crystal display device of the present invention, overlapping images which may be generated due to the light diffusing layer are unlikely to be visually perceived. According to the present invention, the viewing angle characteristics can be improved only by placing the light diffusing layer at a predetermined position on the viewer side of the liquid crystal display panel. The present invention is applicable to any type of known liquid crystal display panels. For example, the present invention is applicable not only to TN mode liquid crystal display panels which have inferior viewing angle characteristics but also to VA mode liquid crystal display panels which have superior viewing angle characteristics. Further, the present invention is also applicable to a liquid crystal display panel which has an alignment-divided structure wherein a pixel includes liquid crystal domains of different alignment directions and/or a pixel-divided (multi pixel) structure wherein a pixel includes regions of different luminances.

BRIEF DESCRIPTION OF DRAWINGS

FIG. 1 A schematic exploded cross-sectional view of a liquid crystal display device 100 of an embodiment of the present invention.

FIG. 2 A schematic exploded perspective view of the liquid crystal display device 100 of an embodiment of the present invention.

FIG. 3 A schematic exploded perspective view of another liquid crystal display device 110 of an embodiment of the present invention.

FIG. 4 A diagram for illustrating the structure and functions of a light diffusing layer 10.

FIGS. 5 (a) and (b) are graphs showing the diffusion characteristics of light outgoing from different light diffusing layers. (a) corresponds to a case where the half-value angle $\Delta\theta_{50}$ of light emitted from the backlight unit is $\pm 10^\circ$. (b) corresponds to a case where the half-value angle $\Delta\theta_{50}$ of light emitted from the backlight unit is $\pm 35^\circ$.

FIG. 6 (a) to (d) are graphs showing the viewing angle dependence of the γ characteristic of a conventional MVA mode liquid crystal display device.

FIG. 7 (a) to (d) are graphs showing the viewing angle dependence of the γ characteristic of an MVA mode liquid crystal display device of an embodiment of the present invention.

FIG. 8 (a) to (d) are graphs showing the viewing angle dependence of the γ characteristic of another MVA mode liquid crystal display device of an embodiment of the present invention.

FIG. 9 A graph showing the color difference in a conventional liquid crystal display device.

FIG. 10 A graph showing the color difference in a liquid crystal display device of an embodiment of the present invention.

FIGS. 11 (a) and (b) are diagrams showing other light diffusing layers of the present invention. (a) is a perspective view of another light diffusing layer. (b) is a front view of still another light diffusing layer.

FIGS. 12 (a) and (b) are diagrams for illustrating overlapping images which can be visually perceived when a light diffusing layer of an embodiment of the present invention is used. (a) is a schematic cross-sectional view. (b) is a schematic plan view.

FIG. 13 A graph showing the thickness (L+H) dependence of position a where an overlapping image occurs, which was experimentally obtained.

FIG. 14 A graph showing an example of line profiles which represent actual measurement results of overlapping images.

FIGS. 15 (a) and (b) are schematic exploded perspective views of other liquid crystal display devices 100A and 110A of embodiments of the present invention.

DESCRIPTION OF THE REFERENCE NUMERALS

- 10, 10A, 10B light diffusion sheet, light diffusing layer (total reflection diffusing layer)
- 12, 12a, 12b high refractive index region (first region)
- 12s interface (total reflection surface)
- 14 low refractive index region (second region)
- 20 MVA mode liquid crystal display panel
- 20a glass substrate on viewer side
- 30 backlight unit
- 40 light scattering layer (diffuse reflection layer)
- 100, 110, 100A, 110A liquid crystal display device
- 302a perpendicular incident light
- 302b light outgoing after having been totally reflected only once (perpendicular incident light)
- 304a, 306a oblique incident light
- 304b light outgoing after having been totally reflected twice (part of oblique incident light)
- 306b light outgoing after having been totally reflected only once (part of oblique incident light)

BEST MODE FOR CARRYING OUT THE INVENTION

Hereinafter, a liquid crystal display device which includes a light diffusion sheet according to an embodiment of the present invention is described as to the structure and properties with reference to the drawings. The liquid crystal display device of the present invention may be a direct-viewing type liquid crystal display device wherein light outgoing from a display surface is directly viewed by a viewer.

A light diffusion sheet 10 and a liquid crystal display device 100 which includes the light diffusing sheet 10 according to an embodiment of the present invention are described as to the structures and properties with reference to FIG. 1 and FIG. 2. FIG. 1 is a schematic exploded cross-sectional view of the liquid crystal display device 100. FIG. 2 is a schematic exploded perspective view of the liquid crystal display device 100.

The example described herein is a VA mode liquid crystal display device. The VA mode liquid crystal display device which uses a vertical alignment type liquid crystal layer has improved viewing angle characteristics as compared with the conventional TN mode. The vertical alignment type liquid crystal layer includes vertical alignment films by which the pretilt angle of liquid crystal molecules in the absence of an applied voltage is regulated to be not less than 85° and not more than 90°, and a nematic liquid crystal material whose

dielectric anisotropy is negative. Among the VA mode liquid crystal display devices, especially, a MVA mode liquid crystal display device described in Patent Document 3 has excellent viewing angle characteristics and therefore has been used in a wide variety of applications. In the MVA mode, alignment control means (slit or rib) which has linear portions extending in two directions perpendicular to each other is provided to form four liquid crystal domains between the alignment control means such that the azimuthal angles of the directors which are representative of the respective domains form angles of 45° relative to the polarization axes (transmission axes) of polarizing plates placed in crossed Nicols. Assuming that the azimuthal angle of 0° is identical with the 3 o'clock direction of the clock dial and that the counterclockwise direction is the positive direction, the azimuthal angles of the directors of the four domains are 45°, 135°, 225°, and 315°. This configuration is most preferable in terms of transmittance because linear polarization in the 45° direction relative to the polarization axes is not absorbed by the polarizing plates. The MVA mode liquid crystal display device has such a configuration in which four domains are formed in one pixel ("4-domain alignment structure" or simply "4D structure") and therefore has improved viewing angle characteristics. However, further improvements in the viewing angle characteristics of the γ characteristic have also been demanded of the MVA mode liquid crystal display device. In the embodiment provided below, an example where the viewing angle characteristics of the γ characteristic of the MVA mode liquid crystal display device are further improved by providing a light diffusing layer is described.

The liquid crystal display device 100 includes the light diffusion sheet 10, a liquid crystal display panel 20, and a backlight unit 30. In an example described herein, the liquid crystal display panel 20 is an MVA mode liquid crystal display panel which includes a phase plate. The entire disclosures of Patent Document 3 are incorporated by reference in this specification. Also, the phase plate used herein may be a known phase plate which is appropriately selected.

The light diffusion sheet 10 includes one light diffusing layer 10 which has a first major surface and a second major surface opposing each other and which is arranged such that the first major surface opposes the viewer side surface of the VA mode liquid crystal display panel. A base film (not shown) may be provided on a side of the light diffusing layer 10 which is closer to the liquid crystal display panel 20 (light incoming side), although the light diffusion sheet 10 is formed only by one light diffusing layer 10 in the example described herein. The viewer side (light outgoing side) of the light diffusing layer 10 may be provided with an antiglare layer, an antireflection layer, a low reflection layer, or a reflection preventing layer (although none of these is shown). As a matter of course, any two or more of these elements may be used in combination when necessary. The light diffusion sheet 10 and the liquid crystal display panel 20 are bonded together via an adhesive layer (not shown). The both outermost surfaces of the liquid crystal display panel 20 are generally provided with polarizing plates, and therefore, the light diffusion sheet is bonded to the polarizing plate on the viewer side. Here, a structure obtained by bonding the light diffusion sheet 10 to the liquid crystal display panel 20 (which does not include the backlight unit 30) is sometimes referred to as a liquid crystal display device.

The light diffusing layer 10 includes the first substance having first refractive index N_1 and the second substance having second refractive index N_2 . Second refractive index N_2 is smaller than first refractive index N_1 . The second substance forms a plurality of second regions (low refractive

index regions **14**. The shape of each of the second regions **14** in a cross section perpendicular to the second major surface is approximated to an isosceles triangle where the base is on the second major surface side and the vertex is on the first major surface side. The plurality of second regions **14** are arranged in a first region (high refractive index region) **12** formed of the first substance at predetermined pitch P in at least one direction in a plane parallel to the second major surface. Light which comes from the high refractive index region side and is incident on interfaces **12s** between the high refractive index region **12** and the low refractive index regions **14** at an angle not smaller than a critical angle is totally reflected.

Since the isosceles triangle of the low refractive regions of the light diffusing layer **10** described herein meets predetermined conditions as will be described later with reference to FIG. 4, light **302a** which is incident perpendicularly onto the major surface of the light diffusing layer **10** (the absolute value of the angle of incidence is not less than 0° and less than 0.1°) undergoes total reflection only once inside the light diffusing layer **10** before outgoing from the light diffusing layer **10** toward the viewer side (outgoing light **302b**). Part of light which is incident on the major surface at an oblique angle (the absolute value of the angle of incidence is 0.1° or greater), **304a**, undergoes total reflection n or more times (n is an integer not less than 2, $n=2$ in FIG. 1) inside the light diffusing layer **10** before outgoing from the light diffusing layer toward the viewer side (outgoing light **304b**). Another part of the light which is incident on the major surface at an oblique angle (the absolute value of the angle of incidence is 0.1° or greater), **306a**, undergoes total reflection only once inside the light diffusing layer **10** before outgoing from the light diffusing layer **10** toward the viewer side (outgoing light **306b**). As a result, the viewing angle characteristics in the at least one direction (polar angle (θ) dependence in an azimuthal angle defined by the at least one direction) is improved. In this way, the light diffusing layer **10** diffuses light by utilizing total reflection and is therefore sometimes referred to as "total reflection diffusing layer". Note that the light utilized for display is not limited to totally reflected light.

The light diffusing layer utilizes total reflection and is therefore less affected by the shape as compared with a case where a refraction effect of a lens is utilized. Further, the low refractive index regions have a simple shape which is approximated to an isosceles triangle and are therefore advantageous in terms of easiness of fabrication. Further, the major surfaces (surfaces) of the light diffusing layer which oppose each other are parallel to each other and can be readily bonded onto the surface of the liquid crystal display panel. The surface which is to be bonded onto the liquid crystal display panel is formed only by the high refractive index region. Therefore, the total reflection characteristics inside the light diffusing layer are not affected at all by the bonding.

Here, as shown in FIG. 2, when viewed in a direction perpendicular to the major surfaces of the light diffusing layer **10**, each of the plurality of second regions **14** has the shape of a vertically-extending rectangle. The plurality of second regions **14** are arranged in a stripe pattern along a horizontal direction. FIG. 1 corresponds to a horizontal cross-section of FIG. 2. As seen from FIG. 1, the light diffusing layer **10** is capable of improving the viewing angle characteristics in the horizontal directions (i.e., the polar angle (θ) dependence in the horizontal directions). In many of the MVA type liquid crystal display panels **20** although it depends on the purpose of use, when describing with an imaginary clock dial superposed on the display surface, the azimuthal angles of the directors of the four domains are set to 45° , 135° , 225° , and

315° , and the polarization axis (transmission axis) of one of a pair of polarizing plates in a crossed Nicols arrangement is generally parallel to the vertical directions (12 o'clock and 6 o'clock directions) of the display surface, the polarization axis of the other being generally parallel to the horizontal directions (3 o'clock and 9 o'clock directions). In the liquid crystal display devices, the required viewing angle characteristics vary depending on the purpose of use. Therefore, by providing the light diffusing layer **10** that includes the plurality of rectangular second regions **14** that extend perpendicular to a direction in which a wide viewing angle characteristic is required and that are arranged along the direction in which a wide viewing angle characteristic is required, the viewing angle characteristics can be effectively improved. In general, the viewing angle characteristics in the horizontal directions are of greater importance. Using a light diffusing layer shown in FIG. 2 which includes a plurality of vertically-extending rectangular second regions **14** that are arranged along a horizontal direction is effective.

Note that, as in a liquid crystal display device **110** whose schematic exploded perspective view is shown in FIG. 3, light diffusing layers **10A** and **10B** may be provided. Here, the light diffusing layer **10A** is the same as the light diffusing layer **10** of the liquid crystal display device **100**. The light diffusing layer **10B** includes a plurality of horizontally-extending rectangular second regions **14** which are arranged in a stripe pattern along a vertical direction. By additionally providing the light diffusing layer **10B** in this way, the viewing angle characteristics in the vertical directions can be improved. As a matter of course, with the view of mainly improving the viewing angle characteristics in the vertical directions, only the light diffusing layer **10B** may be provided while omitting the light diffusing layer **10A**.

Next, the structure and functions of the light diffusing layer **10** are described in detail with reference to FIG. 4. In the following description, for the sake of simplicity, the major surfaces of the liquid crystal display panel **20** and the major surfaces of the light diffusing layer **10** are parallel. Refraction of light which would occur at the interface between these elements and at the interfaces with an adhesive layer (not shown) for bonding these elements is ignored. Note that the description below generally holds true even when such refraction is considered.

Here, as shown in FIG. 4, the pitch of the low refractive index regions **14** is denoted by 2 , the height of the isosceles triangle is denoted by H , and the vertex angle of the isosceles triangle is denoted by 2α . Light **302a** which is incident perpendicularly onto the light diffusing layer **10** ($\Delta\theta=0$ in FIG. 4) undergoes total reflection only once. Therefore, when considering the most strict design conditions, the condition that light totally reflected at the vertex of a low refractive index region **14** outgo from the surface of the light diffusing layer **10** without entering a neighboring low refractive index region **14** (outgoing light **302b**) is necessary. Thus, the following formula holds:

$$H \leq \frac{P}{\tan 2\alpha + \tan \alpha} \quad (1)$$

Also, the condition that light incident on the light diffusing layer **10** in an oblique direction ($|\Delta\theta|>0^\circ$) undergo total reflection once, which is shown below, need to be met (see the incident light **306a** and the outgoing light **306b** in FIG. 1):

$$N_1 \cos \left\{ \sin^{-1} \left(\frac{\sin \Delta \theta}{N_1} \right) + \alpha \right\} > N_2 \quad (2)$$

In order that part of the light incident on the light diffusing layer **10** in an oblique direction ($|\Delta \theta| > 0^\circ$), **304a**, may undergo total reflection twice before outgoing from the light diffusing layer **10** (outgoing light **304b**), θ_2 need to meet the condition that total reflection occur at the interfaces **12s**. θ_2 is given as follows:

$$\theta_2 = \sin^{-1} \left(\frac{\sin \Delta \theta}{N_1} \right) + 2\alpha \quad (3)$$

Therefore, due to the Snell's law, the total reflection condition at the interfaces **12s** between the high refractive index region (first region: N_1) **12** and the low refractive index regions (second regions: N_2) **14** is as follows:

$$N_1 \sin(90^\circ - \theta_2 - \alpha) = N_2 \cos(\theta_2 + \alpha) > N_2 \quad (4)$$

This formula is transformed by replacing θ_2 as follows:

$$N_1 \cos \left\{ \sin^{-1} \left(\frac{\sin \Delta \theta}{N_1} \right) + 3\alpha \right\} > N_2 \quad (5)$$

Actually, in formula (5), the light which undergoes total reflection twice is not collimated light ($\Delta \theta = 0^\circ$ does not hold) but light that is incident at an angle in a region of $\Delta \theta$ which is extremely close to collimated light. Therefore, the following relationship can be deduced:

$$\lim_{\Delta \theta \rightarrow 0} N_1 \cos \left\{ \sin^{-1} \left(\frac{\sin \Delta \theta}{N_1} \right) + 3\alpha \right\} = N_1 \cos(3\alpha) > N_2 \quad (6)$$

$$\therefore \cos(3\alpha) > \frac{N_2}{N_1}$$

As such, to design the light diffusing layer (total reflection diffusing layer) **10** such that light perpendicularly coming in the liquid crystal display panel ($\Delta \theta = 0$) undergoes total reflection only once and part of the light coming in the liquid crystal display panel in an oblique direction ($|\Delta \theta| > 0$) undergoes total reflection twice under the circumstance where the backlight unit used has the half-value angle $\Delta \theta_{50}$ in the case of a certain directivity, the light diffusing layer may be designed so as to meet above formulae (1) and (6). By doing so, not only the once-totally-reflected light of the oblique light but also the twice-totally-reflected light can efficiently be utilized, so that wide viewing angle characteristics are achieved.

In a case where part of the oblique incident light is allowed to undergo total reflection n or more times ($n \geq 2$), above formula (6) can be expanded to the following formula:

$$\cos[\alpha(2n-1)] > \frac{N_2}{N_1} \quad (n \text{ is an integer not less than } 2) \quad (7)$$

Therefore, in a case where part of the oblique incident light is allowed to undergo total reflection n or more times, the light diffusing layer is designed so as to meet formulae (1) and (7).

Also, as a matter of course, it is necessary to meet the condition that light should not finally undergo total reflection

but be refracted at the interface between the high refractive index region **12** (refractive index N_1) and the air so as to outgo from the high refractive index region **12**. Therefore, as for light which undergoes total reflection n times at the interfaces **12s** between the high refractive index region **12** and the low refractive index regions **14**, it is necessary to meet the following formula:

$$N_1 \sin \left\{ \sin^{-1} \left(\frac{\sin \Delta \theta}{N_1} \right) + 2n\alpha \right\} < 1 \quad (8)$$

(total reflection n times, n is an integer not less than 1)

Under the circumstance where formula (1) and formula (6) or formula (1) and formula (7) are met, the maximum intensity in the intensity distribution of light emitted from the backlight unit **30** is assumed to be 100%, and the angles at which the intensity is 10% are denoted by $\pm \Delta \theta_{10}$. Designing the light diffusing layer such that $\pm \Delta \theta_{10}$ meets formula (1) and formula (6) or formula (1) and formula (7) is preferable because light transmitted through and outgoing from the liquid crystal display panel **20** can be utilized efficiently (90% or more) in the light diffusing layer **10**. In this case, the means for condensing the light emitted from the backlight **30** may be selected from a wide variety of known optical elements. For example, a prism sheet, an integral structure of a prism sheet and a diffuse reflection plate (light scattering plate), a lover, or a reversed prism may be used. Note that, in the present specification, when such an element is added, a unit including the added element is referred to as "backlight unit".

Note that the directivity of the light emitted from the backlight unit does not necessarily need to be set such that the above-described conditions are met. The viewing angle characteristics are not affected so long as light incident at an angle which does not meet the above-described conditions is absorbed by the low refractive index regions **14** as will be described later.

Next, the difference in light diffusion characteristic among the cases where light diffusing layers characterized by the following three parameter sets A, B, and C (respectively referred to as "light diffusing layers A, B, and C") are used is described with reference to FIG. 5. The light diffusing layer A meets the above-described conditions whereas the light diffusing layers B and C do not meet the above-described conditions.

A: $N_1=1.55$, $N_2=1.40$, $\alpha=8.0^\circ$, $P=50 \mu\text{m}$, $H=110 \mu\text{m}$

B: $N_1=1.55$, $N_2=1.50$, $\alpha=8.0^\circ$, $P=50 \mu\text{m}$, $H=110 \mu\text{m}$

C: $N_1=1.55$, $N_2=1.50$, $\alpha=6.0^\circ$, $P=50 \mu\text{m}$, $H=155 \mu\text{m}$

FIG. 5(a) shows the diffusion characteristic of light outgoing from the light diffusing layer **10** under the circumstance where light having the directivity of half-value angle $\Delta \theta_{50} = \pm 10^\circ$ comes from the backlight unit and enters the light diffusing layers A and B. The diffusion characteristic shown herein is the polar angle dependence of the outgoing light intensity in a direction in which the low refractive index regions **14** are arranged at a predetermined pitch, and corresponds to the viewing angle characteristics of the liquid crystal display device. It is seen that the light diffusing layer A can efficiently utilize the light which has undergone total reflection twice inside the light diffusing layer and, as a result, the intensity distribution of the outgoing light extends over a wide angle range as compared with the light diffusing layer B.

However, the intensity distribution of the outgoing light of the light diffusing layer A of FIG. 5(a) shows prominent peaks of the once-totally-reflected light and prominent peaks of the twice-totally-reflected light. These peaks may cause the

viewer to feel a sense of discontinuity in the viewing angle characteristics. Thus, to prevent this, decreasing the directivity of light which comes in the light diffusing layer, i.e., increasing the half-value angle $\Delta\theta_{50}$, is preferable. FIG. 5(b) shows a result of the diffusion characteristics under the circumstance where the half-value angle $\Delta\theta_{50}$ of the light emitted from the backlight unit is $\pm 35^\circ$. As seen from FIG. 5(b), the intensity distribution of the outgoing light of the light diffusing layer A which meets the above-described conditions is wider than those of the light diffusing layers B and C, and does not have a prominent peak such as those seen in FIG. 5(a). Thus, it is possible to prevent the viewer from feeling a sense of discontinuity in the viewing angle characteristics.

Next, the viewing angle dependence (polar angle dependence) of the γ characteristic of a conventional MVA mode liquid crystal display device and a MVA mode liquid crystal display device of an embodiment of the present invention is described with reference to FIG. 6, FIG. 7, and FIG. 8. In the graphs of FIG. 6 to FIG. 8, the abscissa axis represents the grayscale levels which are intended to be displayed (input grayscale levels, from level 0 to level 255). The ordinate axis represents the grayscale levels which are actually displayed. Any of these liquid crystal display devices is configured such that the curve of $\gamma=2.2$ is obtained when viewed from a position in front of the display device.

FIGS. 6(a) to 6(d) are graphs showing the viewing angle dependence of the γ characteristic of the conventional MVA mode liquid crystal display device. This conventional liquid crystal display device includes a phase plate. FIGS. 7(a) to 7(d) are graphs showing the viewing angle dependence of the γ characteristic of an MVA mode liquid crystal display device of an embodiment of the present invention, which includes only one light diffusing layer 10 that meets the above-described conditions in addition to the components of the conventional MVA type liquid crystal display device that has the viewing angle characteristics of FIGS. 6(a) to 6(d). This liquid crystal display device has the same structure as that of the liquid crystal display device 100 shown in FIG. 2. FIGS. 8(a) to 8(d) are graphs showing the viewing angle dependence of the γ characteristic of a MVA mode liquid crystal display device of an embodiment of the present invention, which includes two light diffusing layers 10 that meet the above-described conditions in addition to the components of the conventional MVA type liquid crystal display device that has the viewing angle characteristics of FIGS. 6(a) to 6(d). This liquid crystal display device has the same structure as that of the liquid crystal display device 110 shown in FIG. 3. In each of FIG. 6, FIG. 7, and FIG. 8, (a) shows the polar angle θ dependence in the rightward and leftward directions, (b) in the upward and downward directions, (c) in the 45° direction, and (d) in the 135° direction. As for the azimuthal angle, 3 o'clock direction corresponds to 0° , and the counterclockwise direction is the positive direction.

As seen from FIG. 6(a), in the conventional liquid crystal display device, whitening (a phenomenon that the state of display is at a higher luminance than that originally intended) becomes more conspicuous as the polar angle θ increases in any of the azimuthal angle directions. This tendency is most noticeable in the upward and downward (vertical) directions and second most noticeable in the rightward and leftward (horizontal) directions. Although not shown, when the retardation of the liquid crystal layer is large, grayscale inversion (a phenomenon that the luminance decreases as the grayscale level increases) occurs in a range near the highest grayscale level.

On the other hand, referring to FIGS. 7(a) to 7(d), it is seen that, in the liquid crystal display device of the embodiment of

the present invention, the viewing angle characteristics in the rightward and leftward directions are significantly improved. Specifically, in the light diffusing layer 10 included in this liquid crystal display device (see FIG. 2), the low refractive index regions 14 are extending in the vertical direction, and the viewing angle characteristics in the horizontal (rightward and leftward) directions that are perpendicular to the direction in which the low refractive index regions 14 are extending are significantly improved. In the example described herein, the above parameters of the light diffusing layer are $N_1=1.59$, $N_2=1.40$, $\alpha=8.0^\circ$, $P=50\text{ }\mu\text{m}$, and $H=110\text{ }\mu\text{m}$. Specifically, according to the embodiment of the present invention, the whitening in the rightward and leftward directions is greatly ameliorated, and the grayscale characteristics in diagonal directions (polar angle $>0^\circ$) also reach a value which is close to $\gamma=2.2$. Note that the light diffusing layer of the liquid crystal display device of this embodiment includes a plurality of low refractive index regions which are extending in the vertical direction and which are arranged in the horizontal direction such that the direction of arrangement is inclined by $\pm 1^\circ$ or more relative to the bus line. The direction of the inclination may be clockwise or may be counterclockwise. In the example described herein, the inclination is counterclockwise. This inclination produces the effect of preventing moiré which will be described later and also produces the effect of improving the viewing angle characteristic in the 45° direction as shown in FIG. 7(c).

Referring to FIGS. 8(a) to 8(d), it is seen that, in the liquid crystal display device which includes two light diffusing layers such that the low refractive index regions are arranged in stripe patterns in the horizontal direction and the vertical direction (see FIG. 3), the viewing angle characteristics in the upward and downward directions and the horizontal directions are improved, and the viewing angle characteristics in the 45° direction and the 135° direction are also improved. It is also seen that the viewing angle characteristics in all the azimuths reach values which are close to $\gamma=2.2$.

Note that the half-value angle $\Delta\theta_{50}$ of the light emitted from the backlight unit used herein is about $\pm 35^\circ$, and this light includes rays which deteriorate the viewing angle characteristics. Therefore, by limiting the half-value angle $\Delta\theta_{50}$ to $\pm 25^\circ$ or less, more preferably by limiting $\Delta\theta_{50}$ to $\pm 15^\circ$ or less, the grayscale characteristic in an oblique viewing angle ($|\theta|>0$) can reach a value which is closer to $\gamma=2.2$. Note that, when the half-value angle $\Delta\theta_{50}$ is decreased, a viewer may feel a sense of discontinuity in the viewing angle characteristics as illustrated in FIG. 5(a). Therefore, decreasing the half-value angle $\Delta\theta_{50}$ is not necessarily required. Also, as will be described later, when employing a structure where light incident on the light diffusing layer 10 at a large angle of incidence is absorbed by the low refractive index regions 14, the directivity of light emitted from the backlight unit does not necessarily need to be increased, i.e., the half-value angle does not necessarily need to be decreased.

Next, the chromaticity change characteristic is described with reference to FIG. 9 and FIG. 10. FIG. 9 shows the color difference in a conventional liquid crystal display device. FIG. 10 shows the color difference in a liquid crystal display device of an embodiment of the present invention. In FIG. 10, measures are taken to prevent a local chromaticity change (a blue shift in chromaticity at a certain polar angle) in the polar angle dependence of the viewing angle characteristics which will be described later. The conventional liquid crystal display device has the viewing angle dependence of the γ characteristic which is shown in FIG. 6. The liquid crystal display device of this embodiment has the viewing angle dependence of the γ characteristic which is shown in FIG. 8. FIG. 9 and

FIG. 10 represent the chromaticity obtained when the display devices are viewed in the horizontal directions, showing the results obtained when the polar angle θ is 45° and 60° . FIG. 9 and FIG. 10 show the change in chromaticity (difference from the chromaticity at $\theta=0^\circ$ in the Macbeth chart which occurs depending on the viewing angle. The colors up to the 18th (cyan) from the left are chromatic colors, and the colors from the 19th (white) to the 24th (black) are achromatic colors, with the average values shown at the rightmost end.

As shown in FIG. 9, in the conventional liquid crystal display device, as for the chromaticity change in the respective colors at the polar angle $\theta=45^\circ$, some colors have large color differences $\Delta u'v'$ in the $u'v'$ chromaticity coordinates. On the other hand, as shown in FIG. 10, in the liquid crystal display device of the embodiment of the present invention, the color differences $\Delta u'v'$ are small values which are not more than 0.01.

The light diffusing layer of the embodiment of the present invention is not limited to the above-described examples but may be, for example, those illustrated in FIGS. 11(a) and 11(b).

The light diffusing layer 10 shown in FIG. 11(a) includes low refractive index regions 14a and 14b which extend perpendicular to each other to form a square grating. The light diffusing layers 10A and 10B of FIG. 3 are realized by a single light diffusing layer.

The light diffusing layer 10 shown in FIG. 11(b) includes generally-circular high refractive index regions 12 which are in a closest packed arrangement when viewed in a direction perpendicular to the major surfaces. The gaps between the high refractive index regions 12 are provided with a low refractive index region 14c. The shape of the low refractive index region 14c in a cross section perpendicular to the sheet of the drawing is an isosceles triangle (the bottom is on the anterior side of the sheet, and the vertex is on the posterior side). The light diffusing layer 10 shown in FIG. 11(b) serves substantially the same function and produces substantially the same effect as those of the light diffusing layer of FIG. 11(a). In the arrangement of the high refractive index regions 12 in the light diffusing layer 10 of FIG. 11(b), the ratio of the interval in a row direction, M_x , to the interval in a column direction, M_y , satisfies the relationship of $M_x:M_y=2:\sqrt{3}$. The packing fraction of the high refractive index regions in the major surface (sheet surface) of the light diffusing layer 10 on the light outgoing side is the maximum.

In the above-described light diffusing layer, the shape of a cross-section of the low refractive index region which is perpendicular to the major surface in a certain direction is approximated to an isosceles triangle and has the predetermined relationship which has been described with reference to FIG. 4. Therefore, the above-described light diffusing layer has such advantages that the light utilization efficiency is high and that the viewing angle characteristics are greatly improved. However, the light diffusing layer of the liquid crystal display device of the embodiment of the present invention is not limited to this example. Specifically, not only the light diffusing layer A but also light diffusing layers B and C may be used.

The light diffusing layer 10 may include a first region formed of the first substance that has first refractive index N_1 and a plurality of second regions formed of the second substance that has second refractive index N_2 such that the plurality of second regions are arranged in the first region at predetermined pitch P in one direction in a plane parallel to the second major surface, and that the plurality of second regions respectively have a plurality of interfaces with the first region, the interfaces being inclined by α° from the

normal of the second major surface. As the light diffusing layer 10, the light diffusing layer (light diffusion sheet) described in Patent Document 2 may be used. Note that the light diffusing layer described in Patent Document 2 is a diffusion sheet for use in rear projection type display devices and has a configuration that allows only near-collimated rays, which have the angle of incidence in the range of not less than 0° and not more than 10° , to efficiently undergo total reflection only once. Thus, a viewer may feel a sense of discontinuity in the light diffusion characteristics (a greater sense of discontinuity than FIG. 5(a)), and the improvement in viewing angle characteristics is small. A practical rear projection type display device includes a light scattering layer with a high Haze value which is provided over the front surface (viewer side) of such a light diffusion sheet that utilizes total reflection, whereby the sense of discontinuity in the diffusion characteristics is decreased.

As described above, only by providing a light diffusing layer that utilizes total reflection on the viewer side of the liquid crystal display panel, the viewing angle characteristics of the γ characteristic of a VA mode liquid crystal display device can be improved. However, as described above, the present inventor found a problem that, when a light diffusing layer which utilizes total reflection is provided on the viewer side of a direct-viewing type liquid crystal display panel, an overlapping image is visually perceived. This problem is specific to a case where the light diffusing layer is applied to the direct-viewing type.

Next, overlapping images which can be visually perceived when a light diffusing layer of an embodiment of the present invention is used are described with reference to FIGS. 12(a) and 12(b).

As schematically shown in FIG. 12(a), the light emitted from the backlight unit includes rays which meet $|\theta'|>0^\circ$ and which are emitted at angles that do not meet the total reflection conditions in the light diffusing layer. Therefore, a real image (primary image) produced by light of $\theta'=0^\circ$ and overlapping images (secondary images) produced by light incident at angles of $|\theta'|>0^\circ$ may be visually perceived. This is because the light incident on the light diffusing layer 10 at an angle of $|\theta'|>0^\circ$ outgoes frontward at a position distant by distance a (μm) from a position where the light incident at $\theta'=0^\circ$ outgoes from the high refractive index region 12a of the light diffusing layer 10. The light incident on the light diffusing layer 10 at an angle of $|\theta'|>0^\circ$ travels from the high refractive index region 12a into the low refractive index region 14 and is refracted there so as to outgo frontward. When a line for one pixel of the liquid crystal display device is lighted, a viewer viewing the liquid crystal display device in a direction perpendicular to the display surface would visually perceive a real image and overlapping images as shown in FIG. 12(b).

In FIG. 12(a), L_1 denotes the thickness of the base film 16, L_2 denotes the sum of the thickness of a glass substrate 20a and the thickness of the polarizing plate, and L_3 denotes the distance from the bottom surface of the high refractive index substance (first substance) to the vertex of the low refractive index substance (second substance) of the light diffusing layer 10.

θ' shown herein is an angle which represents the traveling direction of light inside the glass substrate 20a and the polarizing plate (not shown because it is thin) provided on the viewer side of the liquid crystal display panel 20. The light is refracted when entering a base film 16 and is again refracted when entering the high refractive index region 12 so as to travel with an angle smaller than θ' , although the difference in refractive index between these elements is small. Since the

decrease in the angle of incidence due to the refraction is not considered, the conditions obtained herein are to be stricter than the actual conditions.

The above-described overlapping images result from the fact that part of the light traveling from the high refractive index region **12** into the low refractive index regions **14** (the light incident at a smaller angle than the critical angle) is not totally reflected by the interfaces **12s** but is refracted to enter the low refractive index regions **14**, and the refracted light outgoes in a direction perpendicular to the display surface.

In a direct-viewing type liquid crystal display device, light emitted from the backlight unit is diffused light. Therefore, the light includes components which meet the following relationship (collimated light components):

$$N_1 \cos \alpha > N_2$$

On the other hand, some components of the oblique incident light ($\Delta\theta > 0$) do not meet the following relationship:

$$N_1 \cos(\theta + (2n-1)\alpha) > N_2 \quad (n \text{ is an integer not less than } 1).$$

Specifically, some components of the oblique incident light are not totally reflected at the interfaces **12s** but are refracted to enter the low refractive index regions **14**.

This problem can occur so long as there is an interface (between the high refractive index region and the low refractive index region) which is inclined relative to the major surface. The problem can occur not only when a light diffusing layer which meets the predetermined relationship described with reference to FIG. **4** is used, but also when the light diffusing layer described in Patent Document 2 is used.

A liquid crystal display device of the present invention provides a solution to this problem. Hereinafter, structures and functions are described which are capable of preventing visual perception of overlapping images that would occur in a direct-viewing type liquid crystal display device which includes a light diffusing layer that utilizes total reflection.

A possible countermeasure is to make overlapping images unperceivable by a human eye although occurrence of the overlapping images may be allowed. The visual acuity is measured as the resolution, i.e., the capability of distinguishing two adjacent dots as being separate from each other, with the use of the Landolt ring. The visual acuity is expressed as the inverse of the smallest detectable visual angle. A capability of distinguishing the visual angle of 1 arc minute (=one sixtieth ($1/60$) of one degree) is defined as "visual acuity 1.0". If the smallest detectable visual angle is 2 arc minutes, the visual acuity is 0.5. The standard distance for visual acuity measurement is 5 meters from the eye chart. In a Landolt ring corresponding to visual acuity 1.0, dots or lines which can be distinguished as being separate from each other are separated by a distance of 1.5 mm: Note that 1.5 mm corresponds to the visual angle of 1 arc minute when viewed from a position 5 meters away from the eye chart.

For example, a viewer who has the visual acuity of 1.0 based on the Landolt ring (1.0 arc minute in visual angle), 50 cm away from the liquid crystal display panel, can distinguish the distance of 150 μm (precisely, 145 μm). Thus, when a is 150 μm or less, visual perception of overlapping images can be efficiently prevented. Therefore, assuming that the sum of L and H is the total distance, the condition of $\tan \theta^*(L+H) < 150 \mu\text{m}$ may be met. The present inventor performed a subjective evaluation and obtained a result that, for a viewer at a position 50 cm away from the liquid crystal display panel, the acceptable value of distance a was 250 μm or less. This corresponds to a visual angle of 1.7 arc minutes or less.

Here, the description is provided with a liquid crystal display device example which employs the configuration shown

in FIG. **3** so that the viewing angle characteristics in the rightward and leftward (horizontal) directions are improved. Specifically, the first light diffusing layer **10A** is closer to the liquid crystal display panel **20** than the second light diffusing layer **10B** is. The plurality of second regions **14** of the first light diffusing layer **10A** (each being a rectangular region) are arranged in a stripe pattern along a horizontal direction of the liquid crystal display panel **20**. The plurality of second regions **14** of the second light diffusing layer **10B** (each being a rectangular region) are arranged in a stripe pattern along a vertical direction of the liquid crystal display panel **20**. The polarization axis of one of a pair of polarizing plates (not shown) extends in the horizontal direction, and the polarization axis of the other extends in the vertical direction. The liquid crystal display panel **20** may be of the above-described VA mode or may be of any other display mode.

The first light diffusing layer **10A** is provided on the viewer side of the liquid crystal display panel **20** with a base film **16** interposed therebetween as shown in FIG. **12(a)**. The second light diffusing layer **10B** may be provided over the first light diffusing layer **10A** with a base film interposed therebetween. However, to prevent occurrence of overlapping images, a base film preferably does not intervene between the second light diffusing layer **10B** and the first light diffusing layer **10A**.

In FIG. **12(a)**, in consideration of the total distance of L and H (the height of the low refractive index regions **14**), a can be described as $\tan \theta^*(L+H)$. Thus, as the value of L+H decreases, a decreases so that overlapping images are less likely to be visually perceived. The light diffusing layer **10A**, which is closer to the liquid crystal display panel **20**, can have a smaller L+H distance than the light diffusing layer **10B**, and therefore can make overlapping images in the horizontal direction less perceivable. Human eyes lie side by side and are therefore more likely to perceive overlapping images in the horizontal direction. As such, to make overlapping images less perceivable, preferably, the first light diffusing layer **10A**, which includes vertically-extending low refractive index regions that are arranged in a stripe pattern along the horizontal direction, is provided closer to the liquid crystal panel **20**.

Note that the value of L in the light diffusing layer **10B** includes, as shown in FIG. **12(a)**, the glass substrate **20a** on the viewer side of the liquid crystal display panel **20**, a polarizing plate (not shown), the base film **16**, and the light diffusing layer **10** of the light diffusing layer **10A**. Therefore, L of the light diffusing layer **10B** is necessarily greater than L of the light diffusing layer **10A** that is provided near the liquid crystal display panel **20**. As a matter of course, the light diffusing layer **10B** provided on the viewer side preferably meets the above-described conditions. Also, using the light diffusing layers illustrated in FIGS. **11(a)** and **11(b)** provides an advantage that overlapping images can be made less perceivable in both the horizontal directions and the vertical directions.

FIG. **13** is a graph showing the thickness (L+H) dependence of position a where an overlapping image occurs, which was experimentally obtained. FIG. **14** shows an example of line profiles which represent actual measurement results of overlapping images. In FIG. **14**, the abscissa axis represents the position, and the ordinate axis represents the luminance. The graph of FIG. **13** was plotted based on the results shown in FIG. **14**.

In FIG. **14**, only one white display line was displayed (RGB were lighted) on the liquid crystal display device, the luminance of the white display line was detected using a CCD camera, and a cross-sectional profile of the luminance was measured by an image processing operation. FIG. **14** shows

an example of three line profiles on the conditions of no light diffusing layer, $L+H=830\text{ }\mu\text{m}$, and $L+H=1230\text{ }\mu\text{m}$, although the actual measurement values were obtained from 10 different samples in total under the conditions where L_1 was any of 5 different values, $0\text{ }\mu\text{m}$, $50\text{ }\mu\text{m}$, $75\text{ }\mu\text{m}$, $100\text{ }\mu\text{m}$, and $190\text{ }\mu\text{m}$, L_2 was any of two different values, $500\text{ }\mu\text{m}$ and $900\text{ }\mu\text{m}$ (the thickness of the polarizing plate was fixed at $200\text{ }\mu\text{m}$), and L_3 was $30\text{ }\mu\text{m}$. In FIG. 14, no overlapping image occurs in the case of no light diffusing layer. That is, a luminance peak which would correspond to an overlapping image does not occur. In the cases of $L+H=830\text{ }\mu\text{m}$ and $L+H=1230\text{ }\mu\text{m}$, the profiles have luminance peaks that correspond to overlapping images, as indicated by down arrows in FIG. 14. In these luminance line profiles, a half of the distance between the overlapping image peaks corresponds to a .

In FIG. 13, open diamonds ($\diamond$) represent actually measured values a with varying thickness $L+H$. The solid line represents the calculated value of a , which is $a=\tan\theta^*(L+H)$. The value of θ^* that was used in the calculation of values A and B of the graph was calculated from a luminance peak perceived at the position of polar angle θ^* among the luminance peaks perceived at the positions of polar angle 0° and polar angle θ' (polar angle $\Delta\theta$ in the air) under a circumstance where collimated light comes into the light diffusing layer from the base side of the isosceles triangle of the low refractive index regions (from the upper side of FIG. 12(a)). Although θ^* can be obtained by actual measurement as described above, θ^* of a light beam which produces an overlapping image in a frontward direction (direction of polar angle 0°) can be theoretically calculated by formula (9) show below:

$$\theta' = 90 - \sin^{-1}\left(\frac{N_2}{N_1} \times \cos\alpha\right) - \alpha \quad (9)$$

In FIG. 13, actually measured values (measurement wavelength: 550 nm) correspond to $N_1=1.59$ and $N_2=1.45$. Calculated values A correspond to $N_1=1.59$ and $N_2=1.45$. Calculated values B correspond to $N_1=1.59$ and $N_2=1.49$. α is commonly 8° .

As for the actually measured values shown in FIG. 13, L_1 was any of the five values, $0\text{ }\mu\text{m}$, $50\text{ }\mu\text{m}$, $75\text{ }\mu\text{m}$, $100\text{ }\mu\text{m}$, and $190\text{ }\mu\text{m}$. L_2 was any of the two values, $500\text{ }\mu\text{m}$ and $900\text{ }\mu\text{m}$ (the thickness of the polarizing plate is fixed at $200\text{ }\mu\text{m}$). L_3 was $30\text{ }\mu\text{m}$. Therefore, L was the sum of a combination of these values, resulting in 10 different actually measured values in total. H was $110\text{ }\mu\text{m}$. As seen from FIG. 13, the actually measured values and calculated values A exhibit good agreement. This agreement can be a basis for a conclusion that calculated values B are also correct both quantitatively and theoretically.

As seen from FIG. 13, in the case of calculated values A , to adjust a to $150\text{ }\mu\text{m}$ or less, i.e., to adjust $\theta_B=\tan^{-1}(a/Lb)$ to 1.0 arc minute (=one sixtieth ($1/60$) of one degree) or less where θ_B is an angle between an overlapping image ray and a real image ray and Lb is the viewing distance, total thickness $L+H$ (sometimes denoted by "Lt") may preferably be not more than $480\text{ }\mu\text{m}$. For example, a possible combination which allows $L+H$ to be not more than $480\text{ }\mu\text{m}$ is $0\text{ }\mu\text{m}$ for L_1 , $360\text{ }\mu\text{m}$ for L_2 ($260\text{ }\mu\text{m}$ thick glass substrate and $100\text{ }\mu\text{m}$ thick polarizing plate), $10\text{ }\mu\text{m}$ for L_3 , and $110\text{ }\mu\text{m}$ for H . As a matter of course, the present invention is not limited to this combination. Any combination is acceptable so long as $L+H$ is $480\text{ }\mu\text{m}$ or less. In the case of calculated values B , in order to adjust a to $150\text{ }\mu\text{m}$ or less, total thickness $L+H$ is preferably $600\text{ }\mu\text{m}$ or

less. In this case also, the present invention is not limited to this combination, and any combination is acceptable.

It is also understood from the result of the subjective evaluation that, to adjust a to $250\text{ }\mu\text{m}$ or less, i.e., to adjust θ_B to 1.7 arc minutes or less, total thickness $L+H$ for calculated values A is preferably $800\text{ }\mu\text{m}$ or less, and total thickness $L+H$ for calculated values B is preferably $980\text{ }\mu\text{m}$ or less. In this case also, total thickness $L+H$ may be realized by any combination. When the structure shown in FIG. 3 is employed and the viewing angle characteristics in the rightward and leftward directions are considered to be more important, such an arrangement can effectively prevent occurrence of overlapping images in the rightward and leftward directions, so that the display characteristics do not degrade.

Further, when the structure shown in FIG. 3 is employed, the liquid crystal display device includes two light diffusing layers 10A and 10B. Therefore, in this case, the total thickness ($2L_1+L_2+2L_3+2H$) may preferably be not more than the values shown above for the respective cases. In this case also, any combination may be acceptable. Such a configuration can effectively prevent occurrence of overlapping images in the rightward and leftward directions as well as effectively prevent occurrence of overlapping images in the upper and lower directions, even when the viewing angle characteristics in the rightward and leftward directions are considered to be more important. Thus, the display characteristics do not degrade in any azimuth.

As appreciated from formula (9) shown above, the above-described value varies as the values of N_1 and N_2 are changed. Therefore, the optimum value of $L+H$ may be determined depending on the configuration.

Note that the typical viewing distance of a liquid crystal display device depends on the use of the device. For example, in monitor applications, it is about 50 cm . Also, it can be generally said that the typical viewing distance of the liquid crystal display device may be longer than a distance with which black matrix (BM) formed between pixels cannot be clearly distinguished. For example, for the BM width of $50\text{ }\mu\text{m}$, the minimum viewing distance is 10 cm when θ_B is 1.7 arc minutes. When θ_B is 1.0 arc minute, the minimum viewing distance is 18 cm .

(Other Countermeasure 1)

Occurrence of overlapping images can be effectively prevented by mixing a material which has the property of absorbing visible light in the low refractive index regions 14 in order to absorb light which comes in the low refractive index regions 14. The material which absorbs visible light may preferably be, for example, carbon black or a mixture of a blue pigment and a red pigment. The visible light absorbance is preferably 95% or more, and more preferably 99% or more.

(Other Countermeasure 2)

To prevent light which comes in the low refractive index regions 14 from outgoing in a direction perpendicular to the display surface, refraction of the light at the low refractive index regions 14 is prevented. This may be accomplished so long as the following condition, which is transformed from formula (2) on the assumption that total reflection occurs n times, is met.

$$N_1 \cos\left\{\sin^{-1}\left(\frac{\sin\Delta\theta}{N_1}\right) + n\alpha\right\} > N_2$$

(n is an integer not less than 1)

For example, $\Delta\theta$ is about 27° . Therefore, by limiting all the light beams emitted from the backlight unit to 27° or less,

overlapping images can be extremely decreased. When light of $n=2$ is further considered, overlapping images cannot be visually perceived in principle by limiting all the light beams from the backlight unit to 13° or less.

Other Countermeasures 1 and 2 described above may be employed separately or in combination. To solve the above-described problem of overlapping images, increasing the directivity of the backlight (decreasing the half-value angle) may be preferable. However, if the directivity of the backlight is excessively increased, the peaks of once-totally-reflected light and twice-totally-reflected light are conspicuous as shown in FIG. 5(a), resulting in a sense of discontinuity in the viewing angle characteristics. Thus, to effectively prevent occurrence of overlapping images, priority is preferably given to Other Countermeasure 1.

As described above, only by providing a light diffusing layer that utilizes total reflection on the viewer side of the liquid crystal display panel, the viewing angle characteristics of the γ characteristic of a VA mode liquid crystal display device can be improved. Further, the distance from the liquid crystal layer to the second major surface of the light diffusing layer can be controlled, and the overlapping image problem can be solved by Other Countermeasures 1 and 2. However, the present inventor found the problem of a local chromaticity change (a blue shift in chromaticity at a certain polar angle) in the polar angle dependence of the viewing angle. This problem is specific to a case where the light diffusing layer is applied to the direct-viewing type.

This problem is due to the fact that the backlight unit used herein emits diffused light as well as the fact that refractive index N_1 of the first substance and refractive index N_2 of the second substance have wavelength dispersion. Specifically, the problem is due to the fact that, as for a light beam $\Delta\theta$ which is emitted from the backlight unit and transmitted through the liquid crystal display panel to enter the first region (refractive index N_1) of the light diffusing layer, whether or not the light meets formula (2) of paragraph [0038] at a sloped interface between the first region and the second region (refractive index N_2) depends on the wavelength of the light.

Specifically, even at the same angle of incidence, whether the reflection is total reflection or partial reflection depends on the wavelength of the incident light. In the case of partial reflection, part of the light is refracted at the interface to enter the second region. This is due to the fact that the refractive indices of materials themselves have wavelength dispersion (wavelength dependence). For example, when the light diffusing layer of $N_1=1.59$, $N_2=1.50$, and $\alpha=8.0^\circ$ is used, a light beam emitted from the backlight unit with an inclination of about 30° passes through the liquid crystal display panel and then travels through the first region with θ' =about 18° before outgoing toward the viewer side with an inclination of about 60° . At the interface between the first region and the second region, total reflection does not occur in the whole wavelength range, i.e., partial reflection occurs in some wavelength bands. Therefore, the reflectance depends on the wavelength, and the spectrum of light radiated from the backlight unit changes as it passes through the light diffusion sheet and outgo toward the viewer side, resulting in a change in colors.

Formula (2) of paragraph [0038], which represents the total reflection condition, can be transformed to the following formula:

$$\cos(\theta' + \alpha) > \frac{N_2(\lambda)}{N_1(\lambda)}$$

where λ is the wavelength. Since the refractive index is a function of the wavelength, whether or not total reflection occurs depends on the wavelength. Note that, when the wavelength dependence is not considered, the refractive index is represented by a refractive index for the light at the wavelength of 550 nm.

When the total reflection condition defined by the above formula is not met, partial reflection occurs. Therefore, under a circumstance where the polarization of the light is s-polarization, reflectance R is as follows:

$$R = \left(\frac{N_1(\lambda) \cdot \cos(90 - \theta' - \alpha) - N_2(\lambda) \cdot \cos\theta_3}{N_1(\lambda) \cdot \cos(90 - \theta' - \alpha) + N_2(\lambda) \cdot \cos\theta_3} \right)^2$$

$$= \left(\frac{\frac{N_1(\lambda)}{N_2(\lambda)} \cdot \sin(\theta' + \alpha) - \cos\theta_3}{\frac{N_1(\lambda)}{N_2(\lambda)} \cdot \sin(\theta' + \alpha) + \cos\theta_3} \right)^2$$

where θ_3 is the angle of refraction which occurs when the light enters the second region. This gives

$$\theta_3 = \sin^{-1} \left[\frac{N_1(\lambda)}{N_2(\lambda)} \cdot \cos(\theta' + \alpha) \right]$$

$\theta_3=90^\circ$ corresponds to total reflection. Thus, if the ratio of N_1 to N_2 is constant irrespective of the wavelength, reflectance R does not depend on the wavelength. So long as reflectance R does not depend on the wavelength, the spectrum of light emitted from the backlight unit is not changed by reflection at the interface 12 between the high refractive index region 12 and the low refractive index regions 14, so that the display colors do not vary.

The wavelength dispersion of the refractive index of materials generally includes "no wavelength dispersion" (the refractive index is substantially constant irrespective of the wavelength), "normal dispersion" (the refractive index decreases as the wavelength increases), and "anomalous dispersion" (the refractive index increases as the wavelength increases). Among these, "no wavelength dispersion" and "normal dispersion" mainly occur. The wavelength dispersion of the refractive index can be described by the Cauchy's dispersion formula.

A local blue shift in chromaticity (at aforementioned polar angle 60°) in the polar angle dependence of the viewing angle characteristics discussed herein remarkably occurs in a combination of "normal dispersion" and "normal dispersion" or a combination of "normal dispersion" and "no wavelength dispersion". This is because, if both N_1 and N_2 have normal dispersion, the difference in refractive index between N_1 and N_2 decreases as the wavelength increases. Specifically, as the wavelength increases, the probability of meeting the relationship defined by the formula of paragraph [0094] decreases. Therefore, the reflectance decreases as the wavelength increases. Thus, when light passes through the light diffusing layer, the spectrum of the light varies. In this case, a blue shift in chromaticity occurs.

When the wavelength dispersion of the refractive index is considered, using materials with no wavelength dispersion for both N_1 and N_2 is desirable for maintaining the ratio of N_1 to N_2 constant. When normal dispersion materials are used for both N_1 and N_2 , the materials may be selected such that the ratio of N_1 to N_2 is constant in the visible light wavelength range (not less than 400 nm and not more than 800 nm).

Specifically, the difference between the maximum and the minimum of N_1/N_2 in the visible light wavelength range may be not more than 0.02 of the average of N_1/N_2 in the visible light wavelength range. Such materials may be selected as necessary.

Alternatively, by setting the refractive indices so as to meet the twice-total-reflection condition, such as a combination of $N_1=1.59$ and $N_2=1.40$, a blue shift in chromaticity can be prevented without maintaining the ratio of N_1 to N_2 constant in the visible light wavelength range.

Although the description has been provided herein with an example of s-polarization, the same also applies to p-polarization.

Thus, as understood from the foregoing, the viewing angle characteristics of the γ characteristic of a VA mode liquid crystal display device can be improved only by providing a light diffusing layer that utilizes total reflection on the viewer side of the liquid crystal display panel. Further, the distance from the liquid crystal layer to the second major surface of the light diffusing layer can be controlled, and the overlapping image problem can be solved by Other Countermeasures 1 and 2. Furthermore, a local chromaticity change in the polar angle dependence of the viewing angle characteristics can be prevented by maintaining the ratio of N_1 to N_2 constant irrespective of the wavelength.

The light diffusing layer of an embodiment of the present invention includes a plurality of low refractive index regions which are arranged at a predetermined pitch in at least one direction as described above. As well known, if periodic structures having slightly different pitches are stacked one on the other, moiré is generated. Therefore, if the pitch of the periodic structure formed by the low refractive index regions of the light diffusing layer and the pitch of the periodic structure of the pixels of the liquid crystal display panel are slightly different, moiré may be generated. To effectively prevent generation of moiré without degrading the display quality, the pitch of the periodic structure formed by the low refractive index regions is preferably not more than three quarters of the arrangement pitch of the pixels in the same direction, and two or more low refractive index regions are preferably placed within the extent of the opening of a pixel. The arrangement direction of the low refractive index regions preferably has an inclination of 1° or more relative to a bus line of the liquid crystal display panel (a gate bus line, a source bus line, and/or a CS bus line).

The liquid crystal display device **100** shown in FIG. **2** includes the light diffusing layer **10** as described above. The light diffusing layer **10** includes a plurality of vertically-extending rectangular second regions (low refractive index regions) **14** which are arranged in a stripe pattern along a horizontal direction. The light diffusing layer **10** improves the viewing angle characteristics in the horizontal directions. The liquid crystal display device **110** shown in FIG. **3** includes the light diffusing layers **10A** and **10B**. The light diffusing layer **10A**, which is closer to the liquid crystal display panel **20**, includes a plurality of vertically-extending rectangular second regions (low refractive index regions) **14** which are arranged in a stripe pattern along a horizontal direction. The light diffusing layer **10B**, which is closer to the viewer side, includes a plurality of horizontally-extending rectangular second regions **14** which are arranged in a stripe pattern along a vertical direction. The light diffusing layer **10A** improves the viewing angle characteristic in the horizontal direction. The light diffusing layer **10B** improves the viewing angle characteristic in the vertical direction.

As in a liquid crystal display device **100A** shown in FIG. **15(a)**, a light scattering layer (diffuse reflection layer) **40** may

be provided on the viewer side of the light diffusing layer **10** of the liquid crystal display device **100**. Alternatively, as in a liquid crystal display device **110A** shown in FIG. **15(b)**, a light scattering layer (diffuse reflection layer) **40** may be provided on the viewer side of the light diffusing layer **10B** of the light diffusing layer **10** of the liquid crystal display device **110**. The light scattering layer **40** may be formed of, for example, a material composed of a resin and particles dispersed therein, the particles having a different refractive index from that of the resin. The light scattering layer **40** may function as an antiglare layer. As a matter of course, as described above, the viewer side of the light diffusing layer **10** or the light diffusing layer **10B** may be provided with another element, such as an antireflection layer, a low reflection layer, or a reflection preventing layer. As a matter of course, any two or more of these elements may be used in combination when necessary.

INDUSTRIAL APPLICABILITY

The present invention is applicable to a wide variety of known liquid crystal display devices and is capable of improving the viewing angle characteristics.

The invention claimed is:

1. A liquid crystal display device, comprising:

a liquid crystal display panel which has a pair of polarizing plates; and

a first light diffusing layer which has a first major surface and a second major surface opposing each other and which is arranged such that the first major surface opposes a viewer side surface of the liquid crystal display panel, wherein

the first light diffusing layer includes a first region formed of a first substance which has a first refractive index N_1 and a plurality of second regions formed of a second substance which has a second refractive index N_2 , the second refractive index N_2 being smaller than the first refractive index N_1 ,

the plurality of second regions are arranged in the first region at a predetermined pitch P in one direction in a plane parallel to the second major surface,

each of the plurality of second regions forms a plurality of interfaces with the first region, the interfaces being inclined by α° from a normal of the second major surface, and

θ_B shown below is not more than 1.7 arc minutes

$$\theta_B = \tan^{-1} \left(\frac{a}{Lb} \right)$$

where Lb is a typical viewing distance of the liquid crystal display panel, and a is expressed as follows:

$$a = \tan \theta \times Lt$$

in which Lt is a distance from the second major surface to a liquid crystal layer side surface of a viewer side substrate of the liquid crystal display panel, and θ' is expressed as follows:

$$\theta' = 90 - \sin^{-1} \left(\frac{N_2}{N_1} \times \cos \alpha \right) - \alpha.$$

2. The liquid crystal display device of claim **1**, wherein θ_B is not more than 1.0 arc minute.

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3. The liquid crystal display device of claim 1, wherein each of the second regions is approximated to an isosceles triangle where a base is on the second major surface side, a vertex is on the first major surface side, and a vertex angle is 2α .

4. The liquid crystal display device of claim 3, wherein formulae shown below are met:

$$H \leq \frac{P}{\tan 2\alpha + \tan \alpha}$$

and

$$\cos[\alpha(2n - 1)] > \frac{N_2}{N_1}$$

where H is a height of the isosceles triangle, and n is an integer not less than 2.

5. The liquid crystal display device of claim 1, wherein the plurality of second regions of the first light diffusing layer are arranged in a stripe pattern along a horizontal direction of the liquid crystal display panel.

6. The liquid crystal display device of claim 1, further comprising a light scattering layer on a viewer side of the first light diffusing layer.

7. The liquid crystal display device of claim 1, further comprising a second light diffusing layer on a viewer side of the first light diffusing layer, wherein

the second light diffusing layer includes a first region formed of a first substance which has a first refractive index N_1 and a plurality of second regions formed of a second substance which has a second refractive index N_2 , the second refractive index N_2 being smaller than the first refractive index N_1 ,

the plurality of second regions are arranged in the first region at a predetermined pitch P in one direction in a plane parallel to the second major surface, and each of the plurality of second regions forms a plurality of interfaces with the first region, the interfaces being inclined by α° from a normal of the second major surface.

8. The liquid crystal display device of claim 7, wherein each of the second regions is approximated to an isosceles

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triangle where a base is on the second major surface side, a vertex is on the first major surface side, and a vertex angle is 2α .

9. The liquid crystal display device of claim 8, wherein formulae shown below are met:

$$H' \leq \frac{P}{\tan 2\alpha + \tan \alpha}$$

and

$$\cos[\alpha(2n' - 1)] > \frac{N_2}{N_1}$$

where H' is a height of the isosceles triangle, and n' is an integer not less than 2.

10. The liquid crystal display device of claim 7, wherein the plurality of second regions of the first light diffusing layer are arranged in a stripe pattern along a horizontal direction of the liquid crystal display panel,

and

the plurality of second regions of the second light diffusing layer are arranged in a stripe pattern along a vertical direction of the liquid crystal display panel.

11. The liquid crystal display device of claim 7, further comprising a light scattering layer on a viewer side of the second light diffusing layer.

12. The liquid crystal display device of claim 1, wherein when the first light diffusing layer is viewed in a direction perpendicular to the second major surface, the plurality of first regions each have a generally circular shape and are arranged in a square grating arrangement or a closest packed arrangement.

13. The liquid crystal display device of claim 1, wherein a difference between a maximum and a minimum of N_1/N_2 in a wavelength range from 400 nm to 800 nm is not more than 0.02 of an average of N_1/N_2 in the wavelength range.

14. The liquid crystal display device of claim 1, wherein the second regions further include a substance which absorbs visible light.

15. The liquid crystal display device of claim 1, wherein the predetermined pitch P is not more than three quarters of a pixel pitch in the direction.

* * * * *

专利名称(译)	液晶显示装置		
公开(公告)号	US8154692	公开(公告)日	2012-04-10
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[标]申请(专利权)人(译)	夏普株式会社		
申请(专利权)人(译)	夏普株式会社		
当前申请(专利权)人(译)	夏普株式会社		
[标]发明人	NISHIHARA YUSUKE AOYAMA IORI TAGUCHI TOKIO YAMAMOTO AKIHIRO KUBO MASUMI		
发明人	NISHIHARA, YUSUKE AOYAMA, IORI TAGUCHI, TOKIO YAMAMOTO, AKIHIRO KUBO, MASUMI		
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摘要(译)

本发明的液晶显示装置包括液晶显示面板和光漫射层，该光漫射层具有第一和第二主表面，并且布置成使得第一主表面与液晶显示面板的观察者侧表面相对。光漫射层包括由具有第一折射率N1的第一物质形成的第一区域和由具有第二折射率N2 (<N1) 的第二物质形成的多个第二区域。第二区域在平行于第二主表面的平面中沿一个方向以预定间距P布置在第一区域中，每个第二区域形成与第一区域的界面，界面从法线的法线倾斜 α° 第二个主要表面。由 $\theta_B = \tan^{-1} (a / L_b)$ 表示的 θ_B 不大于1.7弧分，其中 L_b 是典型的观察距离， a 由 $a = \tan \theta \times L_t$ 表示，其中 θ 是角度从 α ，N1和N2获得的入射率，并且 L_t 是从液晶显示面板的观察者侧基板的第二主表面到液晶层侧表面的距离。根据本发明，通过使用利用全反射的光漫射层，可以改善直视型液晶显示装置的视角特性。

